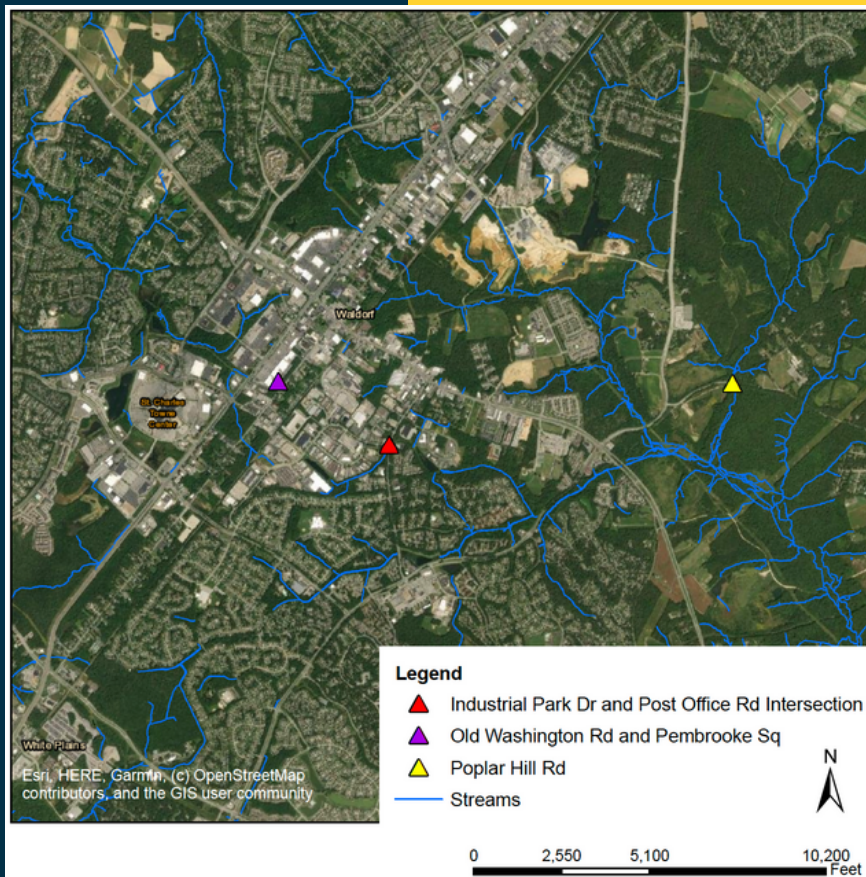


Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

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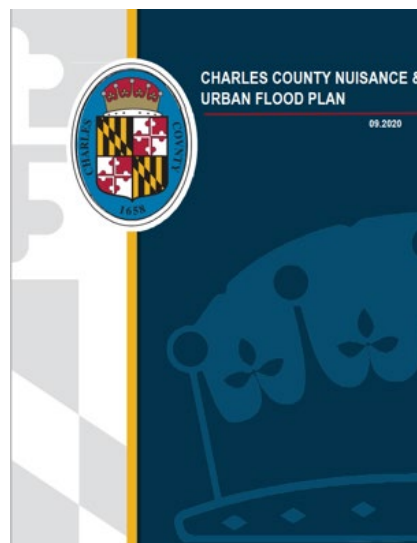
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Section 1 - Purpose of Study and Context

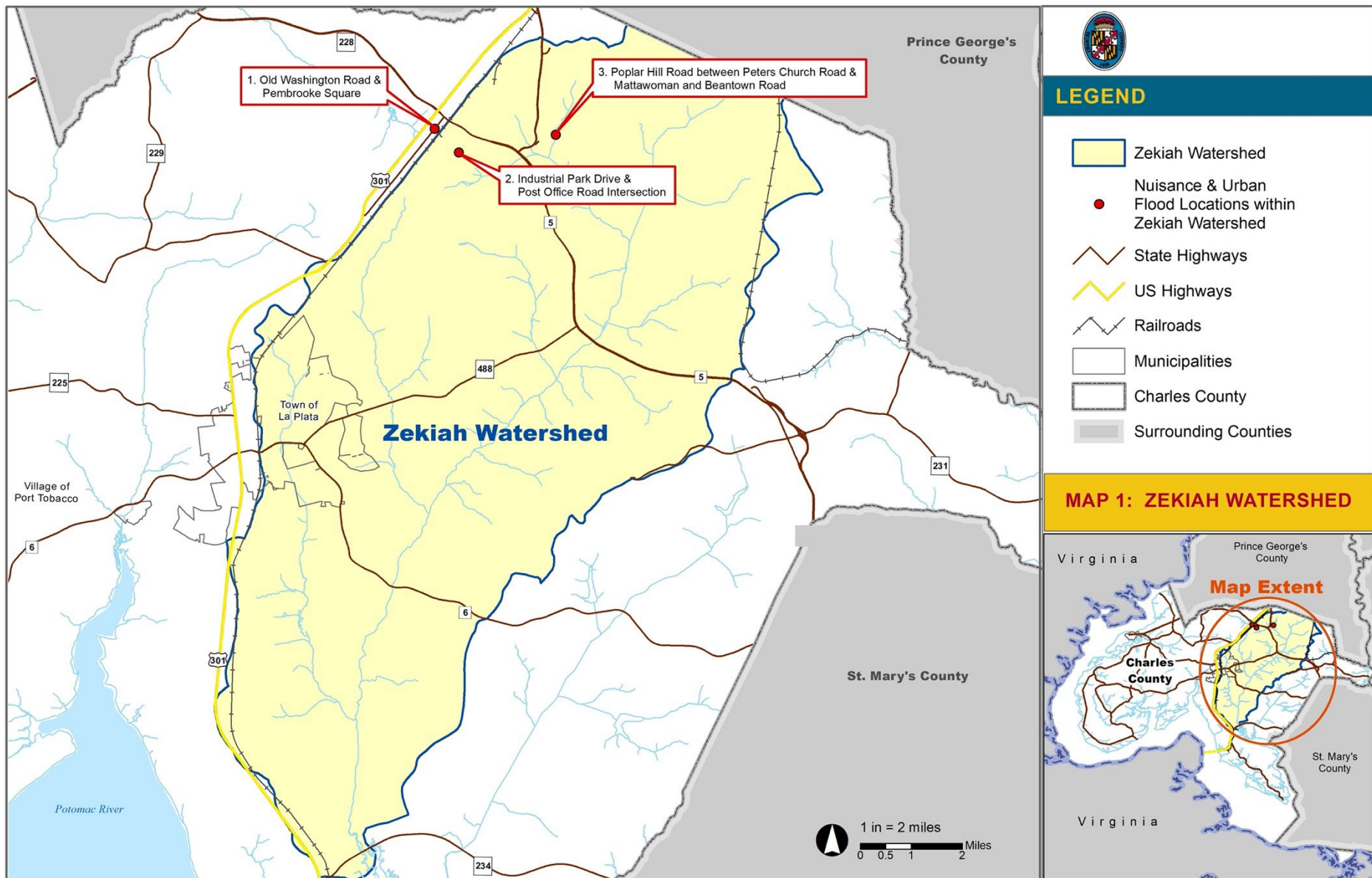
Charles County, Maryland is experiencing flooding outside mapped floodplains with increasing frequency, including both nuisance and urban flooding. Nuisance flooding is associated with high tides that flow back through the stormwater system, increasing/raising the level of groundwater, and overtopping the banks and edge of waterways. Nuisance flooding is an indicator of rising water levels in the Chesapeake Bay and its tributaries. Areas that were previously dry now flood during high tides because the water elevation is high enough to lap over the banks of waterways and to enter stormwater systems through outfalls that were previously high enough to prevent backflow, while allowing outflow. Urban flooding is due to a variety of issues related to development: increased impervious surface, disruption of natural watershed flows and functions, undersized and aged stormwater infrastructure, and changing weather patterns which exacerbate the inadequacies of older stormwater systems and the fragmented watersheds. Urban flooding reflects decades of development that has outstripped the capacity of stormwater infrastructure and disrupted the natural flow and discharge of watersheds. Additionally, many stormwater systems are beyond their expected useful life and in need of repair and replacement. These challenges are compounded by what is becoming the new normal: an increase in the frequency and intensity of storms caused by higher global temperatures that increase evaporation in the ocean and atmosphere, creating more favorable conditions for heavier and more frequent precipitation.

Charles County Nuisance & Urban Flood Plan

To further explore these challenges, forty-eight urban flood locations were identified and prioritized for additional analysis and flood risk reduction solutions in the [2020 CHARLES COUNTY NUISANCE & URBAN FLOOD PLAN](#). The purpose of the nuisance flood plan is to identify sources of nuisance and urban flooding, analyze flood hazards, and recommend actions to reduce flooding and increase community resiliency. The plan fulfills the requirements set forth in Maryland House Bill 1427 (2019), §3-1018(b) and (c), which requires that all local jurisdictions that experience nuisance flooding must develop a nuisance flood plan to address that flooding and update the plan every five years. To maintain the mandated update cycle, the plan will be appended to become part of the County's 2018 Hazard Mitigation Plan Update, which must also be updated every five years.



As part of the nuisance flood plan implementation strategy the county has initiated independent watershed studies to address issues identified in the nuisance flood plan that will serve to build upon and expand this analysis to identify and track localized flood events, mitigate localized flooding. Three of the identified locations are within the **Zekiah Watershed** have been targeted for further analysis and will be addressed in this study. These locations are identified on the location map on the following page.



The frequency and intensity of storms is increasing due to the changing climate that will continue to exacerbate the flood issues at these three locations. The stormwater infrastructure in these areas is aging and was not designed to convey the amount of runoff that is currently occurring and amounts that are predicted to occur in the future. As urbanization and the amount of impervious surface increase the capacity of the existing systems to convey runoff will be reduced. Localized flooding and impaired water quality in these locations are related to untreated stormwater. Without stormwater best management practices or green infrastructure in place to reduce the depth of floodwater and improve water quality, these areas will continue to experience flooding and degraded water quality and habitat in the affected tributaries.

Zekiah Watershed Urban Flood Study Objectives and Expected Outcomes

The Zekiah Watershed Urban Flood Study will be an important tool for future planning capital improvement projects. Principles, policies, and recommendations from County plans are integrated into the study to ensure that a mutually supportive resilience framework exists throughout all County planning efforts. The study concentrates on addressing 4 key objectives:

1. Analyze the cause(s) of flooding at the three locations.
2. Identify solutions that eliminate flooding, improve water quality, and account for future precipitation volumes.
3. Develop conceptual designs to guide implementation of solutions at all three locations.
4. Identify funding opportunities to implement solutions.

The stormwater improvements that are identified in this study will support the goals and policies articulated in the 2018 Charles County Hazard Mitigation Plan Update, the 2020 Charles County Nuisance and Urban Flood Plan, and the Charles County Comprehensive Plan (2016), Charles County Stormwater Management Ordinance and Drainage Ordinance, plus any relevant watershed improvement plans and studies as appropriate for addressing water quantity and quality within the study area.

The solutions identified in this study account for future conditions such as increased volumes of stormwater from more frequent, intense storms and future development in the project areas. The solutions will also integrate a comprehensive approach that will support the implementation of nature-based infrastructure.

Changes in climate are making weather less predictable and generating bigger, stronger storms. Severe storms coupled with increased development in watersheds and an increase in impervious surfaces creates a volume of runoff that is greater than the design capacity of the existing infrastructure throughout the county.

Tools and Resources

This study utilized information gathered from the Charles County Nuisance & Urban Flood Plan, particularly data gathered about the flood characteristics at each location, engaging with County staff who served on the Plan's Stakeholder Group. As part of the ongoing planning process an update to the outreach vehicles used for the Plan (Story Map, web page on County website), will also be updated to include the results of the Zekiah watershed study. Information from Risk Map products, discharge points, and bridges and culverts layers and data contained within MDE's Flood Risk Application and County data resources were used to generate existing and future condition models for this project.

Partner Roles

The study was led by steering committee that is made up of staff from the Department of Emergency Services and Department of Planning and Growth Management. The steering committee will provide overall guidance for the project so that the identified solutions are ones supported by the County, and property owners. The steering committee consisted of the following members:

Zekiah Urban Watershed Study Steering Committee

Name	Title	Department/Contractor
Michelle L. Lilly	Director, Charles County	Charles County Emergency Services
Gary Lewis	Emergency Management Specialist	Charles County Emergency Services
Kerry Kirkwood	Engineer I	Charles County Planning and Growth Management
Beth Groth	Climate Resilience and Sustainability Officer	Resilience Authority of Charles County
Kelly Palmer	Floodplain Manager	Charles County Planning and Growth Management
Karen Wiggen	Planner III	Charles County Planning and Growth Management
Kayla Rhue	Associate Engineer	MES
John Groeger	Senior Engineer	MES
Mark James	Project Manager	Michael Baker
Lori Wade	Department Manager - Environmental Resources Water and Community Planning	Michael Baker
Calt, Elizabeth	Civil Associate – Water	Michael Baker
Virginia Smith	Outreach	Smith Planning and Design

Section 2 - Planning Process

Steering Committee Meetings

Starting in June the Steering Committee began meeting monthly to discuss project development. Copies of meeting slides are provided in Attachment 1. The first steering committee meeting was held virtually on June 9, 2022. This meeting was scheduled to introduce key members of the contracting team, discuss project schedule, and contractor expectations. A data was also made at this time and filled by County GIS resources. Agenda items included:

- Introductions
- Tracking Project to Match Grant
- Project Review and Suggestions
- Data Requests
 - Start off with H&H Analysis
 - Extents of flooding – Inundation Areas and Historic Anticipated Damages
 - Stormwater Infrastructure
 - HMP/NFP Plan
 - Models – DFIRM RiskMAP
 - Utilities / ROW
 - Additional Supplemental Survey Data (may be able to do quick data capture during field meeting or with survey crew)
- Schedule and Project Involvement (Stakeholders)
- Potential Stalls
- Next Steps – Field Meeting (initiate data gathering?)

Data Use Agreements were signed for use of Planning and Growth Management's GIS data. Requested data was transferred and saved to a project teams location. A list of County data resource that were transferred is provided in Attachment 2.

A second team meeting was held in the field on July 28. Staff from Department of Emergency Services and Department of Planning and Growth Management along with consultants conducted a tour of 3 locations where site information was gathered on existing conditions. Field observations and recommendations are summarized and documented in Attachment 3.

During the August 25 steering committee meeting project site review and considerations that were gathered and refined after the field visit. The steering committee were presented site specific data and relevant resources. This included a descriptive analysis of the three project locations, results of the [Zekiah Swamp Watershed Assessment - 2018](#), and a 2015 assessment of Poplar Hill Road. The steering committee were also provided a snapshot of what will be included in the hydrologic and hydraulic analysis at each project site. The hydrologic and hydraulic analysis will be performed at each of the three locations to determine the discharge/flows affecting the area and modeled to calculate the existing and proposed flooding condition at each location for 2050 and 2100 expected conditions.

Modeling results for 25 year and 100-year storm events for current, 2050, and 2100 expected conditions at the three project sites were presented at the September 22 steering committee meeting. Modeling data was compared to in field observations to identify areas of high risk for each site. Modeled results provided the following results:

Old Washington Road and Pembroke Square

- Poor channel conveyance and undersized pipe under Old Washington Road (24" CMP) backing up over the roadway
- Insufficient drainage to capture overflow in parking lot at the low points

Industrial Park Drive And Post Office Road Intersection

- Flooding occurring at roadway inlets J4 and J7 (Industrial Drive) due to capacity issues
- Flooding also occurring at J1 (18" HDPE) under industrial park Drive

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

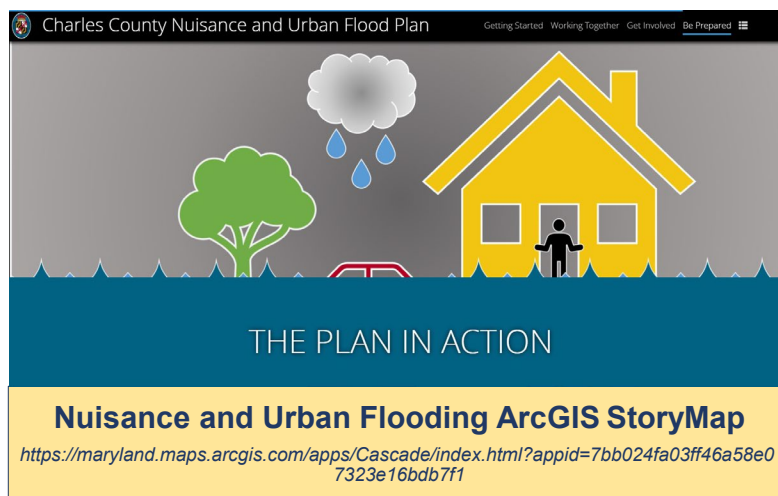
- Overtopping at low point of roadway crossing
- 0-2' of depth over the roadway for all events

During the November 29 steering committee meeting members were presented 5 alternatives and cost estimates for each project location. Alternatives were developed using 25 year and 100-year storm events for current, 2050, and 2100 expected conditions. Selected alternatives were presented to the steering committee to review and approve.

Comments from the November 29 meeting were compiled and taken into consideration in the final design and presentation of the Zekiah Watershed Urban Flood Analysis Hydraulic and Hydrology Report. The report findings and preferred proposed alternatives were presented to the steering committee during the January 20 meeting.

Community Outreach and Project StoryMap

General project information will be conveyed through the County's social media, press releases, and updates to the Nuisance & Urban Flooding Plan ArcGIS StoryMap which will be a major communication vehicle for this and future watershed studies. The StoryMap that was developed for the Nuisance Flood Plan will be modified to include details and results of the Zekiah Urban Watershed Study. This web-based application will continue to enable users to acquire information and engage in project development.



Section 3 – Target Urban Flood Locations within Zekiah Watershed



1. Old Washington Road and Pembroke Square

Old Washington Road and Pembroke Square flood due to stormwater issues and impervious surface. A tributary to the Piney Branch may also be a possible flood source. Conveyance is poor across MD 925 Old Washington Rd and downstream that leads to backups and topping of swale.

The intersection of Old Washington Road and Shoppers World experience severe flooding caused by poor stormwater conveyance, undersized drainage, and large amounts of impervious surface from parking lots, roof runoff, and loading zones. There are three inlets located at the back of the parking lot that collect runoff from Old Washington Road, roof runoff from the shopping center, and impervious runoff from the truck loading zone. Two of these inlets are shallow and are located at the low point of the parking lot. During storm events, these inlets quickly become inundated and clogged with trash and debris. The outfall pipe that conveys these inlets to the front of the shopping center is recessed and no longer performing as it was designed.

The front of the shopping center contains mostly old, corrugated metal pipes (CMP) that are nearing the end of their service life. The residential area located southeast, upstream of the shopping center drains to a ditch which connects to the 24" CMP that transverses Old Washington Road. This 24" CMP empties into a series of conveyance ditches which are located adjacent to the shopping center. These conveyance ditches are inundated with trash and debris and have poor conveyance caused by cross sectional loss, gullies, erosion, and reverse slopes and the 24" CMP does not meet the capacity to convey the residential drainage area. Additionally, the 36" CMP that conveys these drainage ditches has a negative slope, contributing to backwater and ponding upstream.

This poor conveyance leaves Old Washington Road and the surrounding low-lying areas particularly vulnerable to flooding. The residential area, Shoppers World, and a few adjacent businesses all convey stormwater to the basin adjacent to Rt. 301 which eventually drains to an unnamed tributary (UNT) to Piney Branch.





2. Industrial Park Drive and Post Office Road Intersection

Unnamed tributary enters a culvert north of Post Office Road and exits into channel north of the Southern MD Workforce Services property. Dense urban area associated with MD 301 up-stream leads to high volumes of runoff during rain events. Excessive flows will typically top the culvert on the north side of Post Office Drive and flood the intersection and then discharge into the channel on the south side. Also, a large controlled SWMP is located upstream. Note: This may be related to site #10, Piney Branch Wetland.

The intersection of Industrial Park Dr. and Post office Rd. experience severe flooding caused by poor stormwater conveyance, undersized drainage, and large amounts of runoff from increased development located upstream of the site. The dense urban area associated with MD 301 up-stream leads to high volumes of runoff during rain events. Excessive flows will typically top the culvert on the north side of Post Office Drive and flood the intersection and then discharge into the channel on the south side.

There is a 60" RCP culvert that extends under the intersection and conveys an unnamed tributary to Zekiah Swamp Run. There are four inlets located at this intersection that collect runoff from the roadway and convey it into the culvert. A 24" high density polyethylene (HDPE) pipe conveys runoff from the wooded area located southeast of the intersection towards a shallow ditch which is carried to the unnamed tributary by a crushed 18" CMP.

The site was free of and trash, debris, or blockages and scour and erosion were not identified. The overall system slope from the upstream headwall to the downstream is negative, which may be contributing to backwater affects and ponding upstream. The flooding upstream of the culvert may also indicate that the system does not meet the required design capacity.





3. Poplar Hill Road between Peters Church Road & Mattawoman and Beantown Road

The low point of Poplar Hill Rd. between St. Peters Church Rd. and Mattawoman Beantown Rd. experiences overtopping during larger storm events. Two 60" CMP culverts located near the low point of the roadway convey an unnamed tributary to Zekiah Swamp Run. These culverts are both deformed, and one culvert is almost completely crushed towards the downstream outlet point. Closer to the low point of the roadway is a 22" HDPE that was added to increase conveyance of flow under Poplar Hill Rd. however, the roadway is still experiencing overtopping during large events. Neither the upstream nor downstream end of the twin culverts contain headwall structures.

The upstream end of the culvert shows minimal signs of erosion or scour, but large debris was noted during inspection. The downstream end of the culverts spill into a large, scoured area located a couple of feet below the invert of the culverts. This scour hole is disconnected from the downstream end of the stream causing poor conveyance. The proximity of the scour hole has begun to undermine the culverts and may cause instability of the roadway embankment.



Existing drainage condition maps and stormwater inventory maps for each location can be found in Attachment 4.

Section 4 - Modeling Methodology

Hydrology

All three sites are located within the Zekiah Watershed. Drainage areas were developed for each site. Soil information was obtained using NRCS Web Soils Survey and land use information was obtained from the impervious cover data and the NLCD land use layer. Drainage area, soils, and land use information can be found in Attachment 5.

Six storm events were investigated as part of this analysis. These events include the 25-year 24-hour storm frequency, the 100-year 24-hour storm frequency, and the future projected land use conditions for each event for the years 2050 and 2100. Current rainfall data was obtained using NOAA Atlas 14 for Charles County. Future rainfall conditions were obtained using the RAND Corporation climate projections for Charles County, which incorporate regional atmospheric and topographic variability. High air emission scenarios were used (RCP 8.5) as a conservative approach. Table 1 summarizes the total precipitation for each event.

Table 1: Precipitation Volume

Scenario	Precipitation (In.)
25yr	6.31
25yr + 2050 Prediction	7.07
25yr + 2100 Prediction	7.51
100yr	8.70
100yr + 2050 Prediction	10.01
100yr + 2100 Prediction	10.53

A Type II rainfall distribution was utilized for each site. Site locations 10 and 12 hydrology was done in SWMM in conjunction with the hydraulic modeling. Site location 24 flows were developed using Hydrographs 2004 and are summarized in Table 2.

Table 2: Location 24 Peak Flows

Scenario	Peak Flow (Cfs)
25yr	281
25yr + 2050 Prediction	339
25yr + 2100 Prediction	374
100yr	469
100yr + 2050 Prediction	578
100yr + 2100 Prediction	622

Hydrologic parameters can be found in Attachment 5

Hydraulics

A stormwater analysis was conducted to determine if the existing drainage system is up to design standards and evaluate the most critical locations within the system. The Environmental Protection Agencies (EPA) Stormwater Management Model (SWMM) version 5.2 was used to model the existing conditions and the proposed preferred alternative (PPA) for Locations 10 and 12. SWMM is

used for analyses related to stormwater runoff, combined systems, and other drainage systems. It is a free software and is very effective for evaluating green/grey hybrid stormwater systems.

The existing hydraulic computations and PPA for Location 24 were performed using a 1-D steady state HEC-RAS (Version 6.2) analysis. HEC-RAS is a standard step backwater hydraulic model that utilizes site specific geometric cross section data of the stream and floodplain analysis to establish the stream hydraulics.

Section 5: Site Evaluation & Proposed Alternatives for Old Washington Road and Pembroke Square

Site Evaluation

A series of conduit, junction, and storage area connections were used to model the shopping area and associated drainage. Inlets, manholes, and basins were modeled using storage areas based on the area/depth relationship. Pipes and conveyance ditches were modeled utilizing conduit connections and junctions were used at the confluences of these connections and at headwalls.

The existing model was used to identify the most inundated drainage feature within the project area. This included the 24" CMP that transverses Old Washington Rd conveying runoff from the residential area and the two inlets located at the low point in the rear truck loading zone behind Shoppers World. These features were analyzed in addition to basin elevation located downstream and the outfall to Piney Branch UNT. The existing and PPA output is summarized in Tables 3- 5.



Table 3: IN-3 Summary Table (Low Point Inlet)

Storm Event	Existing Node Inflow (Cfs)	Existing Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	30.40	4.39	17.45	3.74
25-Year (2050)	34.39	4.46	19.08	3.79
25-Year (2100)	36.78	4.50	19.67	3.81
100-Year	43.26	4.60	20.79	3.84
100-Year (2050)	50.57	4.70	20.84	3.84
100-Year (2100)	53.58	4.74	20.74	3.84

Table 4: Existing Basin Summary Table

Storm Event	Existing Node Inflow (Cfs)	Existing Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	145.41	3.16	140.54	3.06
25-Year (2050)	151.79	3.30	148.54	3.20
25-Year (2100)	155.94	3.46	151.05	3.28

100-Year	165.62	3.72	160.83	3.59
100-Year (2050)	170.94	3.92	167.30	3.78
100-Year (2100)	172.62	4.02	170.40	3.86

Table 5: OUT-5 Summary Table (Outfall to Piney Branch UNT)

Storm Event	Existing Node Inflow (Cfs)	Existing Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	143.27	3.16	138.45	3.06
25-Year (2050)	148.63	3.28	145.35	3.20
25-Year (2100)	149.64	3.59	148.49	3.28
100-Year	161.61	3.68	156.15	3.64
100-Year (2050)	165.77	3.70	163.46	3.69
100-Year (2100)	165.65	3.70	165.27	3.69

The proposed output is based on an additional 14,000 ft³ of storage in the system to accommodate the increase in existing pipe capacities. Refer to Attachment 6 for the full SWMM report and model schematic and the hydrologic input parameters.

Proposed Alternatives for Old Washington Road and Pembroke Square

Proposed alternatives were developed for the Old Washington Road and Pembroke Square project location. Aside from Alternative 1 – No Build, which does not address the purpose and need, the following distinct build alternatives were developed and analyzed for the Old Washington Road and Pembroke Square project location. The final PPA selection is discussed in Section 5.

Alternative 2: Drainage system improvements

Advantages

- Promote positive drainage by upsizing and cleaning old drainage system
- Increase conveyance throughout system

Disadvantages

- May increase flooding downstream
- Roadway may still flood during large events

Alternative 3: Drainage system improvements, revert impervious area to pervious, add GI and/or underground detention

Advantages

- Promote positive drainage by upsizing and cleaning old drainage system
- Increase conveyance throughout system
- Reduce heat island effect, reduce polluted runoff downstream, and provide storage runoff reduction

Disadvantages

- Proposed GI layout will depend on the shopping center
- ROW acquisition will be required

Alternative 4: Drainage system improvements, add GI and/or underground detention

Advantages

- Promote positive drainage by upsizing and cleaning old drainage system
- Increase conveyance throughout system
- Reduce heat island effect, reduce polluted runoff downstream, and provide storage runoff reduction

Disadvantages

- Roadway may still flood during larger events
- ROW acquisition will be required

Alternative 5: Drainage system improvements, revert impervious area to pervious, add GI and/or underground detention, add pump station

Advantages

- Promote positive drainage by upsizing and cleaning old drainage system
- Increase conveyance throughout system
- Reduce heat island effect, reduce polluted runoff downstream, and provide storage runoff reduction
- Provides faster drainage and storage during larger, high intensity events

Disadvantages

- ROW acquisition will be required
- Most costly option
- Longer construction duration

Section 6: Site Evaluation & Proposed Alternatives for Industrial Park Drive and Post Office Road

Site Evaluation

Conduit and junction connections were used to model the drainage at the intersection of Industrial Park Drive and Post Office Road. Curb inlets, inlets with headwalls, pipe inlets, and downstream outfall were modeled using junctions. Pipes and streams were modeled using conduits.

Pipe dimensions and inverts were input to the model based on field survey conducted on 10/19/2022. A 60" RCP transverses Post Office Road from southwest to northeast and conveys runoff under the existing roadway from a stream inlet to Outfall 1. There are 4 open grate road inlets that connect to this existing system. There is an additional drainage system on the east side of Post Office Road consisting of a 24" HDPE pipe and 16" CMP which is partially crushed and blocked. The downstream outlet of the 16" CMP pipe could not be located and thus was assumed to connect to the 60" RCP system just upstream of Outfall 1.

The existing model was used to identify the most inundated drainage features within the project area. Multiple pipes have negative slopes, and the system inlet has a lower invert than the outlet which may contribute flooding and backwater effects at the site. Results from the existing model were analyzed to obtain maximum inflow and maximum water depth at key features indicating the system performance.

One preferred proposed alternative (PPA) scenario was modeled. The 60" RCP drainage system was upgraded to 58" x 91" reinforced concrete elliptical pipe (RCEP) with a beveled headwall entrance and re-graded to re-establish positive pipe slopes. Beveling the entrance of the headwall reduces the entrance loss coefficient. Additional Green Infrastructure (GI) surface retention was modeled which provides an additional 10,000 ft³ of storage in the overall system. The additional drainage system on the east side of Post Office Road was graded to re-establish positive pipe slopes and the old HDPE/CMP were replaced with one 24" HDPE pipe that connects to the bioswale retention basin to reduce the load at Outfall 1 downstream. Refer to Attachment 6 for the full SWMM report and model schematic and the hydrologic input parameters. The existing and PPA output is summarized in Tables 6-8.



Table 6: J3 Summary Table (60" RCP Upstream Headwall)

Storm Event	Existing Max Total Node Inflow (Cfs)	Existing Max Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	616.53	10.70	616.53	6.55
25-Year (2050)	716.83	11.86	716.83	7.03
25-Year (2100)	776.48	12.59	776.48	7.35
100-Year	941.46	14.72	941.46	8.30
100-Year (2050)	1128.20	17.32	1128.20	9.53
100-Year (2100)	1205.48	18.44	1205.48	10.07

*Roadway elevation low point: 198'

Table 7: J4 Summary Table (Inlet at NW Corner Post Office Rd)

Storm Event	Existing Max Total Node Inflow (Cfs)	Existing Max Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	305.20	5.15	339.66	5.00
25-Year (2050)	327.90	5.15	340.03	5.00
25-Year (2100)	341.37	5.15	341.44	5.00
100-Year	378.23	5.15	373.74	5.00
100-Year (2050)	419.67	5.15	414.78	5.00
100-Year (2100)	436.69	5.15	431.72	5.00

Table 8: Out1 Summary Table (Downstream Headwall)

Storm Event	Existing Max Total Node Inflow (Cfs)	Existing Max Node Depth (Ft)	Proposed Node Inflow (Cfs)	Proposed Node Depth (Ft)
25-Year	216.86	4.08	430.05	3.75
25-Year (2050)	206.46	4.09	443.30	3.75
25-Year (2100)	207.02	4.10	428.49	3.75
100-Year	208.54	4.11	429.67	3.75
100-Year (2050)	210.17	4.12	443.36	3.75
100-Year (2100)	210.82	4.13	445.74	3.75

Increasing the capacity of the system may reduce the headwater elevation by 4-8 ft for the evaluated events. The proposed invert of the culvert is at 191.25 ft. A node depth of 6.55 ft for the 25-year event will reduce flooding from 202 ft to just below 198 ft (the low point of the roadway) for the 25-year event. The increase in flow downstream and decrease in depth indicates an increase in velocity and erosion control measures may be required downstream. This may include baffles, weirs, and scour holes to prevent erosion, scour and sedimentation downstream.

Proposed Alternatives for Industrial Park Drive and Post Office Road

Proposed alternatives were developed for the Industrial Park Drive and Post Office Road project location. Aside from Alternative 1 – No Build, which does not address the purpose and need, the following distinct build alternatives were developed and analyzed for Industrial Park Drive and Post Office Road project location. The final PPA selection is discussed in Section 5.

Alternative 2: Drainage System Improvements; replace 60" RCP with dual 48" RCP

Advantages

- Clean existing RCP pipe system and curb inlets
- Upsize pipes
- Re-establish positive pipe slopes
- Stabilize, widen, and clean streams at system inlets

Disadvantages

- Roadway may still flood during, high volume rainfall events
- Will increase flooding downstream near

Alternative 3: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP

Advantages

- Clean existing RCP pipe system and curb inlets
- Upsize pipes
- Re-establish positive pipe slopes
- Stabilize, widen, and clean streams at system inlets

Disadvantages

- Roadway may still flood during, high volume rainfall events
- Will increase flooding downstream near

Alternative 4: Drainage System Improvements; replace 60" RCP with dual 48" RCP and add Green Infrastructure

Advantages

- Clean existing RCP pipe system and curb inlets
- Upsize pipes
- Re-establish positive pipe slopes
- Stabilize, widen, and clean streams at system inlets
- Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity

Disadvantages

- Flooding may still occur in larger, high intensity events
- ROW acquisition may be required

Alternative 5: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP and add Green Infrastructure

Advantages

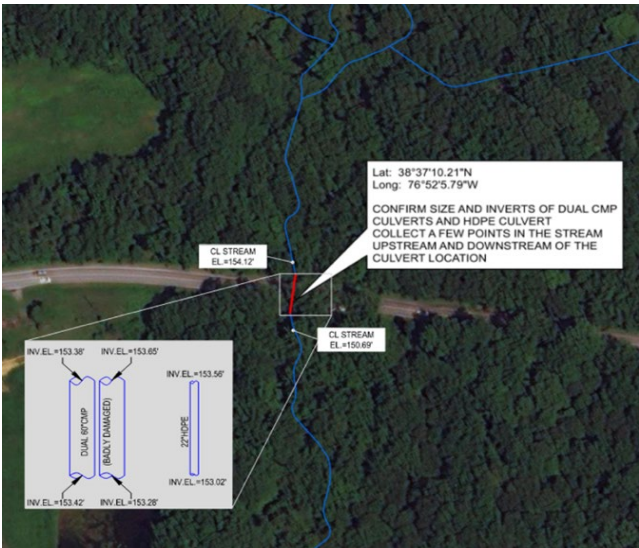
- Clean existing RCP pipe system and curb inlets
- Upsize pipes
- Re-establish positive pipe slopes
- Stabilize, widen, and clean streams at system inlets
- Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity

Disadvantages

- Flooding may still occur in larger, high intensity events
- ROW acquisition may be required

Section 7: Site Evaluations & Proposed Alternatives for Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

Site Evaluation



Cross section geometric data was derived from the NOAA 1-meter vertical accuracy DEM data using RASMapper. The existing culvert dimensions were obtained from survey. The HEC-RAS model was run using the design event peak flow rate, for each of the analyzed storm events. Peak flows were obtained using Hydrographs 2004 software. Normal depth was used as the downstream boundary condition.

Table 9 summarizes the existing and PPA WSEL just upstream of the culvert location.

Table 9: Existing and Proposed WSEL Upstream of Poplar Rd.

Storm Event	Existing Wsel (Ft)	Proposed Wsel (Ft)
25-Year	159.14	157.75
25-Year (2050)	159.33	158.26
25-Year (2100)	159.46	158.55
100-Year	159.75	159.31
100-Year (2050)	160.01	159.53
100-Year (2100)	160.10	159.64

*Roadway Elevation Low Point: 158.7'

Refer to Attachment 5 and 6 for the complete hydrologic and hydraulic backup data, respectively.

Proposed Alternatives for Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

Proposed alternatives were developed for the Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road project location. Aside from Alternative 1 – No Build, which does not address the purpose and need, the following distinct build alternatives were developed and analyzed for Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road project location. The final PPA selection is discussed in Section 5.

Alternative 2: Replace dual 60" CMPs with dual 60" RCP and stream restoration

Advantages

- Promote positive drainage by upsizing old drainage system
- Increase conveyance along the stream through restoration and debris removal
- Reduce scour and erosion by stabilizing stream banks and outfalls

Disadvantages

- Roadway will still flood during 25-year event

Alternative 3: Replace dual 60" CMPs with dual 60" RCP, raise the low point of the roadway, and perform stream restoration

Advantages

- Promote positive drainage by upsizing old drainage system
- Increase conveyance along the stream through restoration and debris removal
- Reduce scour and erosion by stabilizing stream banks and outfalls

Disadvantages

- Most costly option with the longest construction duration
- The roadway will need to be a couple of feet to meet 25-year capacity
- Longer construction duration
-

Alternative 4: Replace dual 60" CMPs with dual 72" RCP (beveled entrance), replace 22" HDPE with 36" HDPE and stream restoration

Advantages

- Promote positive drainage by upsizing old drainage system
- Increase conveyance along the stream through restoration and debris removal
- Reduce scour and erosion by stabilizing stream banks and outfalls

Disadvantages

- Roadway will still flood during future, high volume rainfall events (100 Year)

Alternative 5: Replace dual 60" CMPs with single 10' x 5' reinforced concrete box culvert and stream restoration

Advantages

Promote positive drainage by upsizing old drainage system

Increase conveyance along the stream through restoration and debris removal

Reduce scour and erosion by stabilizing stream banks and outfalls

Disadvantages

Roadway will still flood during 25-year event

A comparison matrix of the developed alternatives, along with a no-build alternative, is available in Attachment 7.

Section 8: Concept Development Recommendations for Target Urban Flood Locations within Zekiah Watershed

The recommended PPA addresses the established purpose and need. Further coordination will be made with local officials to provide feedback on the selected PPA. No fatal flaws have been identified with the PPA.

1. Old Washington Road and Pembroke Square

The recommended PPA is Alternative 3, which includes drainage system improvements, reverting impervious area to pervious in the rear lot, and adding GI and/or underground detention to provide additional storage.



2. Industrial Park Drive and Post Office Road Intersection

The recommended PPA is Alternative 5, which includes drainage system improvements, replacing the 60" RCP run with a 58" x 91" RCEP and adding GI in the form of surface retention/infiltration.

3. Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

The recommended PPA is Alternative 4, which includes the replacement of the dual 60" CMP culverts with dual 72" RCP culverts with beveled entrances at the headwall. The existing 22" HDPE adjacent to the dual culverts will be upsized with a 36" HDPE pipe. The channel will be cleaned, stabilized, and cleared of debris and the downstream channel will be re-graded to promote better conveyance.

Attachment 1

STEERING COMMITTEE MEETINGS





Zekiah Watershed Study Project Site Review & Consideration

August 25, 2022
Virtual

1

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Zekiah Watershed Study Project Site Review & Consideration

August 25, 2022
Virtual

2

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Agenda

- Project Update
 - Schedule
 - Stakeholder Involvement
 - Outreach and StoryMap
- Relevant Data & Resources
 - Nuisance Flood Plan
 - Poplar Hill Evaluation
 - Zekiah Watershed Assessment
- Field Study Findings & Recommendations Discussion
- Next Steps

3

Urban Flood Analysis

Zekiah Watershed

February 2023



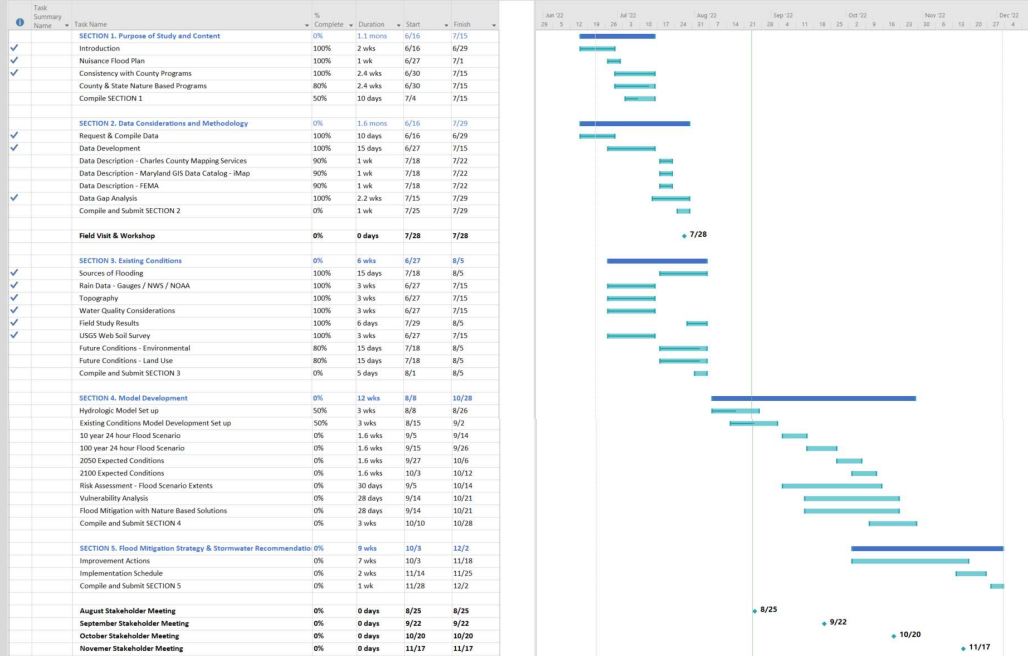
CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Project Update

4

Project Schedule



5

Other Items to Address

- Stakeholder Involvement
- Members and Involvement
- Document Format
- Outreach & StoryMap

Section 1: Purpose and Study Area

Charles County, Maryland is experiencing flooding outside mapped floodplains with increasing frequency, including both nuisance and urban flooding. Nuisance flooding is associated with high tides that flow back through the stormwater system, increasing raising the level of groundwater, and overtopping the banks and edge of waterways. Nuisance flooding is an indicator of rising water levels in the Chesapeake Bay and its tributaries. Areas that were previously dry now flood during high tides because the water elevation is high enough to lap over the banks of waterways and to enter stormwater systems through outfalls that were previously high enough to prevent backflow, while allowing outflow. Urban flooding is due to a variety of issues related to development. Increased impervious surface, disruption of natural watershed flow and functions, undersized and aged stormwater infrastructure, and changing weather patterns which exacerbate the inadequacies of older stormwater systems and the fragmented watersheds. Urban flooding reflects decades of development that has outstripped the capacity of stormwater infrastructure and disrupted the natural flow and discharge of watersheds. Additionally, many stormwater systems are beyond their expected useful life and in need of repair and replacement.

To further explore these challenges, forty-eight locations were identified and prioritized for additional analysis and flood risk reduction solutions were identified in the 2020 CHARLES COUNTY NUISANCE & URBAN FLOOD PLAN. Three of the identified locations are within the Zekiah Watershed have been targeted for further analysis.

1. Industrial Park Drive and Post Office Road Intersection

Unnamed tributary enters a culvert north of Post Office Road and exits into channel north of the Southern MD Workforce Services property. Dense urban area associated with MD 301 up-stream leads to high volumes of runoff during rain events. Excessive runoff will typically lap the culvert on the north side of Post Office Drive and flood the intersection and then discharge into the channel on the south side. Also, a large combined DSWP is located upstream. Note: This may be related to site #10, Piney Branch Wetland.

2. Old Washington Road and Pembroke Square

Old Washington Road and Pembroke Square flood due to stormwater issues and impervious surface. A tributary to the Piney Branch may also be a possible flood source. Conveyance is poor across MD 925 Old Washington Rd and downstream that leads to backups and topping of swale.

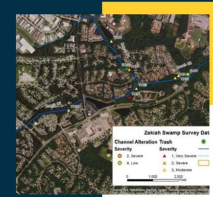
3. Poplar Hill Road between Puters Church Road & Mattawoman and Pleasantown Road

Low section in the road with a culvert running under roadway. Stormwater issues cause roadway flooding.

Urban Flood Analysis

Zekiah Watershed

December 2022



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

6

Urban Flood Analysis

Zekiah Watershed

February 2023

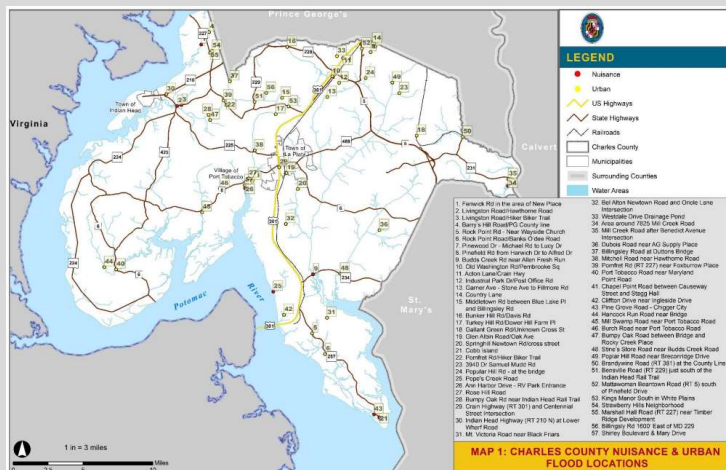


CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Relevant Data & Resources

7



Data gathering process:

- Flood event data was obtained from the National Center for Environmental Information (NCEI) and reviewed to aid in the determination of nuisance and urban flood locations.
- Additional information gathered by the Department of Emergency Services of known flood areas resulted in a listing of roadways and intersections. This listing was used to develop a flood location map.
- Twenty-seven nuisance and urban flood locations were identified. Additional information gathered during the flood identification site visits included a description per site and a site photograph.
- During the Nuisance and Urban Flooding Stakeholder Group held on February 20, 2020. In addition to reviewing and updating of the initial identified flood locations, the stakeholders in attendance identified twenty new flood locations, sites 28 thru 48

Nuisance Flood Plan

8

Old Washington Road and Pembroke Square



- Environmental restrictions are limited factors in this area in terms of projects
- Possibility of using stormwater as grey water and pumping to power plant

Description:

- Old Washington Road and Pembroke Square flood due to stormwater issues and impervious surface. A tributary to the Piney Branch may also be a possible flood source. Conveyance is poor across MD 925 Old Washington Rd and downstream that leads to backups and topping of swale. (Wetland-Piney Branch)

9

Industrial Park Drive and Post Office Rd Intersection



- Evaluate Drain System
- Drainage Improvement Plan

Description:

- Unnamed tributary enters a culvert north of Post Office Road and exits into channel north of the Southern MD Workforce Services property. Dense urban area associated with MD 301 up-stream leads to high volumes of runoff during rain events. Excessive flows will typically top the culvert on the north side of Post Office Drive and flood the intersection and then discharge into the channel on the south side. Also, a large controlled SWMP is located upstream. Note: This may be related to site #10, Piney Branch Wetland.

10

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road



- Culvert replacement project
- Have County SWM engineer review to see if larger pipe is necessary

Description:

- Low section in the road with a culvert running under roadway. Stormwater issues cause roadway flooding.

11

Poplar Hill Road 2015 Evaluation

Project SR-04 - Problem

- 320 foot section of stream that flows from a culvert under Poplar Hill Road.
- Culvert is undermined and the concrete apron is broken with a 1 ½ foot drop to the existing channel invert.
- The culvert appears to be undersized for the drainage area. The channel is a Rosgen G Type channel and is incised with no access to a floodplain.
- Undercut roots are compromising trees which will eventually fall into the channel causing debris jams.
- Bank height decreases as the channel gets closer to its confluence with the main channel.

Solution \$240,000

- Repair the broken concrete apron, installing flowable fill underneath the undercut apron, installing a plunge pool to dissipate velocity, and grading back the banks to allow access to a floodplain. Grade control structures are proposed to prevent down cutting and maintain grade.

Constraints

- H&H Study needed
- Potential Environmental Impacts
- Soil Erosion / Sediment Control Measures and Permitting
- The property is situated on two parcels both owned by Archbishop Patrick O'Boyle of St. Peters Church.

12

Zekiah Swamp Watershed Assessment Analysis

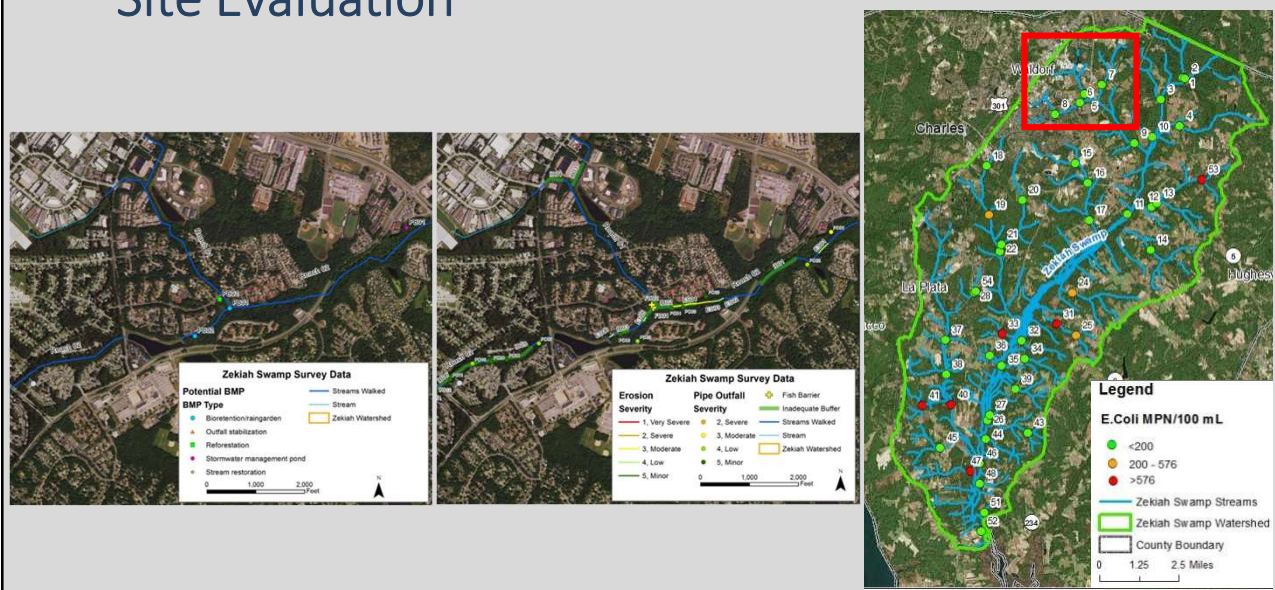
- The primary goal of Zekiah Swamp Watershed Assessment is related to the urban stormwater sector and meeting the restoration goals of the NPDES permit that satisfy section IV.E.1,
- Synoptic water quality sampling was performed across the Zekiah Swamp watershed from April 22-29, 2016. A total of 54 sites were visited for water quality and discharge measurements:

Station	Date	Area (AC)	Discharge(cfs)	Temperature	pH	Dissolved Oxygen(mg/L)	Specific Conductance	Turbidity (NTU)	Optical Brightener (ppm)
ZE-5	3/16/2016	1779.2	0.93	10.3	6.69	10.40	236.4	10.40	1.98
ZE-6	3/16/2016	4524.5	1.76	15.9	7.23	13.44	358.5	4.12	1.21
ZE-7	3/16/2016	1779.2	1.14	9.8	5.98	11.42	156.9	8.01	1.95
ZE-8	3/17/2016	647.4	0.96	16.7	6.56	9.80	347.1	12.50	1.48

Station	Ortho P(mg/L)	TKN (Mg/L)	Nitrate/Nitrite (mg/L)	Total Nitrogen (mg/L)	Total Phosphorus (mg/L)	E. Coli (mg/100 mL)	Ortho P (kg/H/day)	TKN (kg/H/day)	Nitrate Nitrite (kg/H/day)	Total Nitrogen (kg/H/day)	Total Phosphorus (kg/H/day)
ZE-5	0.005	0.25	0.6	0.8	0.02	35	0.00002	0.00079	0.00190	0.00253	0.00006
ZE-6	0.005	0.25	0.15	0.4	0.01	62.7	0.00001	0.00059	0.00035	0.00094	0.00002
ZE-7	0.005	0.25	1.3	1.3	0.005	72.7	0.00002	0.00097	0.00502	0.00502	0.00002
ZE-8	0.080	0.25	0.15	0.4	0.05	8.6	0.00072	0.00225	0.00135	0.00360	0.00045

13

Zekiah Swamp Watershed Assessment Site Evaluation



14

Zekiah Swamp Watershed Assessment Recommendations SWM BMP

Site ID	Existing Conditions	Proposed Improvements
ZE_SR_1	Stream located downstream from development in Waldorf and residential neighborhoods. Channel widened with localized areas of severe bank erosion.	Stream bank and bed stabilization to repair bank erosion.
ZE_BMP_1	Upstream water from residential area is collected through inlet and drains to this outfall grass channel, it eventually drains to the adjacent stream.	Bioretention
ZE_BMP_2	Outfall drains to riprap and storm drain into a stream. Drainage area includes almost the entire community.	Bioretention

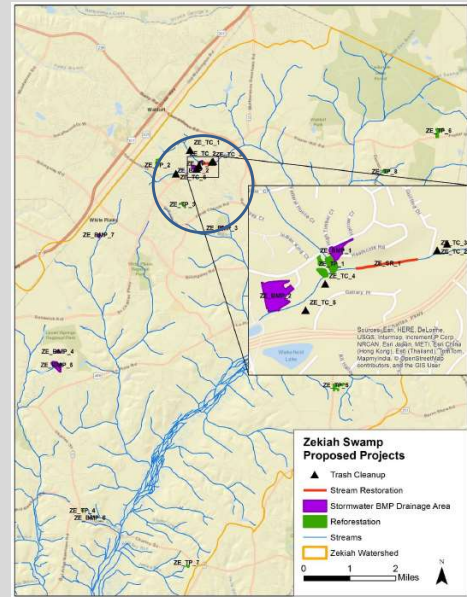


FIGURE 16: LOCATION OF ZEKIAH SWAMP WATERSHED POTENTIAL WATER QUALITY IMPROVEMENT PROJECTS

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Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Field Study Findings & Recommendations Discussion

16

Old Washington Road and Pembroke Square

Known Issues:

- Significant flooding in entire parking lot and surrounding roadways
- Poor flow conveyance to downstream culverts

Observed:

- Only two shallow inlets in rear parking area at the low point
- Trash /debris sediment accumulation at the inlets
- Parking lot and drainage system are flat
- Streams/ditches adjacent to parking area have minimal conveyance (stagnant)
- Downstream culverts look clear but likely aren't getting enough flow
- Some overgrowth in the culvert area

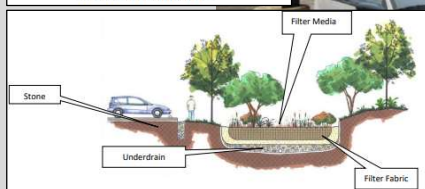
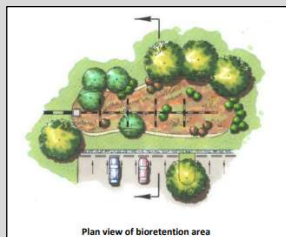


17

Old Washington Road and Pembroke Square

Potential Recommendations:

- (ROW to be considered) Grade parking area
- Regrades ditches and stabilize to convey flow
- Resize pipes as feasible and pitch to convey positive flow
- Consider providing green infrastructure/stormwater storage in unused portions of parking area (pending ROW)



18

Industrial Park Drive and Post Office Rd Intersection

Known Issues:

- Flooding at Intersection

Observed:

- Culvert at low point appears clear.
- Large drainage area believed to drain to low point. Potentially coming from surrounding new development and upstream.
- No significant erosion apparent
- Capacity of system is likely large part of this issue

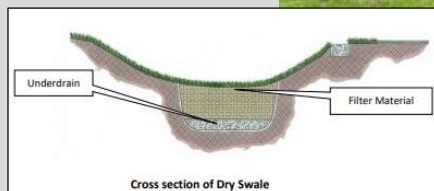
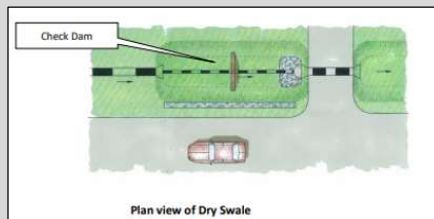


19

Industrial Park Drive and Post Office Rd Intersection

Potential Recommendations:

- Investigate increasing capacity of existing culvert and adjacent drainage system
- Provide storage by adding a basin on downstream culvert at intersection
- Add rip rap and grade off the roadway with curb open to allow flow over rip rap to basin



20

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

Known Issues:

- Flooding at low point of roadway

Observed:

- 2 culvert crossings identified near low point
- New culvert (1 HDPE pipe) located at the roadway low point
 - Large riprap scour hole causing ponding and obstruction of flow
 - Upstream end is overgrowth
- Original culvert (2 CMP pipes) both deformed but one crushed on downstream outlet
 - Downstream area is disconnected from the stream
 - Tree obstruction noted at the upstream end



21

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

Potential Recommendations

- Replace CMP pipes
- Clear vegetation and remove tree blocking
- Considering additional slope stabilization and gabion on side slopes
- Channelize both downstream ends to flow to downstream ditch



22

Zekiah Swamp Watershed Assessment Hydrologic and Hydraulic Analysis

Hydrologic Analysis

The sources of flooding will be identified, and a hydrologic analysis will be performed at each of the three locations to determine the discharge/flows affecting the area. The analysis will include:

- The 25-Year 24-Hour storm frequency (design storm)
- The 100-Year 24-Hour storm frequency
- Future land-use and environmental conditions

Hydraulic Analysis

The modeled discharges will be input into hydraulic models to calculate the existing and proposed flooding condition at each location, including mitigation tactics. The analysis will include:

- 25-Year 24-Hour scenario
- 100-Year 24-Hour scenario
- 2050 Expected Conditions
- 2100 Expected Conditions
- Risk Assessment and Vulnerability Analysis
- Infrastructure upgrades as well as Green Infrastructure will be taken into account

23

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Next Steps

- Hydraulic Analysis For Flood Scenarios
- Hydrologic Analysis For Flood Scenarios
- Risk Assessment For Each Flood Scenario
- Hold Steering Committee Meeting to Present Findings of Each Flood Scenario
- Refine Improvement Actions & Develop Implementation Schedule
- Modify StoryMap to Include Methodology & Findings of Study
- Compile Findings in Report and Present to County for Approval

24

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Zekiah Watershed Study Model Development

September 22, 2022

Virtual

1

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Agenda

- Project Update
 - Schedule
 - StoryMap
- Relevant Data & Resources
 - Nuisance Flood Plan
 - Poplar Hill Evaluation
 - Zekiah Watershed Assessment
- Field Study Findings & Recommendations Discussion
- Next Steps

2

Urban Flood Analysis Zekiah Watershed

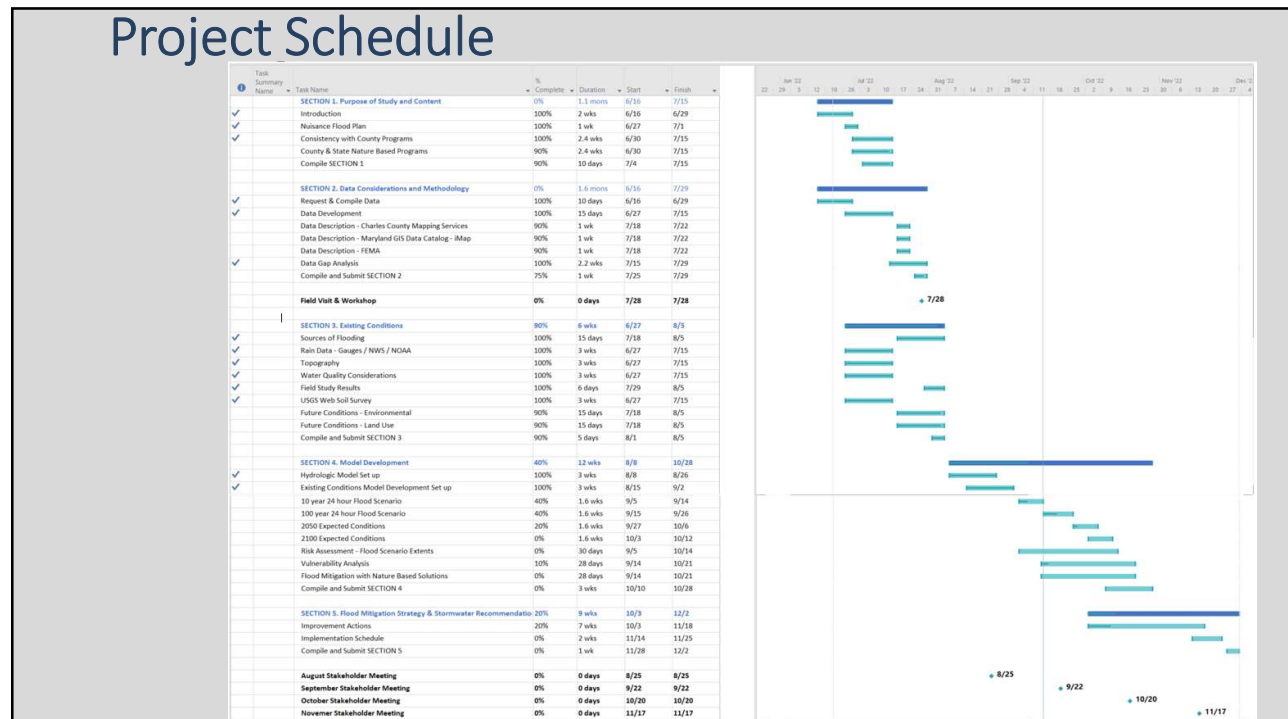
February 2023

CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Project Update

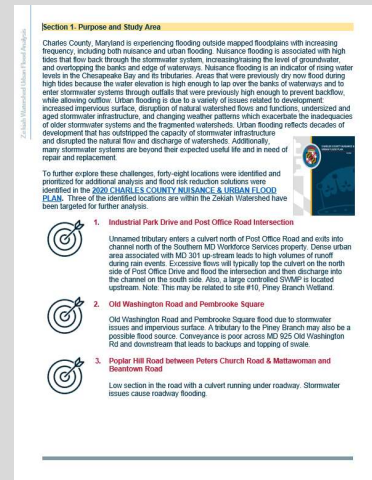
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4

Other Items to Address

- Document Progress
- Outreach & StoryMap
- Methodology and Findings



5

Urban Flood Analysis

Zekiah Watershed

February 2023

CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

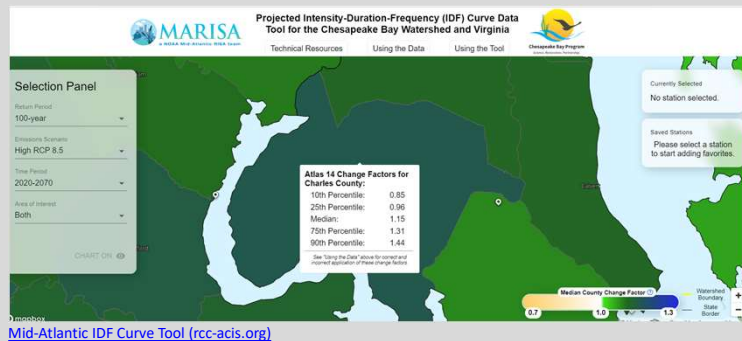
Model Updates

6

Precipitation Data for Charles County

Storm Event	Atlas 14 Precip. (in.)	% Change for 2050	Projected Precip. 2050 (in.)	% Change for 2100	Projected Precip. (2100) (in.)
25 year	6.31	12	7.07	19	7.51
100 year	8.70	15	10.01	21	10.53

• Table developed using Maryland's Stormwater Management Climate Change Action Plan (A-StoRM) [A-StoRMreport.pdf \(maryland.gov\)](#)



7

Old Washington Road and Shoppers World (Previously Pembroke Square)



• Hydrology

- HEC-HMS used to obtain Type II rainfall distribution for each event (six events total) to model in SWMM.

• EPA's Stormwater Management Model (SWMM) Version 5.2

- Curve Number Method
- Subcatchment flow directed to inlets, conduits, and streams/ditches
- Proposed BMPs will be modeled as storage units or LID controls

• Risk Assessment

- Poor channel conveyance and undersized pipe under Old Washington Road (24" CMP) backing up over the roadway
- Insufficient drainage to capture overflow in parking lot at the low points

8

Industrial Park Drive and Post Office Rd Intersection



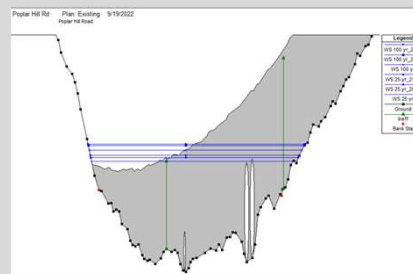
- **Hydrology**
 - HEC-HMS used to obtain Type II rainfall distribution for each event (six events total) to model in SWMM.
- **EPA's Stormwater Management Model (SWMM) Version 5.2**
 - Curve Number Method
 - Subcatchment flow directed to inlets, conduits, and streams
 - Proposed BMPs will be modeled as storage units or LID controls
- **Risk Assessment**
 - Flooding occurring at roadway inlets J4 and J7 (Industrial Drive) due to capacity issues
 - Flooding also occurring at J1 (18" HDPE) under industrial park Drive

9

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road



- **Hydrology**
 - Hydrographs 2004 used to obtain flow data for each event (six events total)
- **Hydraulics**
 - HEC-RAS Version 6.2 (1-D Steady State)
 - Both CMP and HDPE culverts are modeled
- **Risk Assessment**
 - Overtopping at low point of roadway crossing
 - 0-2' of depth over the roadway for all events



10

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Next Steps

- Hold Steering Committee Meeting to Present Vulnerability Analysis
- Refine Improvement Actions & Develop Implementation Schedule
- Modify StoryMap to Include Methodology & Findings of Study
 - Types of BMPs
 - Proposed pipe sizes
 - Channel/Ditch Restoration
 - Design Storm feasible to address flooding
 - Current design storm ~25 year
- Compile Findings in Report and Present to County for Approval

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Zekiah Watershed Study

Current and Future Conditions

November 29, 2022

Virtual

1

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Agenda

- Project Update
 - Schedule
 - StoryMap
- Model Updates
- Next Steps

2

Urban Flood Analysis

Zekiah Watershed

February 2023

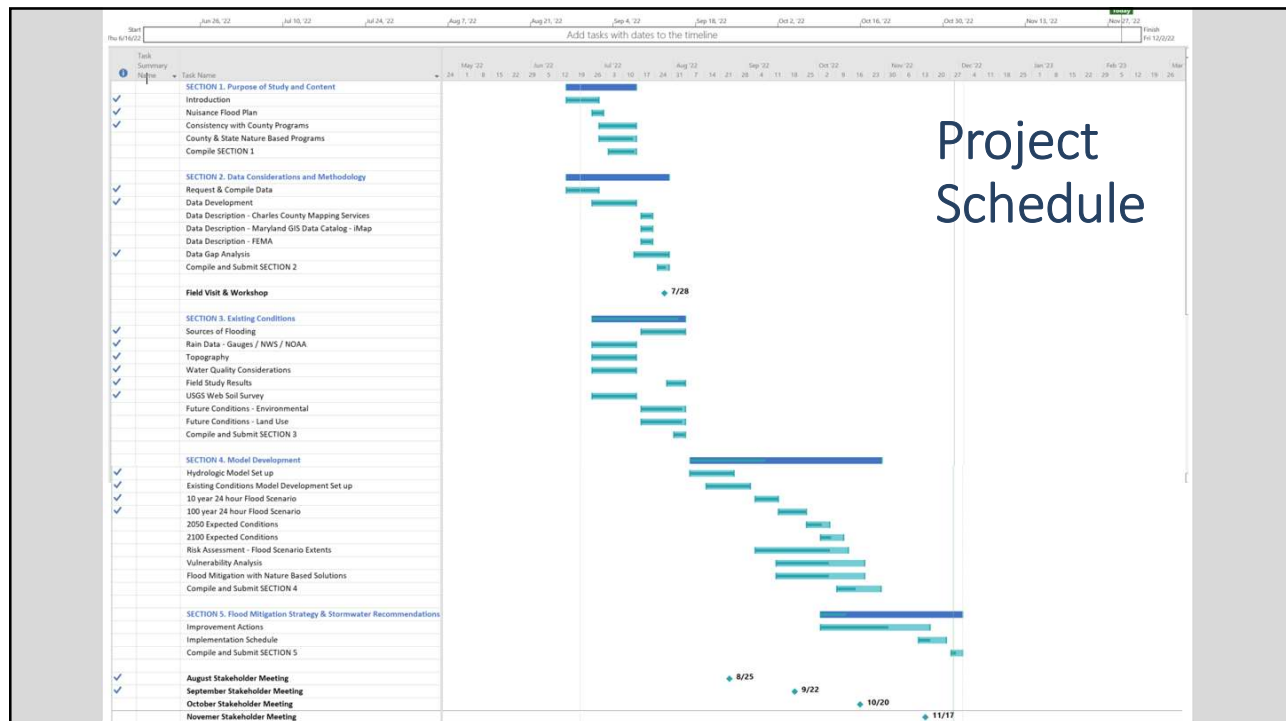


CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Project Update

3



4

Other Items to Address

StoryMap - Include Methodology & Findings of Study

- Types of BMPs
- Proposed pipe sizes
- Channel/Ditch Restoration
- Design Storm feasible to address flooding
- Current design storm ~25 year

5

Urban Flood Analysis

Zekiah Watershed

February 2023



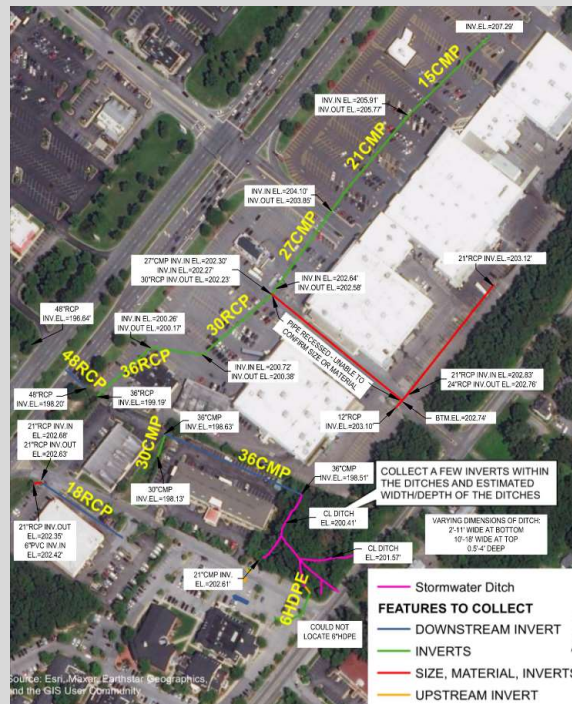
CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Model Updates

6

Old Washington Road and Shoppers World (Previously Pembroke Square)



7

Old Washington Road and Shoppers World



- Alternative
 - Alternative 1: No Build
 - Does not address project need
 - Alternative 2: Drainage System Improvements
 - Upsizing to meet the 25 year will flood out the basin downstream
 - **Alternative 3: Drainage System Improvements, restore portion of lot to pervious, add GI and/or underground Detention**
 - Replace corroded CMP with RCP/HDPE
 - Addresses the 25-year current and future conditions, will not flood basin
 - Alternative 4: Drainage System Improvements, Add GI and/or Underground Detention
 - Addresses the 25-year current and future conditions, will not flood basin
 - Alternative 5: Drainage System Improvements, Add GI, and Install Pump Station
 - Addresses the 25-year current and future conditions, most costly option, will not flood basin
- Cost Estimates
 - Alternative 1: N/A
 - Alternative 2: \$1,170,000
 - **Alternative 3: \$1,480,000**
 - Alternative 4: \$1,450,000
 - Alternative 5: \$1,940,000

8

Old Washington Road and Shoppers World

- Model Results

Inlet at low point of Lot

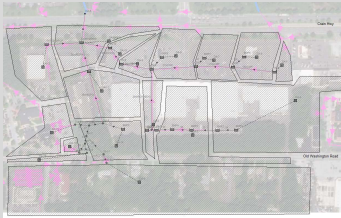
Storm Event	Existing Node Inflow (cfs)	Existing Node Depth (ft)	Proposed Node Inflow (cfs)	Proposed Node Depth (ft)
25-Year	30.40	4.39	17.45	3.74
25-Year (2050)	34.39	4.46	19.08	3.79
25-Year (2100)	36.78	4.50	19.67	3.81
100-Year	43.26	4.60	20.79	3.84
100-Year (2050)	50.57	4.70	20.84	3.84
100-Year (2100)	53.58	4.74	20.74	3.84

Existing Basin

Storm Event	Existing Node Inflow (cfs)	Existing Node Depth (ft)	Proposed Node Inflow (cfs)	Proposed Node Depth (ft)
25-Year	145.41	3.16	140.54	3.06
25-Year (2050)	151.79	3.30	148.54	3.20
25-Year (2100)	155.94	3.46	151.05	3.28
100-Year	165.62	3.72	160.83	3.59
100-Year (2050)	170.94	3.92	167.30	3.78
100-Year (2100)	172.62	4.02	170.40	3.86

Outfall to Piney Branch

Storm Event	Existing Node Inflow (cfs)	Existing Node Depth (ft)	Proposed Node Inflow (cfs)	Proposed Node Depth (ft)
25-Year	143.27	3.16	138.45	3.06
25-Year (2050)	148.63	3.28	145.35	3.20
25-Year (2100)	149.64	3.59	148.49	3.28
100-Year	161.61	3.68	156.15	3.64
100-Year (2050)	165.77	3.70	163.46	3.69
100-Year (2100)	165.65	3.70	165.27	3.69



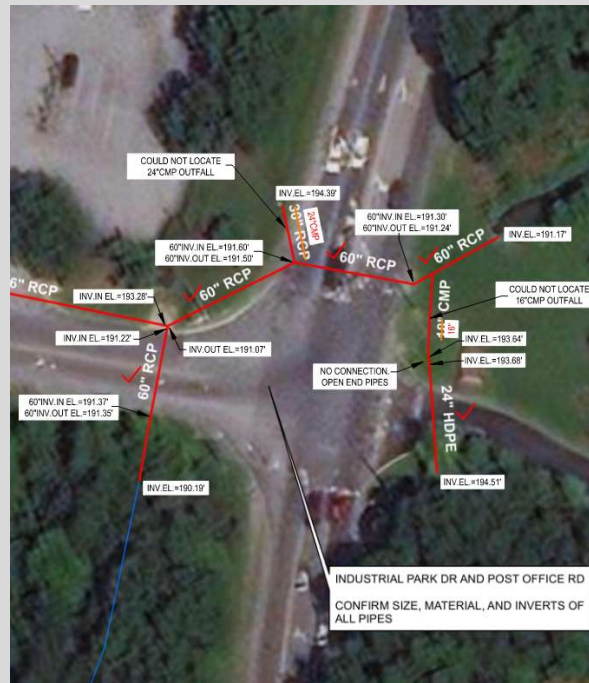
9

Old Washington Road and Shoppers World



10

Industrial Park Drive and Post Office Rd Intersection



11

Industrial Park Drive and Post Office Rd Intersection



- **Alternative**
 - Alternative 1: No Build
 - Does not address project need
 - Alternative 2: Drainage System Improvements; replace 60" RCP with dual 48" RCP
 - Will Increase downstream flooding
 - Alternative 3: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP
 - Will Increase downstream flooding
 - Alternative 4: Drainage System Improvements; replace 60" RCP with dual 48" RCP and add GI
 - Addresses the 25-year current and future conditions, will help mitigate downstream flooding
 - **Alternative 5: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP and add GI**
 - Addresses the 25-year current and future conditions, will help mitigate downstream flooding
- **Cost Estimates**
 - Alternative 1: N/A
 - Alternative 2: \$1,020,000
 - Alternative 3: \$960,000
 - Alternative 4: \$1,090,000
 - **Alternative 5: \$1,020,000**

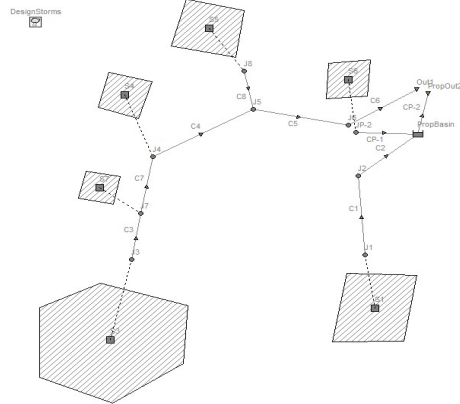
12

Industrial Park Drive and Post Office Rd Intersection

• Model Results

Downstream Headwall

Storm Event	Existing Max Total Node Inflow (cfs)	Existing Max Node Depth (ft)	Proposed Node Inflow (cfs)	Proposed Node Depth (ft)
25-Year	149.76	3.51	335.37	4.97
25-Year (2050)	166.54	3.70	340.70	5.01
25-Year (2100)	177.83	3.82	343.49	5.03
100-Year	202.37	4.06	346.40	5.05
100-Year (2050)	203.08	4.06	346.40	5.05
100-Year (2100)	203.20	4.06	346.40	5.05



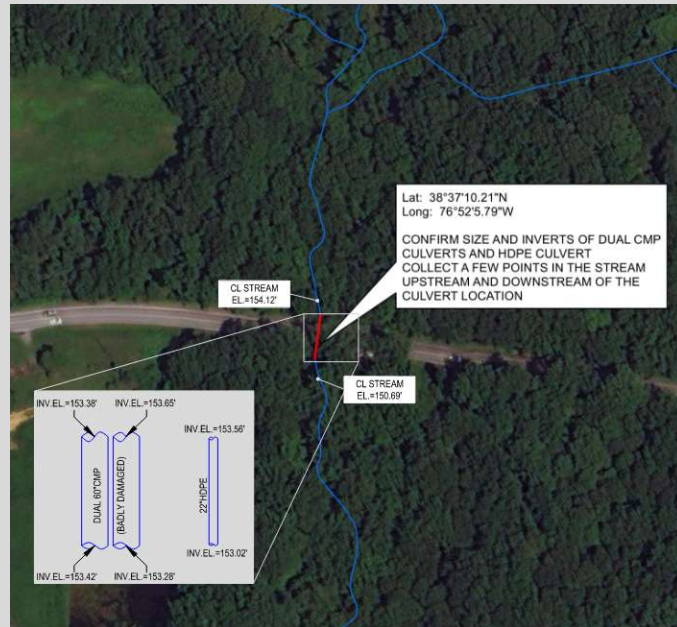
13

Industrial Park Drive and Post Office Rd Intersection



14

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road



15

Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road



- Alternative
 - Alternative 1: No Build
 - Does not address project need
 - Alternative 2: Replace dual 60" CMP with dual 60" RCP and restore stream
 - Does not meet the 25-year event
 - Alternative 3: Replace dual 60" CMP with dual 60" RCP, raise the roadway profile, and restore stream
 - Most costly option, would require a profile raise of 2-3'
 - **Alternative 4: Replace dual 60" CMPs with dual 72" RCP, replace 22" HDPE with 36" HDPE, restore stream**
 - Addresses the 25-year current and future conditions
 - Alternative 5: Replace dual 60" CMP with single 10'x5' reinforced concrete box culvert, restore stream
 - Does not address the 25-year event
- Cost Estimates
 - Alternative 1: N/A
 - Alternative 2: \$960,000
 - Alternative 3: \$1,020,000
 - **Alternative 4: \$980,000**
 - Alternative 5: \$1,120,000

Existing and Proposed Water Surface Elevations Upstream of Poplar Rd. (Alternative 4)

Storm Event	Existing WSEL (ft)	Proposed WSEL (ft)
25-Year	159.14	157.75
25-Year (2050)	159.33	158.26
25-Year (2100)	159.46	158.55
100-Year	159.75	159.31
100-Year (2050)	160.01	159.53
100-Year (2100)	160.10	159.64

*Roadway Elevation Low Point: 158.7'

16

Urban Flood Analysis

Zekiah Watershed

February 2023



CHARLES COUNTY, MARYLAND

AN ADDENDUM TO THE NUISANCE & URBAN FLOOD PLAN

Next Steps

- **Hold Steering Committee Meeting to Present Vulnerability Analysis**
- **Refine Improvement Actions & Develop Implementation Schedule**
- **Modify StoryMap to Include Methodology & Findings of Study**
- **Compile Findings in Report and Present to County for Approval**

Attachment 2

DESCRIPTION OF DATA



Description of Data

- Extents of flooding, inundation areas and historic anticipated damages
 - The State's Sea Level Rise Vulnerability layers can be viewed as a service from MD's GIS Data catalog at <https://data.imap.maryland.gov/>. Just search for "Sea Level Rise".
 - If the Flood Plain is needed that can also be viewed as a service or downloaded from the above site, just search for "Flood Plain".
 - Other online sources include: <https://mdfloodmaps.net/> or <https://www.fema.gov/flood-maps/products-tools/products>
 - Emergency Services may also have related data.
- Stormwater Infrastructure
 - PGM to provide the following GIS datasets: Streams, Streams_Hydrojunctions, swBMP, swCulvert, swDrainAreas, swEasements, swPipes, swStructures, and swVirtualDrainline.
- Models – DFIRM RiskMAP
 - PGM to provide DFIRM RiskMAP that we received with the 2015 comprehensive update to the Floodplain Maps, if available or can be obtained.
- Utilities/ROW
 - Water and sewer data would come from Utilities. Pat Anderson (Engineer II) with Utilities is the contact (301-609-5644, andersop@charlescountymd.gov).
 - PGM to provide GIS Parcel Data, from which ROW can be obtained.
- Topography – date of latest topography
 - The latest topography is 2014, 2 foot. We also have 1 foot raw data for 2014. Next LiDAR will be flown in 2023.
 - PGM to provide 2014, 2 foot topography.
- Supplemental survey data for: (1) Old Washington Road behind Waldorf Shoppers World/Burlington Coat Factory, (2) Intersection of Industrial Park Drive/Post Office Road, and (3) Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road
 - PGM does not have supplemental survey data.

Attachment 3

FIELD VISIT SUMMARIES



Field Visit Summaries

Old Washington Road and Pembroke Square

Observed:

- Only two inlets in back parking area- inlets are shallow
- Trash /debris sediment apparent inlets at low area
- Parking lot is flat and drainage system likely no pitch
- Streams/ditches adjacent to parking area have stagnant water – no pitch
- Culverts downstream look pretty clear but likely aren't getting enough flow
- Some overgrowth in the culvert area

Potential Recommendations:

- (ROW to be considered) Grade parking area
- Regrades ditches and stabilize to convey flow
- Resize pipes as feasible and pitch to convey positive flow
- Consider providing green infrastructure/stormwater storage in unused portions of parking area (pending ROW)



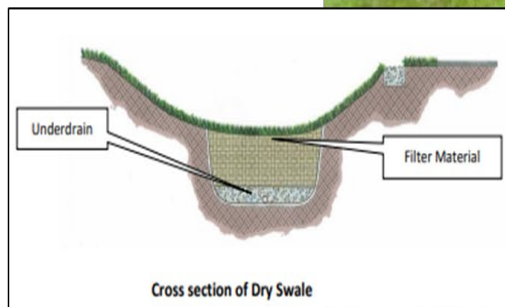
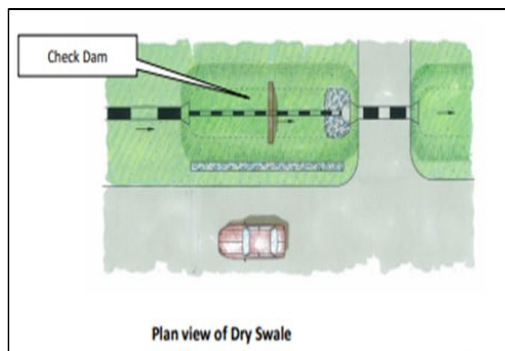
Industrial Park Drive and Post Office Road Intersection

Observed:

- Culvert at low point appears clear.
- Large drainage area believed to drain to low point. Potentially coming from surrounding new development and upstream.
- No significant erosion apparent
- Capacity of system is likely large part of this issue

Potential Recommendations:

- Investigate increasing capacity of existing culvert and adjacent drainage system
- Provide storage by adding a basin on downstream culvert at intersection
- Add rip rap and grade off the roadway with curb open to allow flow over rip rap to basin



Poplar Hill Road between St. Peters Church Road & Mattawoman Beantown Road

Observed:

- New one (2 HDPE pipes) at what appears to be the most low lying point- riprap in area and scour hole appeared to form flow on downstream ends seems to pond a bit
- On upstream end of the HDPE appears to be overgrowth
- Another appears to be original- 2 CMPs both deformed but one crushed on downstream outlet
- Also downstream appears to have no direct connection to downstream ditch
- On upstream end of CMPs there is a large tree completely blocking one opening

Potential Recommendations

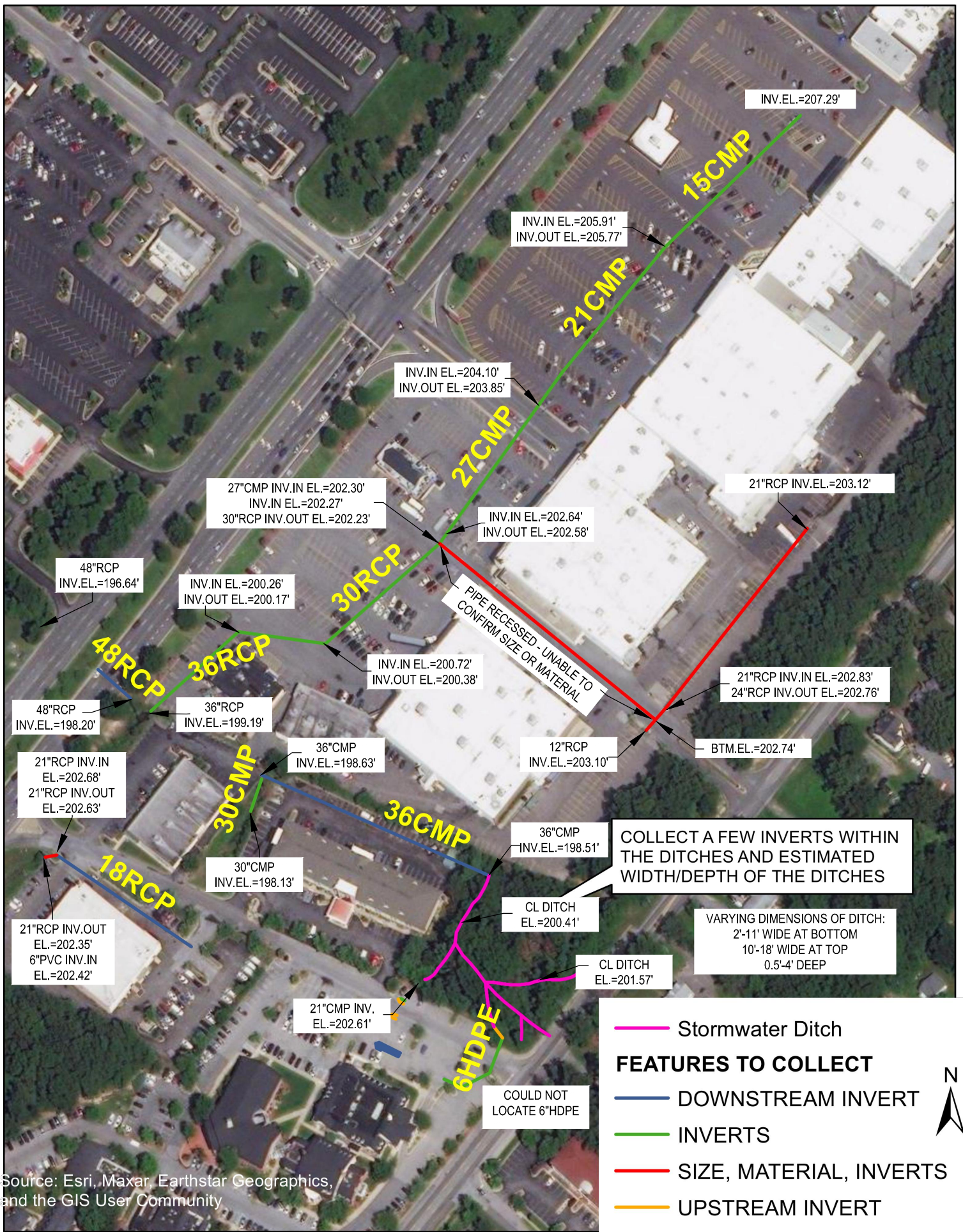
- Replace CMP pipes
- Clear vegetation and remove tree blocking
- Considering additional slope stabilization and gabion on side slopes
- Channelize both downstream ends to flow to downstream ditch



Attachment 4

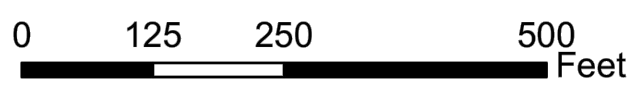
EXISTING DRAINAGE MAPS & STORMWATER INVENTORY

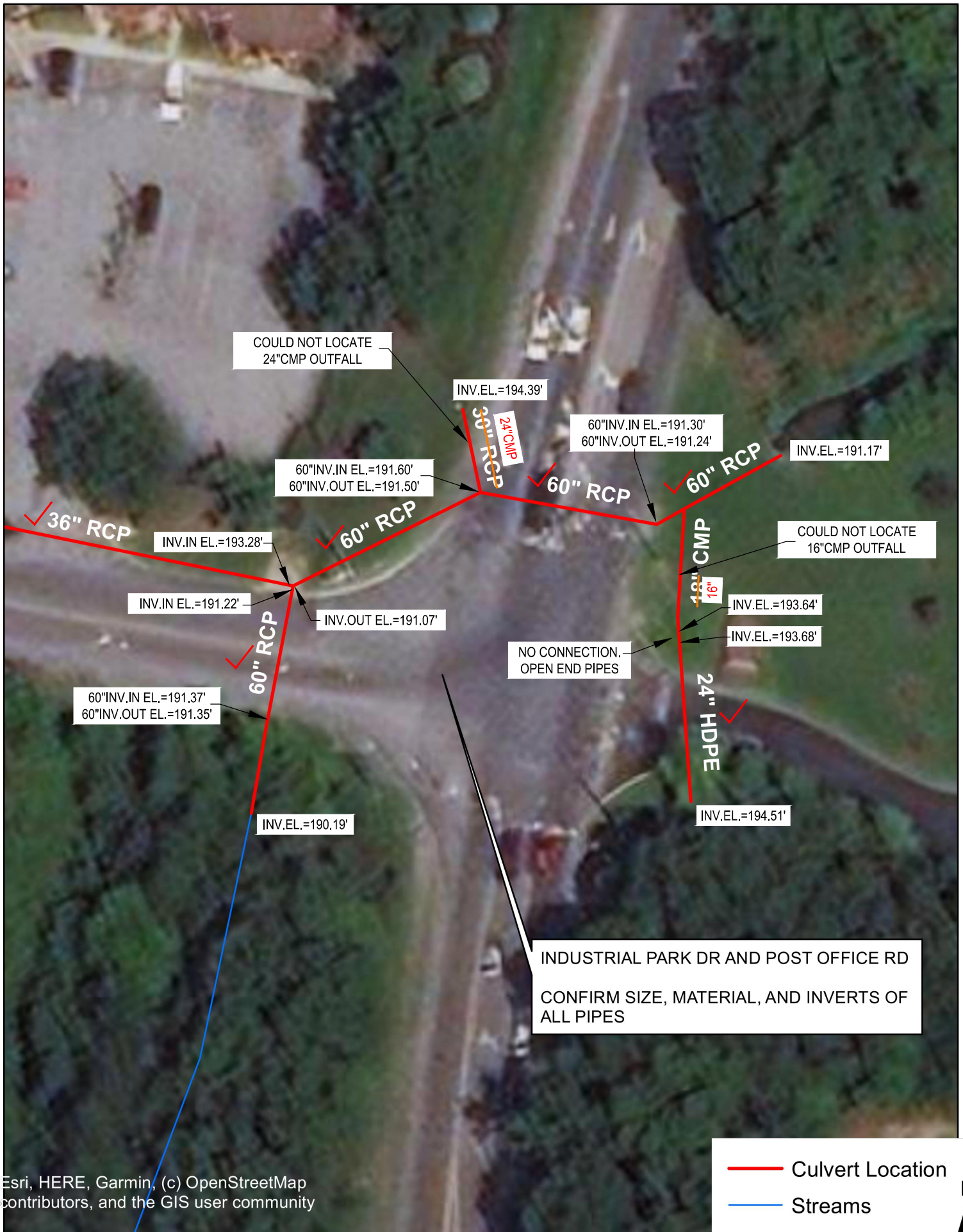


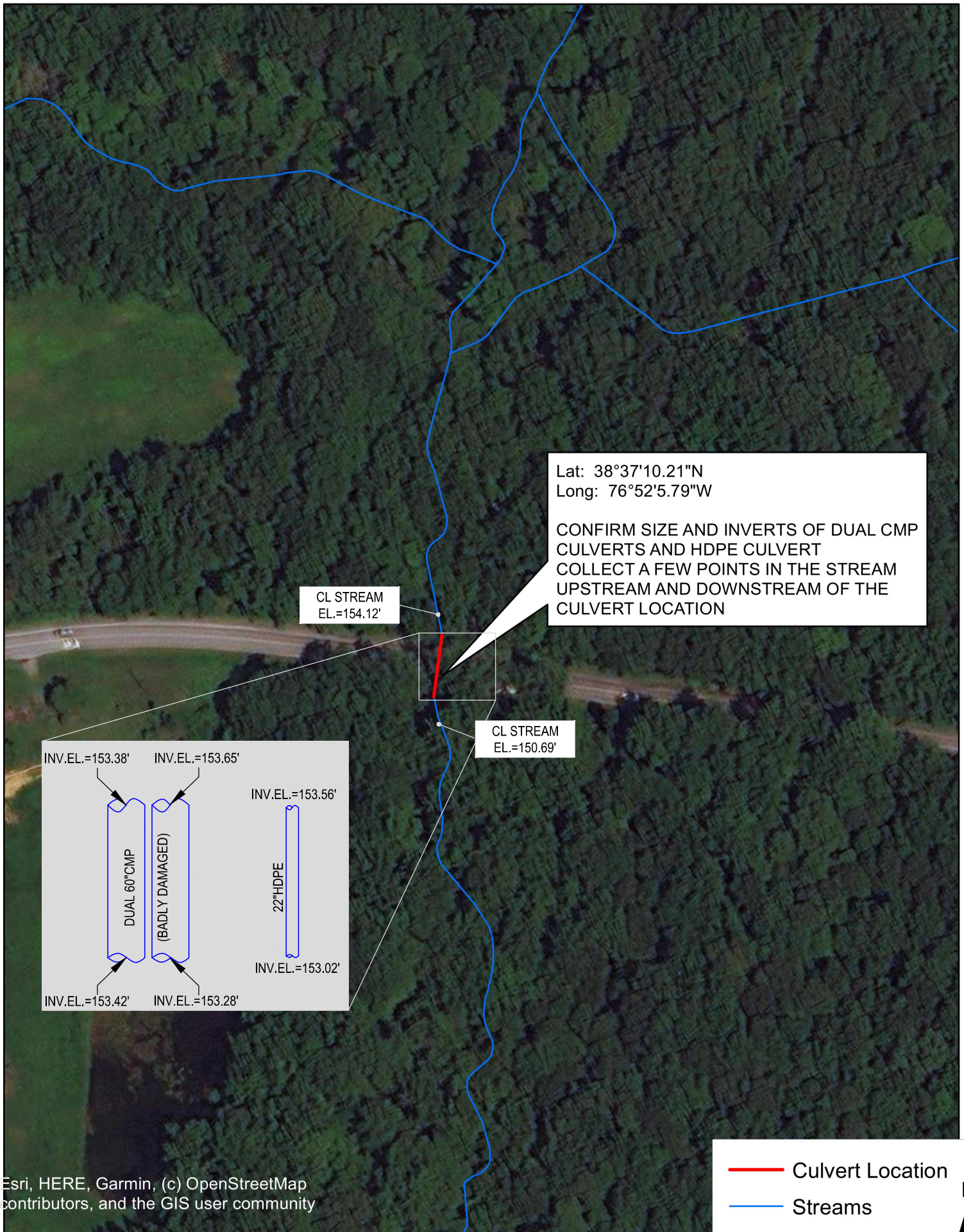


Source: Esri, Maxar, Earthstar Geographics,
and the GIS User Community

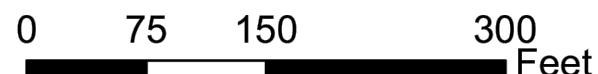
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SURVEY DATE: 10/19/2022
VERTICAL DATUM: NAVD88

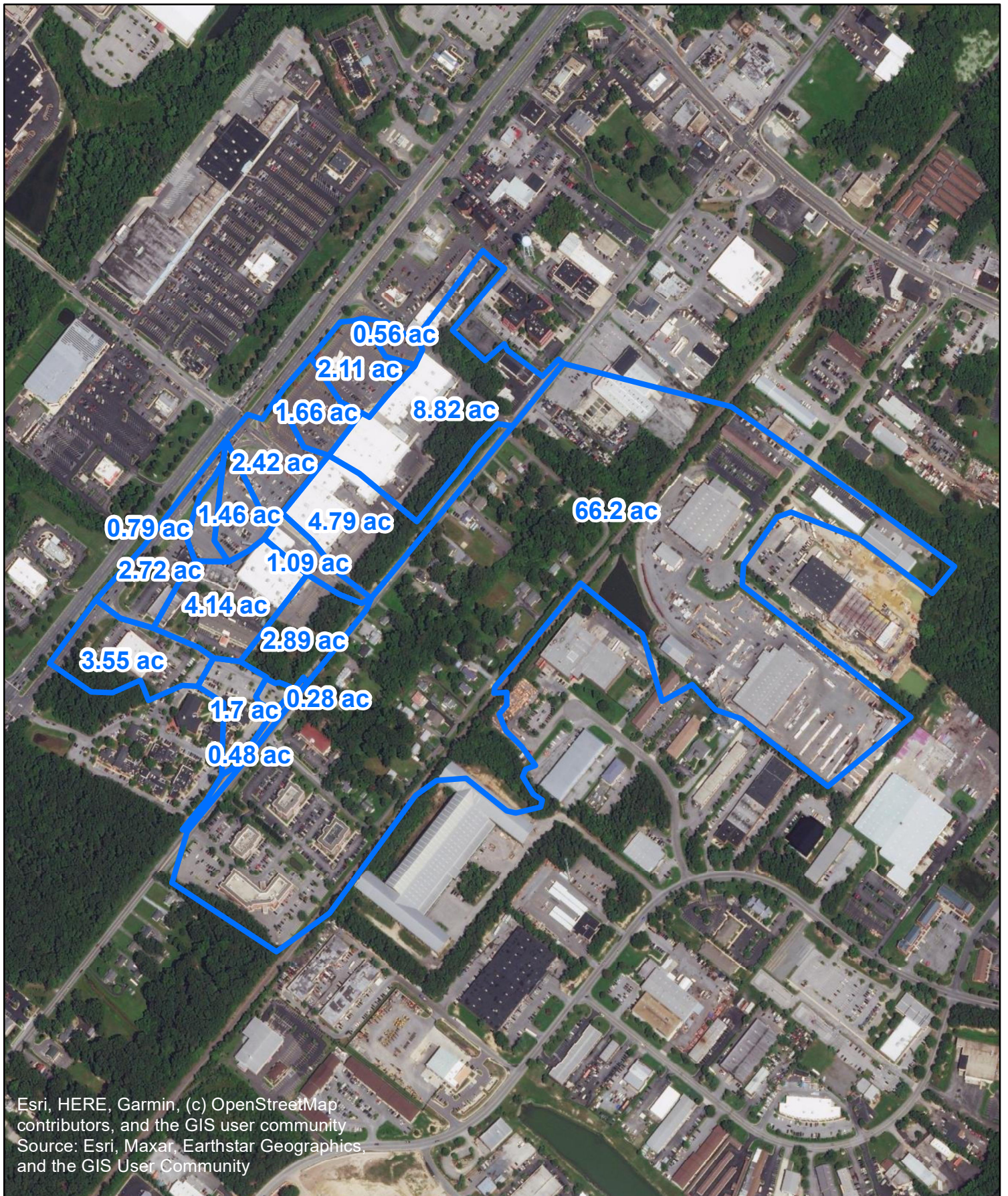






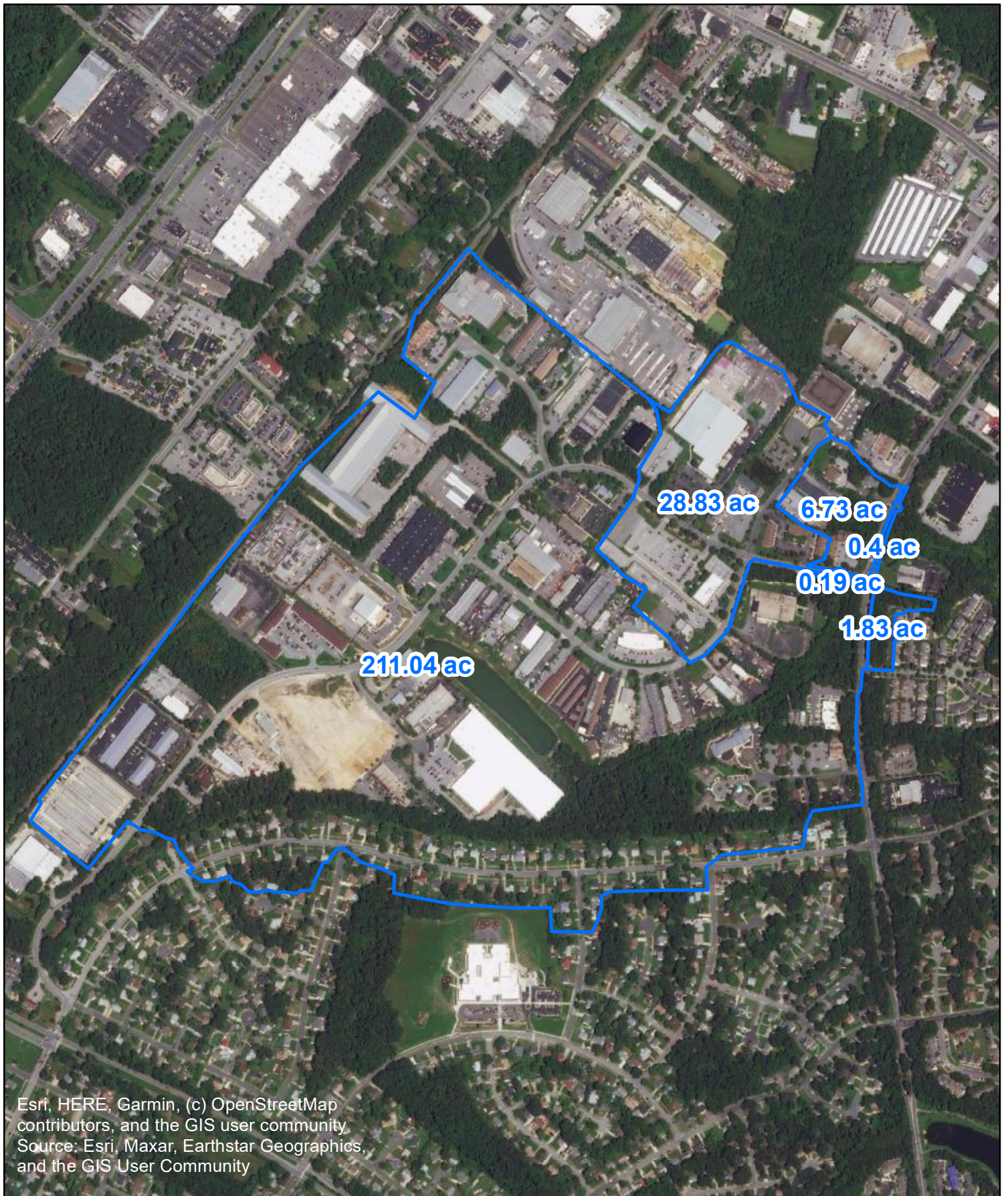
FIELD SURVEY ELEVATIONS COLLECTED BY MES SURVEY.
SURVEY DATE: 10/19/2022
VERTICAL DATUM: NAVD88





0 375 750 1,500 Feet

Charles County Zekiah Watershed Study
Location 10: Old Washington Rd at Shoppers World
Drainage Area Map



Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user community
Source: Esri, Maxar, Earthstar Geographics, and the GIS User Community



0 500 1,000 2,000 Feet

Charles County Zekiah Watershed Study
Location 12: Industrial Park Drive and Post Office Road
Drainage Area Map



Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user community
Source: Esri, Maxar, Earthstar Geographics, and the GIS User Community



0 1,000 2,000 4,000
Feet

Charles County Zekiah Watershed Study
Location 24: Poplar Hill Road
Drainage Area Map



Maryland Department of Planning Land Use/Land Cover Classification Definitions

Urban Land Uses

- 11 Low-density residential - Detached single-family/duplex dwelling units, yards and associated areas. Areas of more than 90 percent single-family/duplex dwelling units, with lot sizes of less than five acres but at least one-half acre (.2 dwelling units/acre to 2 dwelling units/acre).
- 12 Medium-density residential - Detached single-family/duplex, attached single-unit row housing, yards, and associated areas. Areas of more than 90 percent single-family/duplex units and attached single-unit row housing, with lot sizes of less than one-half acre but at least one-eighth acre (2 dwelling units/acre to 8 dwelling units/acre).
- 13 High-density residential - Attached single-unit row housing, garden apartments, high-rise apartments/condominiums, mobile home and trailer parks; areas of more than 90 percent high-density residential units, with more than 8 dwelling units per acre.
* subsidized housing
- 14 Commercial - Retail and wholesale services. Areas used primarily for the sale of products and services, including associated yards and parking areas. This category includes:
*Airports
*Welcome houses
*Telecommunication towers
*Boat Marinas
- 15 Industrial - Manufacturing and industrial parks, including associated warehouses, storage yards, research laboratories, and parking areas. Warehouses that are returned by a commercial query should be categorized as industrial. Also included are power plants.
- 16 Institutional - Elementary and secondary schools, middle schools, junior and senior high schools, public and private colleges and universities, military installations (built-up areas only, including buildings and storage, training, and similar areas), churches, medical and health facilities, correctional facilities, and government offices and facilities that are clearly separable from the surrounding land cover. This category includes:
*campgrounds owned by groups/community groups (ie girl scouts)
Sports venues

- 17 Extractive - Surface mining operations, including sand and gravel pits, quarries, coal surface mines, and deep coal mines. Status of activity (active vs. abandoned) is not distinguished.
- 18 Open urban land - Urban areas whose use does not require structures, or urban areas where non-conforming uses characterized by open land have become isolated. Included are golf courses, parks, recreation areas (except areas associated with schools or other institutions), cemeteries, and entrapped agricultural and undeveloped land within urban areas. When addressing parks, buildings are classified as 18 and ground cover is classified according to imagery.
- 191 Large lot subdivision (agriculture) - Residential subdivisions with lot sizes of less than 20 acres but at least 5 acres, with a dominant land cover of open fields or pasture.
- 192 Large lot subdivision (forest) - Residential subdivisions with lot sizes of less than 20 acres but at least 5 acres, with a dominant land cover of deciduous, evergreen or mixed forest.

Agriculture

- 21 Cropland - Field crops and forage crops.
- 22 Pasture - Land used for pasture, both permanent and rotated; grass.
- 23 Orchards/vineyards/horticulture - Areas of intensively managed commercial bush and tree crops, including areas used for fruit production, vineyards, sod and seed farms, nurseries, and green houses.
- 24 Feeding operations - Cattle feed lots, holding lots for animals, hog feeding lots, poultry houses, and commercial fishing areas (including oyster beds).
- 241 Feeding operations - Cattle feed lots, holding lots for animals, hog feeding lots, poultry houses.
- 242 Agricultural building breeding and training facilities, storage facilities, built-up areas associated with a farmstead, small farm ponds, and commercial fishing areas.
- 25 Row and garden crops - Intensively managed truck and vegetable farms and associated areas.

Forest

- 41 Deciduous forest - Forested areas in which the trees characteristically lose their leaves at the end of the growing season. Included are such species as oak, hickory, aspen, sycamore, birch, yellow poplar, elm, maple, and cypress. Note that forest classifications may not be reliable as to type (deciduous versus evergreen).
- 42 Evergreen forest - Forested areas in which the trees are characterized by persistent foliage throughout the year. Included are such species as white pine, pond pine, hemlock, southern white cedar, and red pine. Note that forest classifications may not be reliable as to type (deciduous versus evergreen).

- 43 Mixed forest - Forested areas in which neither deciduous nor evergreen species dominate, but in which there is a combination of both types.
- 44 Brush - Areas which do not produce timber or other wood products but may have cut-over timber stands, abandoned agriculture fields, or pasture. These areas are characterized by vegetation types such as sumac, vines, rose, brambles, and tree seedlings.

Water

- 50 Water - Rivers, waterways, reservoirs, ponds, bays, estuaries, and ocean.

Wetlands

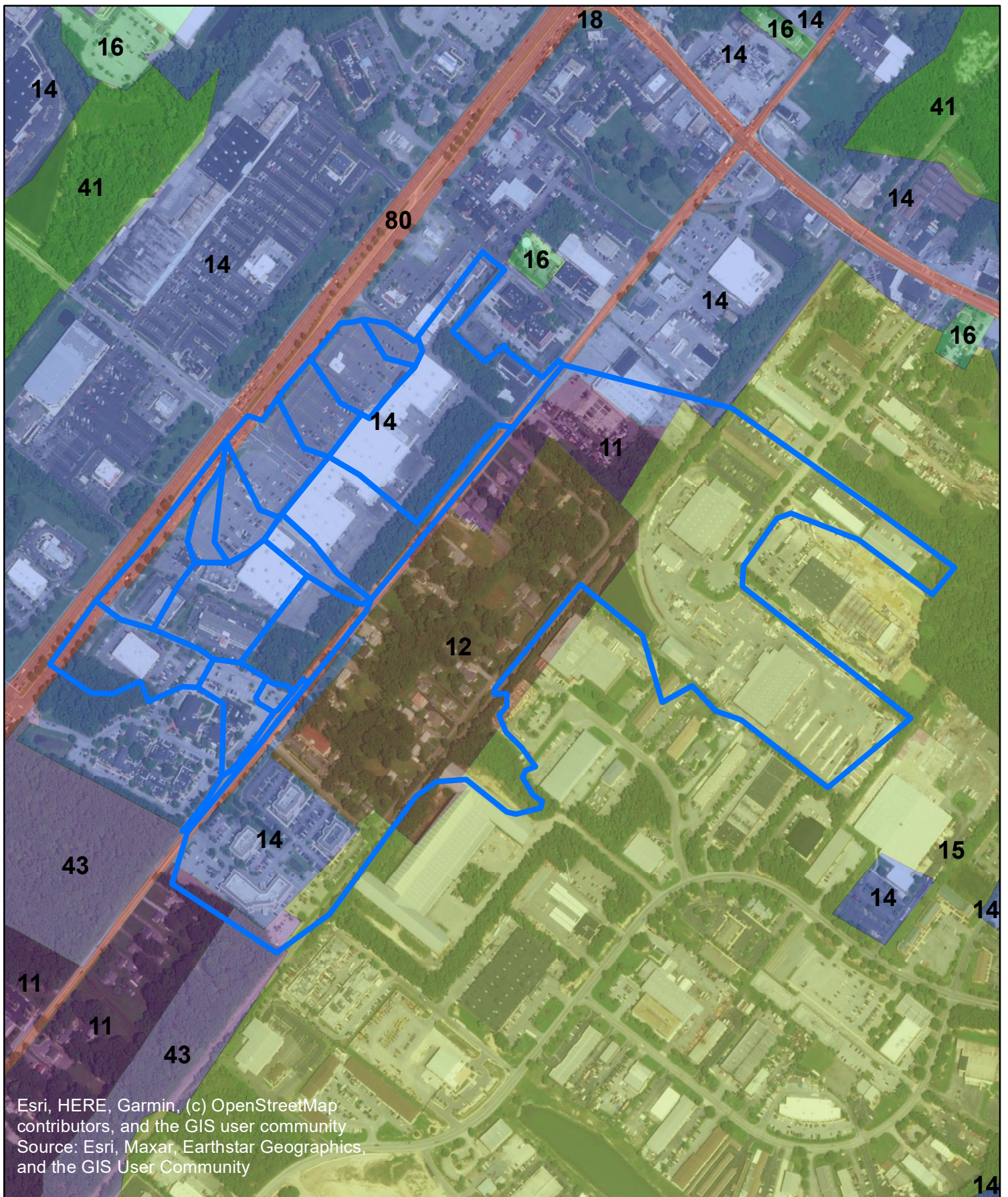
- 60 Wetlands - Forested or non-forested wetlands, including tidal flats, tidal and non-tidal marshes, and upland swamps and wet areas.

Barren Land

- 70 Barren land
- 71 Beaches - Extensive shoreline areas of sand and gravel accumulation, with no vegetative cover or other land use.
- 72 Bare exposed rock - Areas of bedrock exposure, scarps, and other natural accumulations of rock without vegetative cover.
- 73 Bare ground - Areas of exposed ground caused naturally, by construction, or by other cultural processes. Landfills (cultural process) are included in this category

Transportation

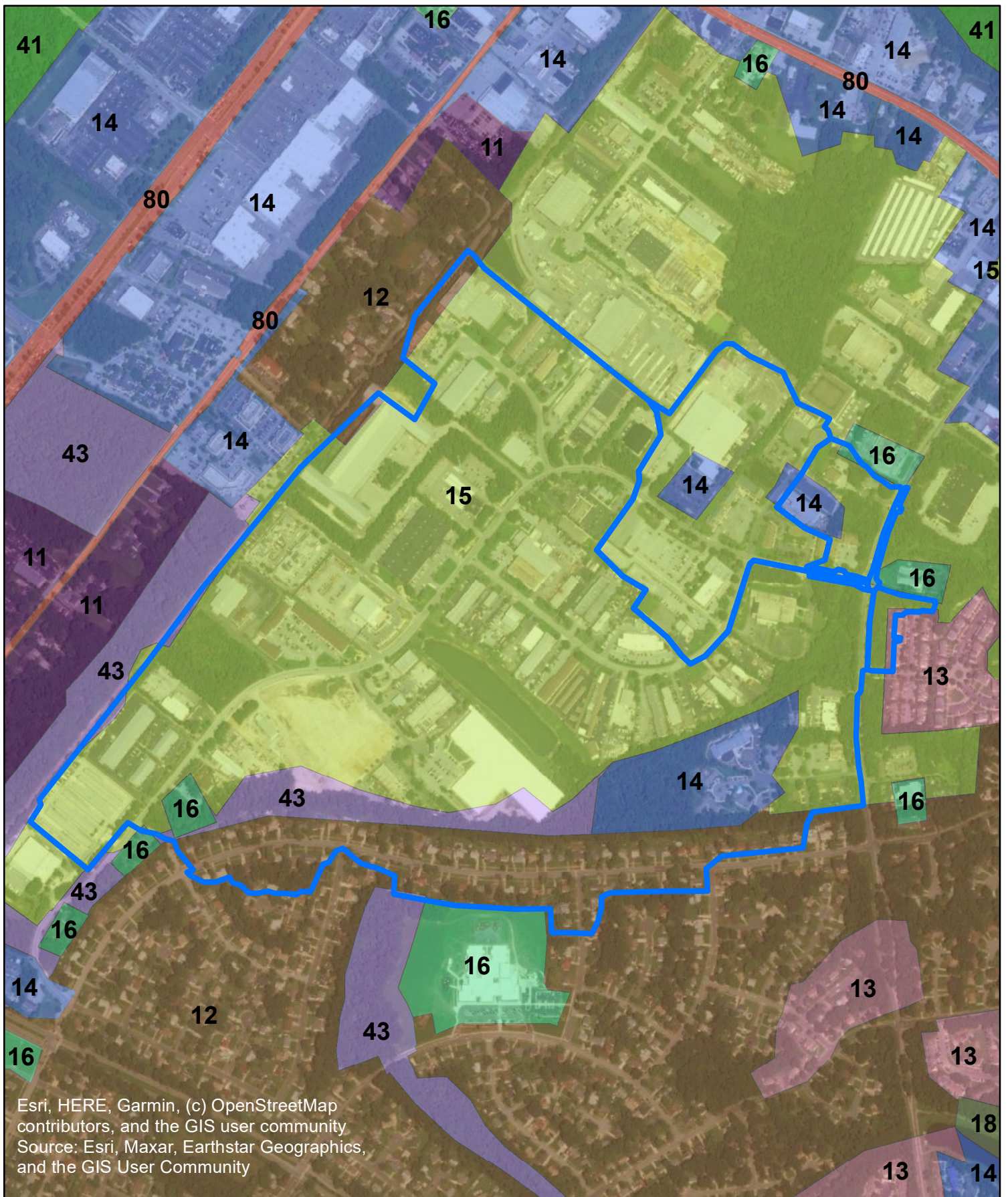
- 80 Transportation - Transportation features include major highways, light rail or metro stations and large "Park 'N Ride" lots, generally over ten acres in size. Major highways were defined as those appearing on the State Highway maps as Controlled Access Highways or Primary Highways



Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user community
Source: Esri, Maxar, Earthstar Geographics, and the GIS User Community



Charles County Zekiah Watershed Study
Location 10: Old Washington Rd at Shoppers World
Landuse Map

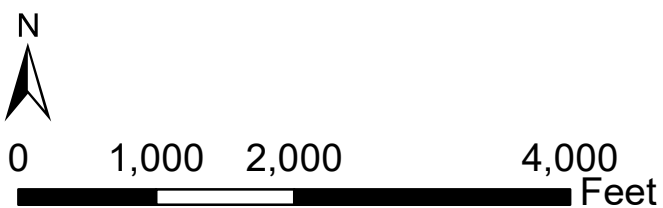
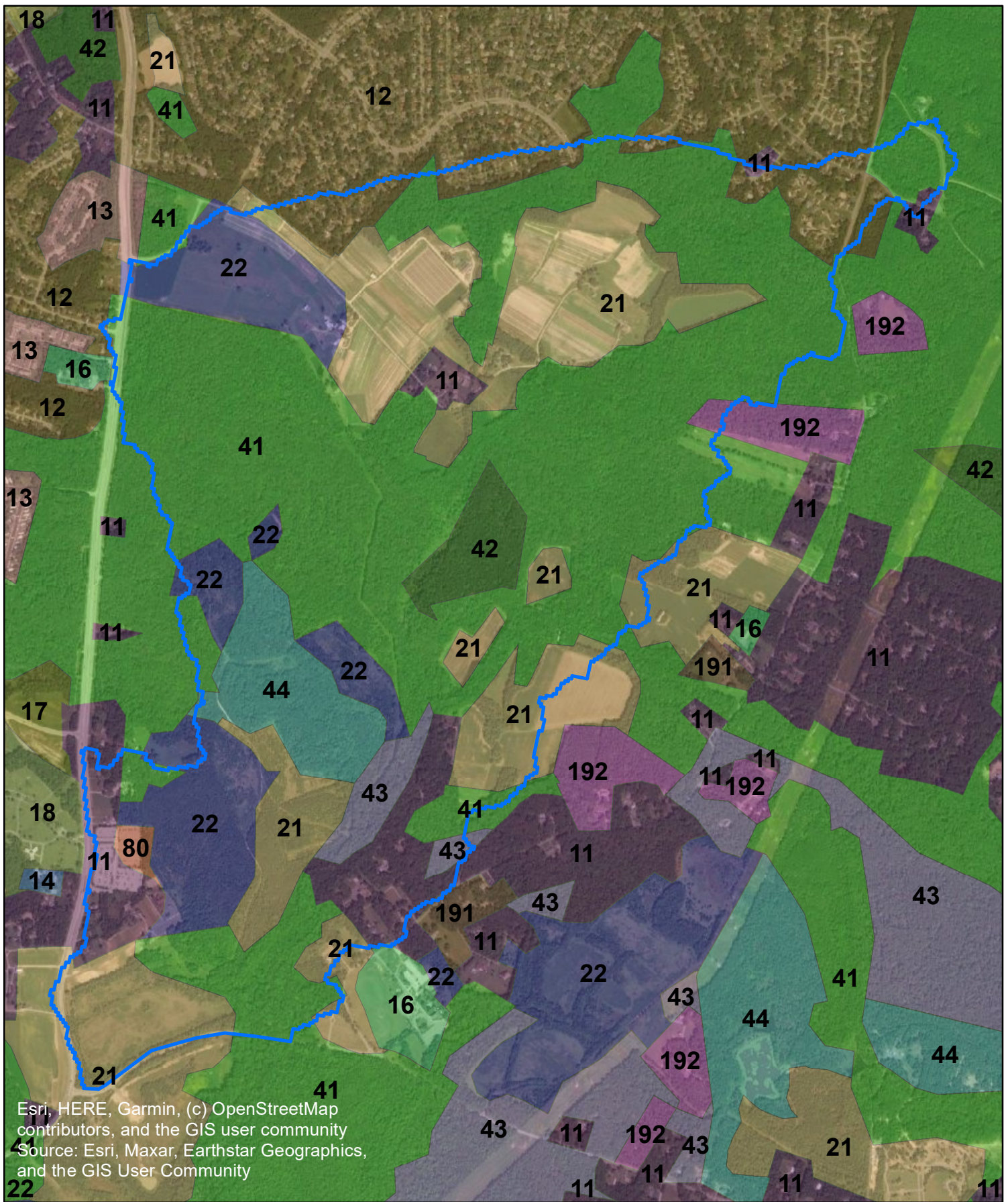


Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user community
Source: Esri, Maxar, Earthstar Geographics, and the GIS User Community



0 500 1,000 2,000 Feet

Charles County Zekiah Watershed Study
Location 12: Industrial Park Drive and Post Office Road
Landuse Map



Charles County Zekiah Watershed Study
Location 24: Poplar Hill Road
Landuse Map



United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Charles County, Maryland

Locations 10 & 12



July 20, 2022

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

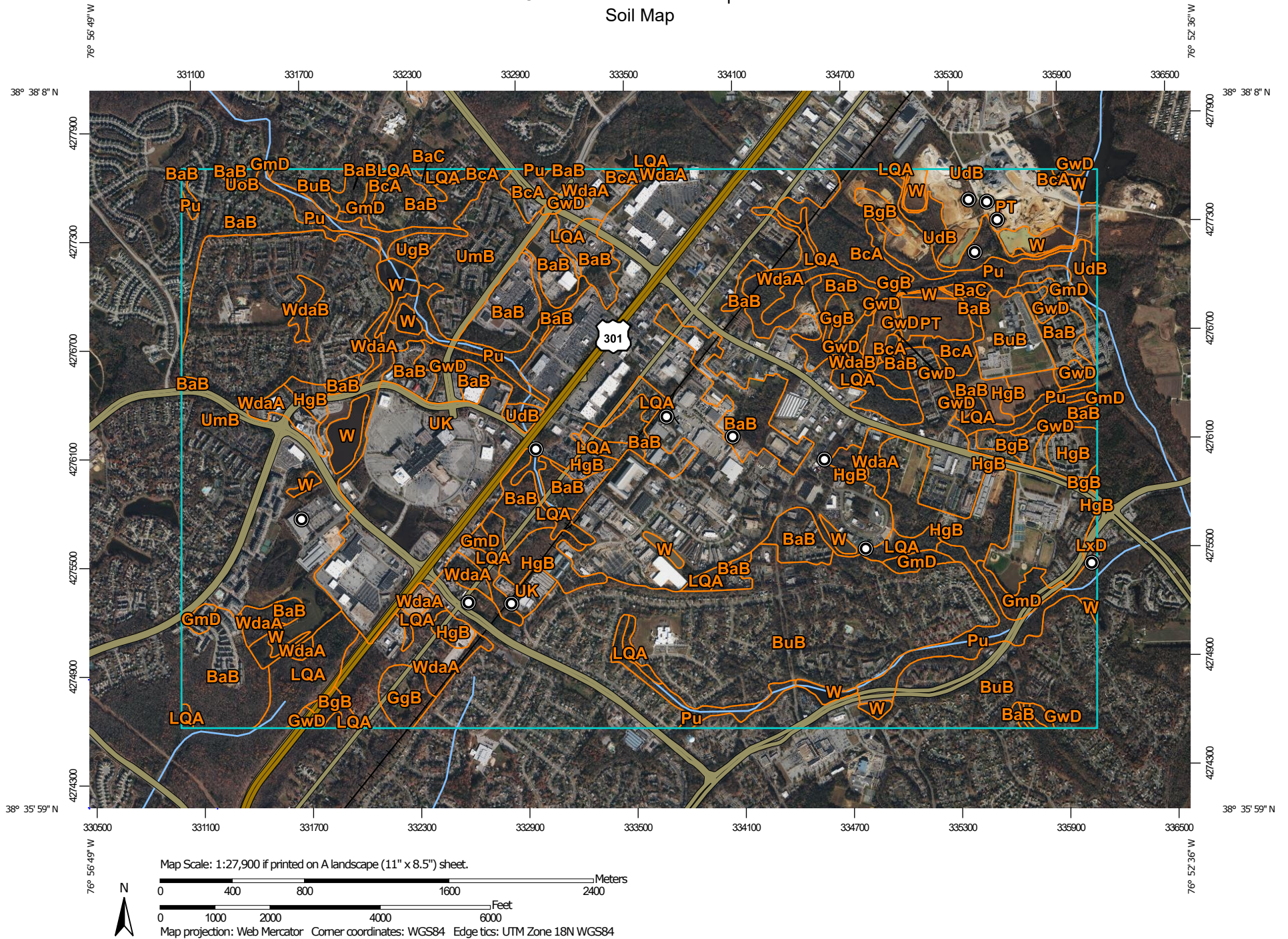
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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

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MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

 Blowout

 Borrow Pit

 Clay Spot

 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop

 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

Water Features

 Streams and Canals

Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Charles County, Maryland

Survey Area Data: Version 15, Aug 27, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Nov 23, 2020—Nov 28, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BaB	Beltsville silt loam, 2 to 5 percent slopes	471.8	12.1%
BaC	Beltsville silt loam, 5 to 10 percent slopes	8.9	0.2%
BcA	Beltsville-Aquasco complex, 0 to 2 percent slopes	101.8	2.6%
BgB	Beltsville-Grosstown-Woodstown complex, 0 to 5 percent slopes	29.2	0.8%
BuB	Beltsville-Urban land complex, 0 to 5 percent slopes	694.0	17.9%
GgB	Grosstown gravelly silt loam, 2 to 5 percent slopes	25.5	0.7%
GmD	Grosstown-Marr-Hoghole complex, 5 to 15 percent slopes	52.0	1.3%
GwD	Grosstown-Woodstown-Beltsville complex, 5 to 15 percent slopes	69.2	1.8%
HgB	Hoghole-Grosstown complex, 0 to 5 percent slopes	148.9	3.8%
LQA	Lenni and Quindocqua soils, 0 to 2 percent slopes	169.7	4.4%
LxD	Liverpool-Piccowaxen complex, 5 to 15 percent slopes	4.1	0.1%
PT	Pits, gravel	107.6	2.8%
Pu	Potobac-Issue complex, frequently flooded	152.1	3.9%
UdB	Udorthents, loamy, 0 to 5 percent slopes	34.5	0.9%
UgB	Udorthents, reclaimed gravel pits, 0 to 5 percent slopes	8.3	0.2%
UK	Urban land	1,009.3	26.0%
UmB	Urban land-Beltsville complex, 0 to 5 percent slopes	542.6	14.0%
UoB	Urban land-Grosstown complex, 0 to 5 percent slopes	2.8	0.1%
W	Water	75.5	1.9%
WdaA	Woodstown sandy loam, 0 to 2 percent slopes, Northern Coastal Plain	161.4	4.2%
WdaB	Woodstown sandy loam, 2 to 5 percent slopes, Northern Coastal Plain	18.2	0.5%

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Totals for Area of Interest		3,887.6	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

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Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Charles County, Maryland

BaB—Beltsville silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzx2

Elevation: 10 to 400 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Beltsville and similar soils: 70 percent

Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam

E - 3 to 8 inches: silt loam

Bt - 8 to 20 inches: silt loam

Btx - 20 to 41 inches: loam

2B't - 41 to 65 inches: sandy clay loam

2BCg - 65 to 71 inches: very gravelly sandy clay loam

2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: 20 to 40 inches to fragipan

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Aquasco

Percent of map unit: 10 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Reybold

Percent of map unit: 10 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

Grosstown

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

BaC—Beltsville silt loam, 5 to 10 percent slopes

Map Unit Setting

National map unit symbol: 1qzx3
Elevation: 10 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Beltsville and similar soils: 70 percent
Minor components: 30 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 5 to 10 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Grosstown

Percent of map unit: 15 percent
Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (three-dimensional): Interfluve, tread
Down-slope shape: Linear
Across-slope shape: Linear, convex
Hydric soil rating: No

Reybold

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Aquasco

Percent of map unit: 5 percent
Landform: Broad interstream divides

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Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Hoghole

Percent of map unit: 5 percent
Landform: Hillslopes
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Convex
Hydric soil rating: No

BcA—Beltsville-Aquasco complex, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1qzww
Elevation: 10 to 360 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Beltsville and similar soils: 50 percent
Aquasco and similar soils: 40 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained

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Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Hydric soil rating: No

Description of Aquasco

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 4 inches: silt loam

E - 4 to 10 inches: silt loam

Bt - 10 to 20 inches: silty clay loam

Btx - 20 to 44 inches: loam

BCt - 44 to 72 inches: clay loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 8 to 40 inches to fragipan

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.01 to 0.20 in/hr)

Depth to water table: About 10 to 16 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Hydric soil rating: No

Minor Components

Lenni, undrained

Percent of map unit: 5 percent

Landform: Depressions on broad interstream divides

Hydric soil rating: Yes

Reybold

Percent of map unit: 5 percent

Landform: Fluviomarine terraces, broad interstream divides

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Landform position (three-dimensional): Interfluve, tread
Hydric soil rating: No

BgB—Beltsville-Grosstown-Woodstown complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzx7
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Beltsville and similar soils: 35 percent
Grosstown and similar soils: 30 percent
Woodstown and similar soils: 15 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Hydric soil rating: No

Description of Grosstown

Setting

Landform: Swales, depressions, drainhead complexes, broad interstream divides
Landform position (three-dimensional): Tread
Down-slope shape: Linear, concave
Across-slope shape: Convex, concave
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: A
Hydric soil rating: No

Description of Woodstown

Setting

Landform: Depressions, swales, drainageways, drainhead complexes, broad interstream divides
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 8 inches: sandy loam
Bt - 8 to 28 inches: loam
BC - 28 to 42 inches: fine sandy loam
CB - 42 to 60 inches: sandy loam
CBg - 60 to 72 inches: loamy sand

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Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.20 to 2.00 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 10 percent

Landform: Drainhead complexes, broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

Issue

Percent of map unit: 5 percent

Landform: Swales, drainageways, drainhead complexes

Down-slope shape: Concave

Across-slope shape: Linear

Hydric soil rating: No

Quindocqua, undrained

Percent of map unit: 5 percent

Landform: Depressions, drainhead complexes

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

BuB—Beltsville-Urban land complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzx4

Elevation: 10 to 360 feet

Mean annual precipitation: 40 to 50 inches

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Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Beltsville and similar soils: 50 percent

Urban land: 40 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam

E - 3 to 8 inches: silt loam

Bt - 8 to 20 inches: silt loam

Btx - 20 to 41 inches: loam

2B't - 41 to 65 inches: sandy clay loam

2BCg - 65 to 71 inches: very gravelly sandy clay loam

2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 20 to 40 inches to fragipan

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D

Hydric soil rating: No

Minor Components

Aquasco

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

GgB—Grosstown gravelly silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzxd
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Grosstown and similar soils: 80 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (two-dimensional): Summit, shoulder, backslope
Landform position (three-dimensional): Interfluve, tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: A
Hydric soil rating: No

Minor Components

Woodstown

Percent of map unit: 20 percent
Landform: Depressions on broad interstream divides, stream terraces, swales, fluviomarine terraces
Landform position (three-dimensional): Tread
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: No

GmD—Grosstown-Marr-Hoghole complex, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzxb
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Grosstown and similar soils: 31 percent
Marr and similar soils: 29 percent
Hoghole and similar soils: 15 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

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Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam

Bt1 - 4 to 20 inches: silt loam

Bt2 - 20 to 26 inches: gravelly loam

2Bt3 - 26 to 71 inches: extremely gravelly silt loam

3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Hydric soil rating: No

Description of Marr

Setting

Landform: Knolls

Landform position (three-dimensional): Side slope, nose slope, head slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: fine sandy loam

Bt1 - 4 to 25 inches: fine sandy loam

Bt2 - 25 to 57 inches: sandy clay loam

BC - 57 to 76 inches: loamy fine sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Custom Soil Resource Report

Available water supply, 0 to 60 inches: High (about 9.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Hydric soil rating: No

Description of Hoghole

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and gravelly fluviomarine deposits

Typical profile

A - 0 to 4 inches: sand

Bw1 - 4 to 33 inches: very gravelly sand

Bw2 - 33 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (1.98 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Beltsville

Percent of map unit: 10 percent

Landform: Knolls, hillslopes, stream terraces, fluviomarine terraces

Landform position (three-dimensional): Side slope, interfluve, riser

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

Dodon

Percent of map unit: 10 percent

Landform: Stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Issue

Percent of map unit: 5 percent
Landform: Flood plains, drainageways
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

GwD—Grosstown-Woodstown-Beltsville complex, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzx8
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Grosstown and similar soils: 31 percent
Woodstown and similar soils: 29 percent
Beltsville and similar soils: 20 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (three-dimensional): Interfluvium, tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low

Custom Soil Resource Report

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Hydric soil rating: No

Description of Woodstown

Setting

Landform: Swales, depressions, interfluves, broad interstream divides, fluviomarine terraces, drainhead complexes

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Tread

Down-slope shape: Linear, concave

Across-slope shape: Concave, linear

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 28 inches: loam

BC - 28 to 42 inches: fine sandy loam

CB - 42 to 60 inches: sandy loam

CBg - 60 to 72 inches: loamy sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C

Hydric soil rating: No

Description of Beltsville

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluvium

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Custom Soil Resource Report

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 10 percent
Landform: Hillslopes, drainhead complexes
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Convex
Hydric soil rating: No

Issue

Percent of map unit: 5 percent
Landform: Flood plains, drainageways, drainhead complexes
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

HgB—Hoghole-Grosstown complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwm

Elevation: 0 to 400 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Prime farmland if irrigated

Map Unit Composition

Hoghole and similar soils: 45 percent

Grosstown and similar soils: 30 percent

Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hoghole

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and gravelly fluviomarine deposits

Typical profile

A - 0 to 4 inches: sand

Bw1 - 4 to 33 inches: very gravelly sand

Bw2 - 33 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (1.98 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Hydric soil rating: No

Description of Grosstown

Setting

Landform: Stream terraces, fluvio marine terraces, broad interstream divides

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy and gravelly fluvio marine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam

Bt1 - 4 to 20 inches: silt loam

Bt2 - 20 to 26 inches: gravelly loam

2Bt3 - 26 to 71 inches: extremely gravelly silt loam

3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 15 percent

Landform: Stream terraces, fluvio marine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Woodstown

Percent of map unit: 10 percent

Landform: Depressions, stream terraces, swales, broad interstream divides, fluvio marine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Hydric soil rating: No

LQA—Lenni and Quindocqua soils, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1qzxc
Elevation: 10 to 360 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Prime farmland if drained

Map Unit Composition

Lenni, undrained, and similar soils: 50 percent
Quindocqua, undrained, and similar soils: 30 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lenni, Undrained

Setting

Landform: Depressions on broad interstream divides, fluviomarine terraces
Landform position (three-dimensional): Tread
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Parent material: Clayey fluviomarine deposits

Typical profile

A - 0 to 6 inches: silt loam
Eg - 6 to 9 inches: silt loam
Btg1 - 9 to 26 inches: silty clay loam
Btg2 - 26 to 49 inches: clay
2Cg - 49 to 54 inches: loamy sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.60 in/hr)
Depth to water table: About 0 to 10 inches
Frequency of flooding: None
Frequency of ponding: Occasional
Available water supply, 0 to 60 inches: Moderate (about 7.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5w
Hydrologic Soil Group: C/D
Hydric soil rating: Yes

Description of Quindocqua, Undrained

Setting

Landform: Depressions on broad interstream divides, fluviomarine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Typical profile

Oi - 0 to 4 inches: slightly decomposed plant material

A - 4 to 11 inches: loam

Btg - 11 to 33 inches: loam

2BCg - 33 to 59 inches: very fine sandy loam

2CBg - 59 to 64 inches: very fine sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)

Depth to water table: About 0 to 10 inches

Frequency of flooding: None

Frequency of ponding: Occasional

Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Hydric soil rating: Yes

Minor Components

Annemessex

Percent of map unit: 10 percent

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Concave

Hydric soil rating: No

Beltsville

Percent of map unit: 5 percent

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex, linear

Across-slope shape: Convex, linear

Hydric soil rating: No

Liverpool

Percent of map unit: 5 percent

Landform: Broad interstream divides

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

LxD—Liverpool-Piccowaxen complex, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzy1

Elevation: 10 to 370 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Liverpool and similar soils: 45 percent

Piccowaxen and similar soils: 40 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Liverpool

Setting

Landform: Fluvio-marine terraces

Landform position (three-dimensional): Riser

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty and loamy fluvio-marine deposits

Typical profile

A - 0 to 2 inches: silt loam

E - 2 to 5 inches: silt loam

Bt1 - 5 to 13 inches: silt loam

Bt2 - 13 to 35 inches: clay loam

Btg - 35 to 64 inches: sandy clay loam

BC - 64 to 74 inches: sandy clay loam

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.60 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Custom Soil Resource Report

Hydrologic Soil Group: D

Hydric soil rating: No

Description of Piccowaxen

Setting

Landform: Fluvio-marine terraces

Landform position (three-dimensional): Riser

Down-slope shape: Concave, linear

Across-slope shape: Linear

Parent material: Silty and loamy fluvio-marine deposits

Typical profile

A - 0 to 4 inches: loam

Bt - 4 to 16 inches: silt loam

Btg1 - 16 to 28 inches: silt loam

Btg2 - 28 to 56 inches: clay loam

2BCg - 56 to 72 inches: fine sandy loam

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.57 in/hr)

Depth to water table: About 10 to 20 inches

Frequency of flooding: None

Frequency of ponding: Rare

Available water supply, 0 to 60 inches: High (about 10.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C/D

Hydric soil rating: No

Minor Components

Croom

Percent of map unit: 10 percent

Landform: Hillslopes, knolls

Landform position (three-dimensional): Side slope

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Marr

Percent of map unit: 5 percent

Landform: Fluvio-marine terraces

Landform position (three-dimensional): Riser

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

PT—Pits, gravel

Map Unit Composition

Pits, gravel: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Pu—Potobac-Issue complex, frequently flooded

Map Unit Setting

National map unit symbol: 1qzxf

Elevation: 0 to 250 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 58 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Potobac and similar soils: 70 percent

Issue and similar soils: 25 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Potobac

Setting

Landform: Flood plains

Down-slope shape: Linear

Across-slope shape: Linear

Typical profile

A - 0 to 8 inches: loam

Bg - 8 to 17 inches: loam

Cg1 - 17 to 39 inches: sandy loam

Cg2 - 39 to 59 inches: very gravelly coarse sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

*Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)*

Depth to water table: About 0 to 10 inches

Frequency of flooding: Frequent

Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Hydric soil rating: Yes

Description of Issue

Setting

Landform: Flood plains

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy alluvium

Typical profile

Ap - 0 to 4 inches: silt loam

Bw - 4 to 19 inches: loam

Bg1 - 19 to 30 inches: fine sandy loam

Bg2 - 30 to 58 inches: fine sandy loam

Ab - 58 to 70 inches: silt loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 2.00 in/hr)

Depth to water table: About 10 to 20 inches

Frequency of flooding: Occasional

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Hydric soil rating: No

Minor Components

Lenni, undrained

Percent of map unit: 5 percent

Landform: Depressions on fluvio-marine terraces

Landform position (three-dimensional): Tread

Hydric soil rating: Yes

UdB—Udorthents, loamy, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwn

Elevation: 0 to 300 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Setting

Landform: Broad interstream divides

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Fluvio-marine deposits

Typical profile

AC - 0 to 2 inches: loam

C - 2 to 72 inches: gravelly loam

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very high (0.01 to 19.98 in/hr)

Depth to water table: About 40 to 72 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Urban land

Percent of map unit: 7 percent

Custom Soil Resource Report

Landform: Flats
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: Unranked

Beltsville

Percent of map unit: 3 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

UgB—Udorthents, reclaimed gravel pits, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwq
Elevation: 0 to 300 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, reclaimed gravel pits, and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Reclaimed Gravel Pits

Setting

Landform: Terraces, flood plains, broad interstream divides
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Mine spoil or earthy fill

Typical profile

AC - 0 to 4 inches: gravelly sandy loam
C - 4 to 72 inches: very gravelly sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 5.95 in/hr)
Depth to water table: About 0 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

UK—Urban land

Map Unit Setting

National map unit symbol: 1qzwt

Elevation: 0 to 130 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Flats

Down-slope shape: Linear

Across-slope shape: Linear

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D

Hydric soil rating: Unranked

Minor Components

Udorthents, loamy

Percent of map unit: 7 percent

Landform: Broad interstream divides

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Beltsville

Percent of map unit: 3 percent

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

UmB—Urban land-Beltsville complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzws
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 58 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 50 percent
Beltsville and similar soils: 35 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Flats
Down-slope shape: Linear
Across-slope shape: Linear

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 8
Hydrologic Soil Group: D
Hydric soil rating: Unranked

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Side slope, interfluvial
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: 20 to 40 inches to fragipan

Custom Soil Resource Report

Drainage class: Moderately well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Grosstown

Percent of map unit: 5 percent
Landform: Stream terraces, fluvio-marine terraces, broad interstream divides
Landform position (three-dimensional): Tread
Hydric soil rating: No

Aquasco

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions on fluvio-marine terraces
Landform position (three-dimensional): Tread
Hydric soil rating: Yes

UoB—Urban land-Grosstown complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwr
Elevation: 10 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 80 percent
Grosstown and similar soils: 15 percent
Minor components: 5 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D

Hydric soil rating: No

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam

Bt1 - 4 to 20 inches: silt loam

Bt2 - 20 to 26 inches: gravelly loam

2Bt3 - 26 to 71 inches: extremely gravelly silt loam

3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Beltsville

Percent of map unit: 5 percent

Landform: Broad interstream divides

Landform position (three-dimensional): Side slope, interfluvial

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

W—Water

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

WdaA—Woodstown sandy loam, 0 to 2 percent slopes, Northern Coastal Plain

Map Unit Setting

National map unit symbol: 2thvw

Elevation: 0 to 280 feet

Mean annual precipitation: 42 to 48 inches

Mean annual air temperature: 52 to 58 degrees F

Frost-free period: 180 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Woodstown and similar soils: 81 percent

Minor components: 19 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodstown

Setting

Landform: Depressions, flats, fluviomarine terraces, broad interstream divides

Landform position (two-dimensional): Footslope, summit

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 7 inches: sandy loam

E - 7 to 11 inches: sandy loam

Bt - 11 to 29 inches: sandy loam

BCg - 29 to 45 inches: fine sandy loam

Cg - 45 to 80 inches: loamy sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

*Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)*

Depth to water table: About 20 to 40 inches

Custom Soil Resource Report

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Fallsington

Percent of map unit: 7 percent

Landform: Drainageways, depressions, swales, flats

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Dip, talf

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Hydric soil rating: Yes

Hammonton

Percent of map unit: 7 percent

Landform: Flats, broad interstream divides

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Hambrook

Percent of map unit: 5 percent

Landform: Flats, fluviomarine terraces

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

WdaB—Woodstown sandy loam, 2 to 5 percent slopes, Northern Coastal Plain

Map Unit Setting

National map unit symbol: 2thvx

Elevation: 0 to 490 feet

Mean annual precipitation: 42 to 48 inches

Mean annual air temperature: 52 to 58 degrees F

Frost-free period: 180 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Woodstown and similar soils: 81 percent

Minor components: 19 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodstown

Setting

Landform: Flats, depressions, fluvio marine terraces, broad interstream divides

Landform position (two-dimensional): Shoulder, footslope

Landform position (three-dimensional): Riser, dip

Down-slope shape: Convex, concave

Across-slope shape: Linear, concave

Parent material: Loamy fluvio marine deposits

Typical profile

Ap - 0 to 7 inches: sandy loam

E - 7 to 11 inches: sandy loam

Bt - 11 to 29 inches: sandy loam

BCg - 29 to 45 inches: fine sandy loam

Cg - 45 to 80 inches: loamy sand

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Hammonton

Percent of map unit: 7 percent

Landform: Flats, broad interstream divides

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Dip

Down-slope shape: Convex

Across-slope shape: Linear

Hydric soil rating: No

Fallsington, occasionally ponded

Percent of map unit: 7 percent

Landform: Drainageways, depressions, swales, flats

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Dip, tal

Custom Soil Resource Report

Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: Yes

Hambrook

Percent of map unit: 5 percent
Landform: Flats, fluviomarine terraces
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Riser, dip
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

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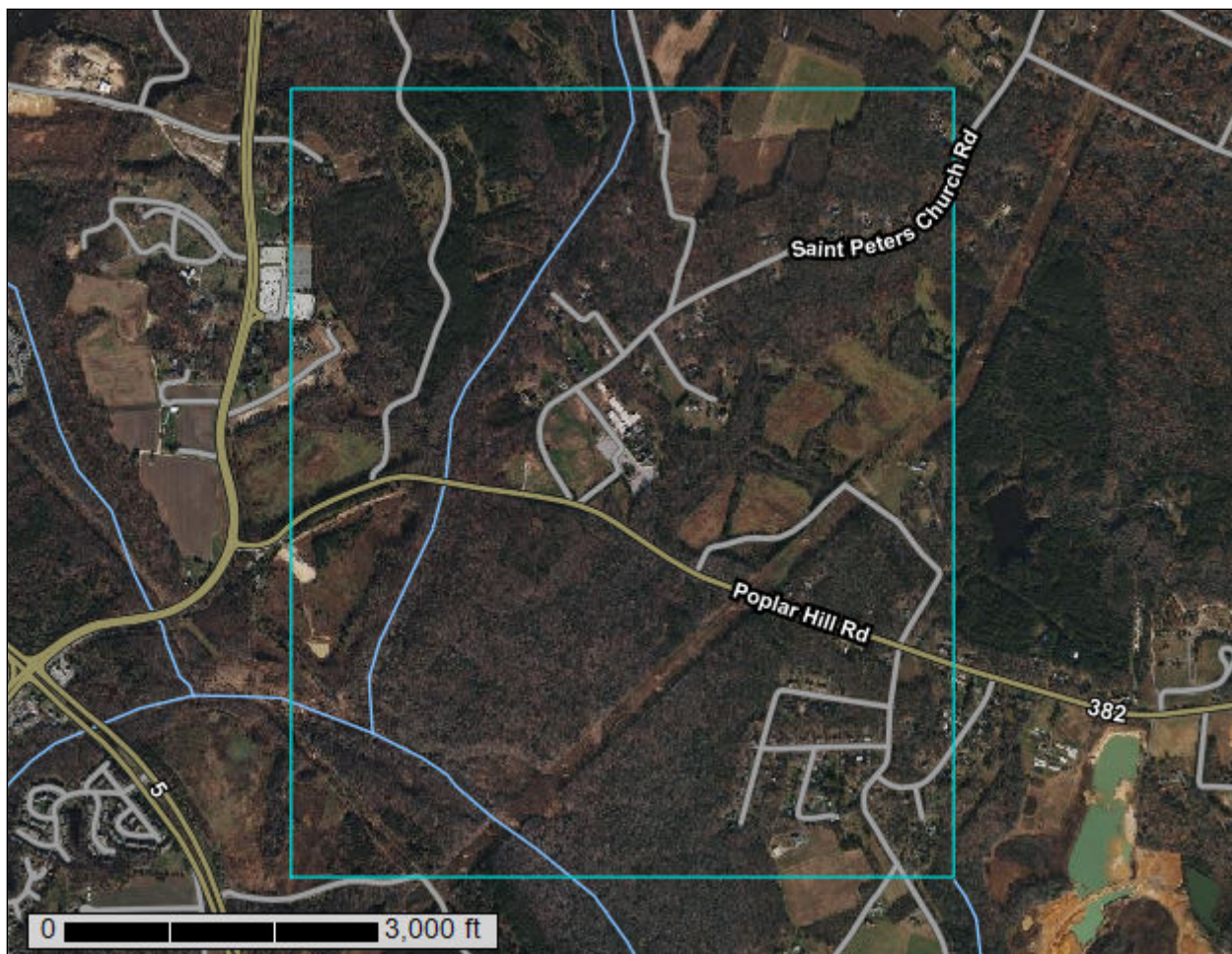
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Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for **Charles County, Maryland**

Location 24



July 20, 2022

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report

Soil Map



Custom Soil Resource Report

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

 Blowout

 Borrow Pit

 Clay Spot

 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop

 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

Water Features

 Streams and Canals

Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Charles County, Maryland

Survey Area Data: Version 15, Aug 27, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Nov 23, 2020—Nov 28, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
AsA	Annemessex silt loam, 0 to 2 percent slopes	3.3	0.3%
BaB	Beltsville silt loam, 2 to 5 percent slopes	243.2	22.2%
BaC	Beltsville silt loam, 5 to 10 percent slopes	22.5	2.0%
BcA	Beltsville-Aquasco complex, 0 to 2 percent slopes	28.6	2.6%
BgB	Beltsville-Grosstown-Woodstown complex, 0 to 5 percent slopes	113.3	10.3%
GgB	Grosstown gravelly silt loam, 2 to 5 percent slopes	0.5	0.0%
GmD	Grosstown-Marr-Hoghole complex, 5 to 15 percent slopes	109.3	10.0%
GmF	Grosstown-Marr-Hoghole complex, 15 to 40 percent slopes	65.2	5.9%
GwD	Grosstown-Woodstown-Beltsville complex, 5 to 15 percent slopes	52.9	4.8%
HgB	Hoghole-Grosstown complex, 0 to 5 percent slopes	36.2	3.3%
Is	Issue silt loam, occasionally flooded	22.6	2.1%
LQA	Lenni and Quindocqua soils, 0 to 2 percent slopes	33.0	3.0%
LsB	Liverpool silt loam, 2 to 5 percent slopes	45.6	4.2%
PT	Pits, gravel	12.2	1.1%
Pu	Potobac-Issue complex, frequently flooded	135.9	12.4%
UdB	Udorthents, loamy, 0 to 5 percent slopes	163.5	14.9%
UdD	Udorthents, loamy, 5 to 15 percent slopes	0.2	0.0%
WdaA	Woodstown sandy loam, 0 to 2 percent slopes, Northern Coastal Plain	4.0	0.4%
WdaB	Woodstown sandy loam, 2 to 5 percent slopes, Northern Coastal Plain	4.2	0.4%
Totals for Area of Interest		1,096.2	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas

shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Charles County, Maryland

AsA—Annemessex silt loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1qzy2

Elevation: 10 to 50 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Annemessex and similar soils: 60 percent

Dodon and similar soils: 25 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Annemessex

Setting

Landform: Stream terraces, fluviomarine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Concave

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 2 inches: silt loam

E - 2 to 8 inches: silt loam

Bt1 - 8 to 18 inches: silt loam

Bt2 - 18 to 44 inches: loam

BC - 44 to 57 inches: loamy fine sand

2BCg - 57 to 62 inches: loamy very fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high
(0.03 to 1.98 in/hr)

Depth to water table: About 10 to 20 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: B/D

Hydric soil rating: No

Description of Dodon

Setting

Landform: Stream terraces

Landform position (three-dimensional): Interfluve, tread

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 9 inches: fine sandy loam

Bt - 9 to 36 inches: sandy clay loam

BC - 36 to 48 inches: sandy clay loam

CB - 48 to 64 inches: fine sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 2.00 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Elkton, undrained

Percent of map unit: 10 percent

Landform: Depressions on fluviomarine terraces

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: Yes

Quindocqua, undrained

Percent of map unit: 5 percent

Landform: Depressions on fluviomarine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

BaB—Beltsville silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzx2

Elevation: 10 to 400 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Beltsville and similar soils: 70 percent

Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam

E - 3 to 8 inches: silt loam

Bt - 8 to 20 inches: silt loam

Btx - 20 to 41 inches: loam

2B't - 41 to 65 inches: sandy clay loam

2BCg - 65 to 71 inches: very gravelly sandy clay loam

2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: 20 to 40 inches to fragipan

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Custom Soil Resource Report

Hydric soil rating: No

Minor Components

Aquasco

Percent of map unit: 10 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Reybold

Percent of map unit: 10 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

Grosstown

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

BaC—Beltsville silt loam, 5 to 10 percent slopes

Map Unit Setting

National map unit symbol: 1qzx3
Elevation: 10 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Beltsville and similar soils: 70 percent
Minor components: 30 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam

E - 3 to 8 inches: silt loam

Bt - 8 to 20 inches: silt loam

Btx - 20 to 41 inches: loam

2B't - 41 to 65 inches: sandy clay loam

2BCg - 65 to 71 inches: very gravelly sandy clay loam

2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 5 to 10 percent

Depth to restrictive feature: 20 to 40 inches to fragipan

Drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Grosstown

Percent of map unit: 15 percent

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear, convex

Hydric soil rating: No

Reybold

Percent of map unit: 5 percent

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Aquasco

Percent of map unit: 5 percent

Landform: Broad interstream divides

Custom Soil Resource Report

Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Hoghole

Percent of map unit: 5 percent
Landform: Hillslopes
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Convex
Hydric soil rating: No

BcA—Beltsville-Aquasco complex, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1qzww
Elevation: 10 to 360 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Beltsville and similar soils: 50 percent
Aquasco and similar soils: 40 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained

Custom Soil Resource Report

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Hydric soil rating: No

Description of Aquasco

Setting

Landform: Broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 4 inches: silt loam

E - 4 to 10 inches: silt loam

Bt - 10 to 20 inches: silty clay loam

Btx - 20 to 44 inches: loam

BCt - 44 to 72 inches: clay loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 8 to 40 inches to fragipan

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.01 to 0.20 in/hr)

Depth to water table: About 10 to 16 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Hydric soil rating: No

Minor Components

Lenni, undrained

Percent of map unit: 5 percent

Landform: Depressions on broad interstream divides

Hydric soil rating: Yes

Reybold

Percent of map unit: 5 percent

Landform: Fluviomarine terraces, broad interstream divides

Custom Soil Resource Report

Landform position (three-dimensional): Interfluve, tread
Hydric soil rating: No

BgB—Beltsville-Grosstown-Woodstown complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzx7
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Beltsville and similar soils: 35 percent
Grosstown and similar soils: 30 percent
Woodstown and similar soils: 15 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Hydric soil rating: No

Description of Grosstown

Setting

Landform: Swales, depressions, drainhead complexes, broad interstream divides
Landform position (three-dimensional): Tread
Down-slope shape: Linear, concave
Across-slope shape: Convex, concave
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: A
Hydric soil rating: No

Description of Woodstown

Setting

Landform: Depressions, swales, drainageways, drainhead complexes, broad interstream divides
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 8 inches: sandy loam
Bt - 8 to 28 inches: loam
BC - 28 to 42 inches: fine sandy loam
CB - 42 to 60 inches: sandy loam
CBg - 60 to 72 inches: loamy sand

Custom Soil Resource Report

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.20 to 2.00 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 10 percent

Landform: Drainhead complexes, broad interstream divides

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

Issue

Percent of map unit: 5 percent

Landform: Swales, drainageways, drainhead complexes

Down-slope shape: Concave

Across-slope shape: Linear

Hydric soil rating: No

Quindocqua, undrained

Percent of map unit: 5 percent

Landform: Depressions, drainhead complexes

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

GgB—Grosstown gravelly silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzxd

Elevation: 0 to 400 feet

Mean annual precipitation: 40 to 50 inches

Custom Soil Resource Report

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Grosstown and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam

Bt1 - 4 to 20 inches: silt loam

Bt2 - 20 to 26 inches: gravelly loam

2Bt3 - 26 to 71 inches: extremely gravelly silt loam

3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Woodstown

Percent of map unit: 20 percent

Landform: Depressions on broad interstream divides, stream terraces, swales, fluviomarine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Hydric soil rating: No

GmD—Grosstown-Marr-Hoghole complex, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzxb
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Grosstown and similar soils: 31 percent
Marr and similar soils: 29 percent
Hoghole and similar soils: 15 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (two-dimensional): Summit, shoulder, backslope
Landform position (three-dimensional): Interfluve, tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: A

Custom Soil Resource Report

Hydric soil rating: No

Description of Marr

Setting

Landform: Knolls

Landform position (three-dimensional): Side slope, nose slope, head slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: fine sandy loam

Bt1 - 4 to 25 inches: fine sandy loam

Bt2 - 25 to 57 inches: sandy clay loam

BC - 57 to 76 inches: loamy fine sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Hydric soil rating: No

Description of Hoghole

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and gravelly fluviomarine deposits

Typical profile

A - 0 to 4 inches: sand

Bw1 - 4 to 33 inches: very gravelly sand

Bw2 - 33 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (1.98 to 19.98 in/hr)

Depth to water table: More than 80 inches

Custom Soil Resource Report

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Beltsville

Percent of map unit: 10 percent

Landform: Knolls, hillslopes, stream terraces, fluviomarine terraces

Landform position (three-dimensional): Side slope, interfluve, riser

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

Dodon

Percent of map unit: 10 percent

Landform: Stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

Issue

Percent of map unit: 5 percent

Landform: Flood plains, drainageways

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

GmF—Grosstown-Marr-Hoghole complex, 15 to 40 percent slopes

Map Unit Setting

National map unit symbol: 1qzxc

Elevation: 0 to 400 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Grosstown and similar soils: 31 percent

Marr and similar soils: 29 percent

Custom Soil Resource Report

Hoghole and similar soils: 15 percent

Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluvio marine terraces, broad interstream divides

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy and gravelly fluvio marine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam

Bt1 - 4 to 20 inches: silt loam

Bt2 - 20 to 26 inches: gravelly loam

2Bt3 - 26 to 71 inches: extremely gravelly silt loam

3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 15 to 40 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: A

Hydric soil rating: No

Description of Marr

Setting

Landform: Knolls

Landform position (three-dimensional): Side slope, nose slope, head slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy fluvio marine deposits

Typical profile

Ap - 0 to 4 inches: fine sandy loam

Bt1 - 4 to 25 inches: fine sandy loam

Bt2 - 25 to 57 inches: sandy clay loam

BC - 57 to 76 inches: loamy fine sand

Properties and qualities

Slope: 15 to 40 percent

Depth to restrictive feature: More than 80 inches

Custom Soil Resource Report

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.20 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: B

Hydric soil rating: No

Description of Hoghole

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and gravelly fluviomarine deposits

Typical profile

A - 0 to 4 inches: sand

Bw1 - 4 to 33 inches: very gravelly sand

Bw2 - 33 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 15 to 40 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): High to very high (1.98 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Potobac

Percent of map unit: 10 percent

Landform: Flood plains, drainageways

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: Yes

Dodon

Percent of map unit: 10 percent

Custom Soil Resource Report

Landform: Stream terraces
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Beltsville

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Side slope, interfluvium
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Hydric soil rating: No

GwD—Grosstown-Woodstown-Beltsville complex, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzx8
Elevation: 0 to 400 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: Not prime farmland

Map Unit Composition

Grosstown and similar soils: 31 percent
Woodstown and similar soils: 29 percent
Beltsville and similar soils: 20 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (three-dimensional): Interfluvium, tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: A
Hydric soil rating: No

Description of Woodstown

Setting

Landform: Swales, depressions, interfluves, broad interstream divides, fluviomarine terraces, drainhead complexes
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread
Down-slope shape: Linear, concave
Across-slope shape: Concave, linear
Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 8 inches: sandy loam
Bt - 8 to 28 inches: loam
BC - 28 to 42 inches: fine sandy loam
CB - 42 to 60 inches: sandy loam
CBg - 60 to 72 inches: loamy sand

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Hydric soil rating: No

Description of Beltsville

Setting

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Parent material: Silty eolian deposits over loamy fluviomarine deposits

Typical profile

A - 0 to 3 inches: silt loam
E - 3 to 8 inches: silt loam
Bt - 8 to 20 inches: silt loam
Btx - 20 to 41 inches: loam
2B't - 41 to 65 inches: sandy clay loam
2BCg - 65 to 71 inches: very gravelly sandy clay loam
2CB - 71 to 76 inches: gravelly coarse sandy loam

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: 20 to 40 inches to fragipan
Drainage class: Moderately well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 10 percent
Landform: Hillslopes, drainhead complexes
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Convex
Hydric soil rating: No

Issue

Percent of map unit: 5 percent
Landform: Flood plains, drainageways, drainhead complexes
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Lenni, undrained

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

HgB—Hoghole-Grosstown complex, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwm

Elevation: 0 to 400 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Prime farmland if irrigated

Map Unit Composition

Hoghole and similar soils: 45 percent

Grosstown and similar soils: 30 percent

Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hoghole

Setting

Landform: Stream terraces, fluvio-marine terraces, broad interstream divides

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and gravelly fluvio-marine deposits

Typical profile

A - 0 to 4 inches: sand

Bw1 - 4 to 33 inches: very gravelly sand

Bw2 - 33 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (1.98 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Custom Soil Resource Report

Hydrologic Soil Group: A
Hydric soil rating: No

Description of Grosstown

Setting

Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Loamy and gravelly fluviomarine deposits

Typical profile

Ap - 0 to 4 inches: gravelly silt loam
Bt1 - 4 to 20 inches: silt loam
Bt2 - 20 to 26 inches: gravelly loam
2Bt3 - 26 to 71 inches: extremely gravelly silt loam
3BC - 71 to 80 inches: extremely gravelly coarse sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: A
Hydric soil rating: No

Minor Components

Reybold

Percent of map unit: 15 percent
Landform: Stream terraces, fluviomarine terraces, broad interstream divides
Landform position (three-dimensional): Interfluve, tread
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Woodstown

Percent of map unit: 10 percent
Landform: Depressions, stream terraces, swales, broad interstream divides, fluviomarine terraces
Landform position (three-dimensional): Tread
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: No

Is—Issue silt loam, occasionally flooded

Map Unit Setting

National map unit symbol: 1qzxg

Elevation: 0 to 250 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Issue and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Issue

Setting

Landform: Flood plains, drainageways

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy alluvium

Typical profile

Ap - 0 to 4 inches: silt loam

Bw - 4 to 19 inches: loam

Bg1 - 19 to 30 inches: fine sandy loam

Bg2 - 30 to 58 inches: fine sandy loam

Ab - 58 to 70 inches: silt loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 2.00 in/hr)

Depth to water table: About 10 to 20 inches

Frequency of flooding: Occasional

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Hydric soil rating: No

Minor Components

Woodstown

Percent of map unit: 10 percent

Landform: Depressions, drainageways, swales

Hydric soil rating: No

Potobac

Percent of map unit: 10 percent

Landform: Flood plains, drainageways

Hydric soil rating: Yes

LQA—Lenni and Quindocqua soils, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1qzxk

Elevation: 10 to 360 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Lenni, undrained, and similar soils: 50 percent

Quindocqua, undrained, and similar soils: 30 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lenni, Undrained

Setting

Landform: Depressions on broad interstream divides, fluviomarine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Parent material: Clayey fluviomarine deposits

Typical profile

A - 0 to 6 inches: silt loam

Eg - 6 to 9 inches: silt loam

Btg1 - 9 to 26 inches: silty clay loam

Btg2 - 26 to 49 inches: clay

2Cg - 49 to 54 inches: loamy sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: High

Custom Soil Resource Report

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.60 in/hr)

Depth to water table: About 0 to 10 inches

Frequency of flooding: None

Frequency of ponding: Occasional

Available water supply, 0 to 60 inches: Moderate (about 7.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: C/D

Hydric soil rating: Yes

Description of Quindocqua, Undrained

Setting

Landform: Depressions on broad interstream divides, fluvio-marine terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Typical profile

Oi - 0 to 4 inches: slightly decomposed plant material

A - 4 to 11 inches: loam

Btg - 11 to 33 inches: loam

2BCg - 33 to 59 inches: very fine sandy loam

2CBg - 59 to 64 inches: very fine sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)

Depth to water table: About 0 to 10 inches

Frequency of flooding: None

Frequency of ponding: Occasional

Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Hydric soil rating: Yes

Minor Components

Annemessex

Percent of map unit: 10 percent

Landform: Stream terraces, fluvio-marine terraces, broad interstream divides

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Concave

Hydric soil rating: No

Beltsville

Percent of map unit: 5 percent

Custom Soil Resource Report

Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex, linear
Across-slope shape: Convex, linear
Hydric soil rating: No

Liverpool

Percent of map unit: 5 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

LsB—Liverpool silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzy0
Elevation: 0 to 210 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 57 degrees F
Frost-free period: 180 to 210 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Liverpool and similar soils: 75 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Liverpool

Setting

Landform: Terraces
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Silty and loamy fluviomarine deposits

Typical profile

A - 0 to 2 inches: silt loam
E - 2 to 5 inches: silt loam
Bt1 - 5 to 13 inches: silt loam
Bt2 - 13 to 35 inches: clay loam
Btg - 35 to 64 inches: sandy clay loam
BC - 64 to 74 inches: sandy clay loam

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained

Custom Soil Resource Report

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.60 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: D

Hydric soil rating: No

Minor Components

Piccowaxen

Percent of map unit: 10 percent

Landform position (three-dimensional): Tread

Down-slope shape: Concave

Across-slope shape: Linear

Hydric soil rating: No

Annemessex

Percent of map unit: 10 percent

Landform: Fluvio-marine terraces

Landform position (three-dimensional): Tread

Hydric soil rating: No

Elkton, undrained

Percent of map unit: 5 percent

Landform: Depressions

Landform position (three-dimensional): Tread

Hydric soil rating: Yes

PT—Pits, gravel

Map Unit Composition

Pits, gravel: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Pu—Potobac-Issue complex, frequently flooded

Map Unit Setting

National map unit symbol: 1qzxf

Elevation: 0 to 250 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 58 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Potobac and similar soils: 70 percent

Issue and similar soils: 25 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Potobac

Setting

Landform: Flood plains

Down-slope shape: Linear

Across-slope shape: Linear

Typical profile

A - 0 to 8 inches: loam

Bg - 8 to 17 inches: loam

Cg1 - 17 to 39 inches: sandy loam

Cg2 - 39 to 59 inches: very gravelly coarse sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)

Depth to water table: About 0 to 10 inches

Frequency of flooding: Frequent

Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Hydric soil rating: Yes

Description of Issue

Setting

Landform: Flood plains

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Loamy alluvium

Typical profile

Ap - 0 to 4 inches: silt loam

Bw - 4 to 19 inches: loam

Bg1 - 19 to 30 inches: fine sandy loam

Bg2 - 30 to 58 inches: fine sandy loam

Ab - 58 to 70 inches: silt loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Custom Soil Resource Report

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 2.00 in/hr)

Depth to water table: About 10 to 20 inches

Frequency of flooding: Occasional

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 9.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Hydric soil rating: No

Minor Components

Lenni, undrained

Percent of map unit: 5 percent

Landform: Depressions on fluviomarine terraces

Landform position (three-dimensional): Tread

Hydric soil rating: Yes

UdB—Udorthents, loamy, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1qzwn

Elevation: 0 to 300 feet

Mean annual precipitation: 40 to 50 inches

Mean annual air temperature: 52 to 57 degrees F

Frost-free period: 180 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Setting

Landform: Broad interstream divides

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Fluviomarine deposits

Typical profile

AC - 0 to 2 inches: loam

C - 2 to 72 inches: gravelly loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very high (0.01 to 19.98 in/hr)
Depth to water table: About 40 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Urban land

Percent of map unit: 7 percent
Landform: Flats
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: Unranked

Beltsville

Percent of map unit: 3 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

UdD—Udorthents, loamy, 5 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1qzwp
Elevation: 0 to 300 feet
Mean annual precipitation: 40 to 50 inches
Mean annual air temperature: 52 to 58 degrees F
Frost-free period: 175 to 220 days
Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 90 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Setting

Landform: Broad interstream divides
Down-slope shape: Linear, convex
Across-slope shape: Linear
Parent material: Fluvio-marine deposits

Typical profile

AC - 0 to 2 inches: loam
C - 2 to 72 inches: gravelly loam

Properties and qualities

Slope: 5 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very high (0.01 to 19.98 in/hr)
Depth to water table: About 40 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Urban land

Percent of map unit: 7 percent
Landform: Flats
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: Unranked

Beltsville

Percent of map unit: 3 percent
Landform: Broad interstream divides
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

WdaA—Woodstown sandy loam, 0 to 2 percent slopes, Northern Coastal Plain

Map Unit Setting

National map unit symbol: 2thvw

Elevation: 0 to 280 feet

Mean annual precipitation: 42 to 48 inches

Mean annual air temperature: 52 to 58 degrees F

Frost-free period: 180 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Woodstown and similar soils: 81 percent

Minor components: 19 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodstown

Setting

Landform: Depressions, flats, fluviomarine terraces, broad interstream divides

Landform position (two-dimensional): Footslope, summit

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 7 inches: sandy loam

E - 7 to 11 inches: sandy loam

Bt - 11 to 29 inches: sandy loam

BCg - 29 to 45 inches: fine sandy loam

Cg - 45 to 80 inches: loamy sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)

Depth to water table: About 20 to 40 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Fallsington

Percent of map unit: 7 percent
Landform: Drainageways, depressions, swales, flats
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Dip, talf
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: Yes

Hammonton

Percent of map unit: 7 percent
Landform: Flats, broad interstream divides
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Hambrook

Percent of map unit: 5 percent
Landform: Flats, fluviomarine terraces
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Tread, talf
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

WdaB—Woodstown sandy loam, 2 to 5 percent slopes, Northern Coastal Plain

Map Unit Setting

National map unit symbol: 2thvx
Elevation: 0 to 490 feet
Mean annual precipitation: 42 to 48 inches
Mean annual air temperature: 52 to 58 degrees F
Frost-free period: 180 to 220 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Woodstown and similar soils: 81 percent
Minor components: 19 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodstown

Setting

Landform: Flats, depressions, fluviomarine terraces, broad interstream divides
Landform position (two-dimensional): Shoulder, footslope

Custom Soil Resource Report

Landform position (three-dimensional): Riser, dip
Down-slope shape: Convex, concave
Across-slope shape: Linear, concave
Parent material: Loamy fluviomarine deposits

Typical profile

Ap - 0 to 7 inches: sandy loam
E - 7 to 11 inches: sandy loam
Bt - 11 to 29 inches: sandy loam
BCg - 29 to 45 inches: fine sandy loam
Cg - 45 to 80 inches: loamy sand

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.57 to 1.98 in/hr)
Depth to water table: About 20 to 40 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Hydric soil rating: No

Minor Components

Hammonton

Percent of map unit: 7 percent
Landform: Flats, broad interstream divides
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Dip
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

Fallsington, occasionally ponded

Percent of map unit: 7 percent
Landform: Drainageways, depressions, swales, flats
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Dip, tal
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: Yes

Hambrook

Percent of map unit: 5 percent
Landform: Flats, fluviomarine terraces
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Riser, dip
Down-slope shape: Convex
Across-slope shape: Linear

Custom Soil Resource Report

Hydric soil rating: No

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Attachment 5

HYDROLOGIC ANALYSIS





NOAA Atlas 14, Volume 2, Version 3
Location name: Port Tobacco, Maryland, USA*
Latitude: 38.5079°, Longitude: -77.0678°
Elevation: 156.5 ft**

* source: ESRI Maps

** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.364 (0.330-0.401)	0.437 (0.397-0.481)	0.520 (0.471-0.572)	0.580 (0.524-0.638)	0.656 (0.589-0.723)	0.713 (0.637-0.786)	0.770 (0.684-0.851)	0.825 (0.728-0.915)	0.897 (0.783-1.00)	0.953 (0.825-1.07)
10-min	0.582 (0.527-0.640)	0.700 (0.634-0.769)	0.832 (0.754-0.916)	0.927 (0.838-1.02)	1.05 (0.939-1.15)	1.14 (1.01-1.25)	1.22 (1.09-1.35)	1.31 (1.15-1.45)	1.42 (1.24-1.58)	1.50 (1.30-1.68)
15-min	0.728 (0.659-0.800)	0.879 (0.797-0.967)	1.05 (0.954-1.16)	1.17 (1.06-1.29)	1.33 (1.19-1.46)	1.44 (1.29-1.59)	1.55 (1.37-1.71)	1.65 (1.46-1.83)	1.79 (1.56-1.99)	1.88 (1.63-2.11)
30-min	0.998 (0.904-1.10)	1.22 (1.10-1.34)	1.50 (1.36-1.65)	1.70 (1.54-1.87)	1.96 (1.76-2.16)	2.17 (1.94-2.39)	2.37 (2.11-2.62)	2.57 (2.27-2.85)	2.84 (2.48-3.17)	3.05 (2.64-3.42)
60-min	1.24 (1.13-1.37)	1.52 (1.38-1.68)	1.92 (1.74-2.11)	2.21 (2.00-2.44)	2.61 (2.35-2.88)	2.93 (2.62-3.24)	3.26 (2.90-3.60)	3.60 (3.18-4.00)	4.08 (3.56-4.55)	4.45 (3.86-4.99)
2-hr	1.46 (1.32-1.61)	1.78 (1.61-1.97)	2.25 (2.04-2.49)	2.62 (2.36-2.89)	3.14 (2.81-3.47)	3.57 (3.17-3.94)	4.01 (3.54-4.44)	4.48 (3.93-4.97)	5.15 (4.46-5.74)	5.69 (4.88-6.38)
3-hr	1.58 (1.42-1.76)	1.92 (1.73-2.14)	2.44 (2.19-2.71)	2.84 (2.54-3.16)	3.42 (3.04-3.81)	3.90 (3.44-4.34)	4.41 (3.86-4.91)	4.95 (4.30-5.53)	5.73 (4.91-6.43)	6.38 (5.39-7.19)
6-hr	1.94 (1.75-2.17)	2.35 (2.12-2.63)	2.97 (2.67-3.32)	3.48 (3.11-3.88)	4.22 (3.75-4.71)	4.86 (4.27-5.41)	5.54 (4.83-6.19)	6.29 (5.41-7.04)	7.39 (6.26-8.32)	8.32 (6.94-9.41)
12-hr	2.34 (2.10-2.64)	2.83 (2.54-3.19)	3.60 (3.22-4.04)	4.25 (3.78-4.77)	5.24 (4.61-5.87)	6.10 (5.31-6.84)	7.06 (6.07-7.93)	8.13 (6.90-9.15)	9.76 (8.11-11.0)	11.2 (9.13-12.7)
24-hr	2.67 (2.41-3.01)	3.24 (2.93-3.65)	4.20 (3.80-4.73)	5.04 (4.54-5.66)	6.31 (5.64-7.06)	7.43 (6.59-8.29)	8.70 (7.65-9.67)	10.1 (8.82-11.2)	12.3 (10.6-13.6)	14.2 (12.0-15.7)
2-day	3.07 (2.76-3.45)	3.73 (3.35-4.19)	4.83 (4.34-5.42)	5.77 (5.17-6.48)	7.20 (6.41-8.04)	8.45 (7.47-9.41)	9.84 (8.62-11.0)	11.4 (9.90-12.7)	13.8 (11.8-15.3)	15.8 (13.4-17.6)
3-day	3.25 (2.94-3.65)	3.95 (3.56-4.43)	5.09 (4.59-5.70)	6.07 (5.45-6.79)	7.54 (6.73-8.41)	8.82 (7.83-9.82)	10.2 (9.01-11.4)	11.8 (10.3-13.1)	14.2 (12.3-15.8)	16.3 (13.9-18.1)
4-day	3.44 (3.11-3.85)	4.17 (3.77-4.66)	5.36 (4.84-5.99)	6.37 (5.73-7.11)	7.89 (7.05-8.78)	9.20 (8.18-10.2)	10.7 (9.40-11.8)	12.3 (10.7-13.6)	14.7 (12.7-16.3)	16.8 (14.4-18.6)
7-day	3.99 (3.64-4.39)	4.81 (4.40-5.30)	6.08 (5.57-6.70)	7.17 (6.54-7.88)	8.78 (7.97-9.65)	10.2 (9.17-11.1)	11.7 (10.5-12.8)	13.4 (11.9-14.6)	15.8 (13.9-17.3)	18.0 (15.6-19.7)
10-day	4.56 (4.19-4.98)	5.47 (5.04-5.98)	6.82 (6.28-7.45)	7.95 (7.30-8.67)	9.58 (8.75-10.4)	10.9 (9.95-11.9)	12.4 (11.2-13.5)	14.0 (12.6-15.2)	16.3 (14.5-17.7)	18.2 (16.0-19.8)
20-day	6.12 (5.70-6.60)	7.28 (6.78-7.85)	8.81 (8.19-9.50)	10.0 (9.32-10.8)	11.8 (10.9-12.7)	13.2 (12.1-14.1)	14.6 (13.4-15.7)	16.1 (14.7-17.3)	18.2 (16.5-19.5)	19.9 (17.9-21.4)
30-day	7.55 (7.05-8.09)	8.94 (8.35-9.58)	10.6 (9.94-11.4)	12.0 (11.2-12.9)	13.9 (12.9-14.8)	15.3 (14.2-16.4)	16.8 (15.6-18.0)	18.4 (16.9-19.7)	20.5 (18.7-21.9)	22.1 (20.1-23.7)
45-day	9.48 (8.90-10.1)	11.2 (10.5-11.9)	13.1 (12.3-13.9)	14.6 (13.7-15.5)	16.5 (15.4-17.5)	18.0 (16.8-19.1)	19.4 (18.1-20.6)	20.8 (19.4-22.1)	22.6 (21.0-24.1)	24.0 (22.1-25.6)
60-day	11.3 (10.6-11.9)	13.3 (12.5-14.0)	15.4 (14.5-16.2)	16.9 (15.9-17.9)	18.9 (17.8-20.0)	20.4 (19.1-21.5)	21.8 (20.4-23.0)	23.1 (21.6-24.5)	24.8 (23.1-26.3)	26.0 (24.2-27.6)

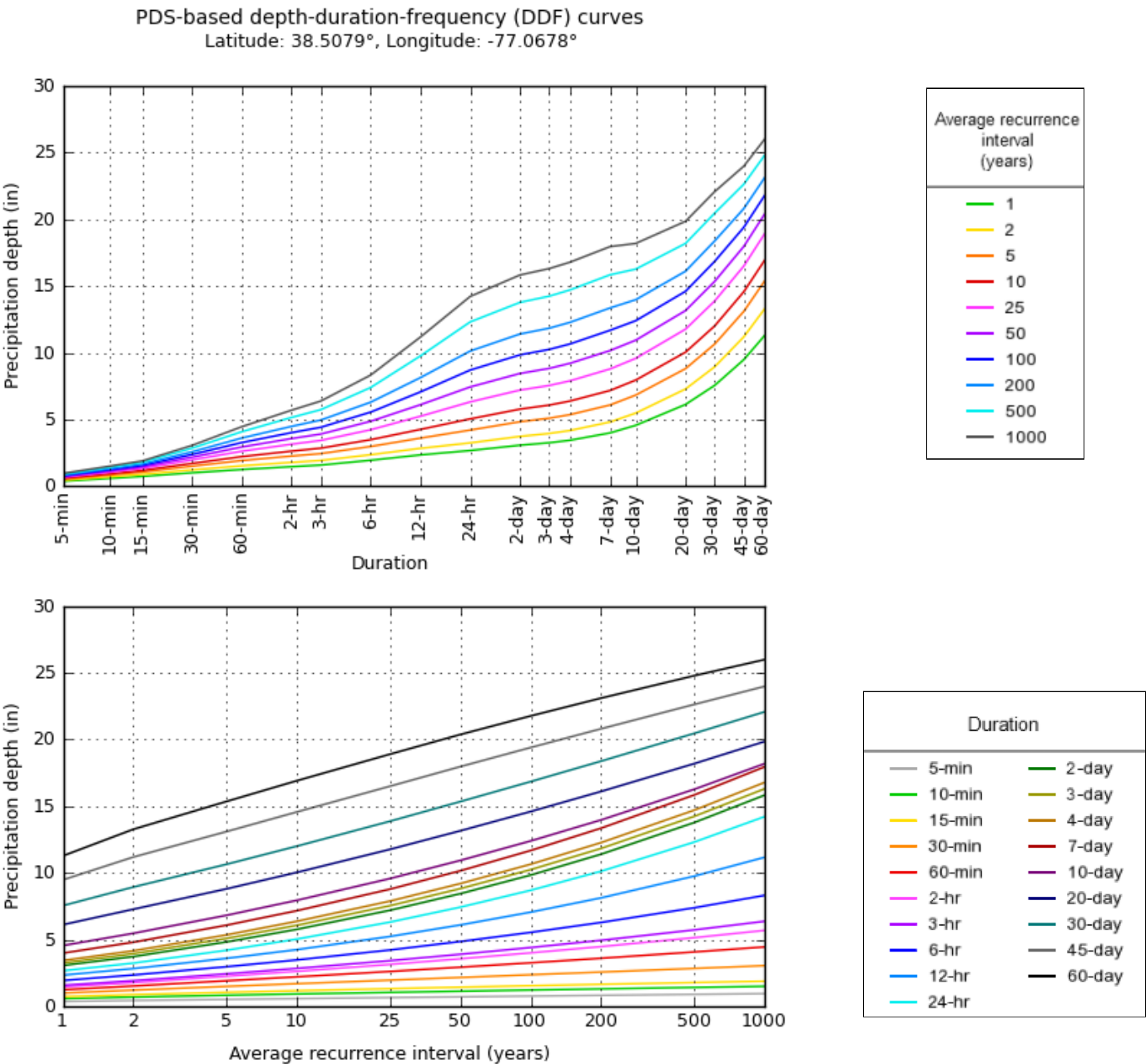
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical



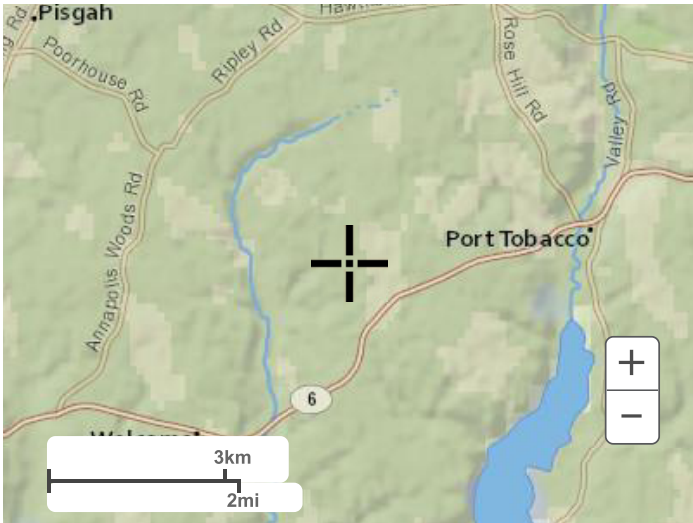
NOAA Atlas 14, Volume 2, Version 3

Created (GMT): Tue Nov 15 21:38:35 2022

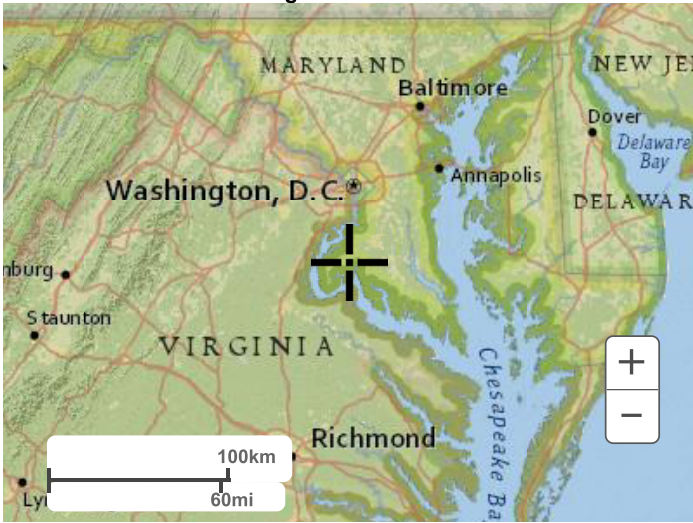
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Maps & aerials

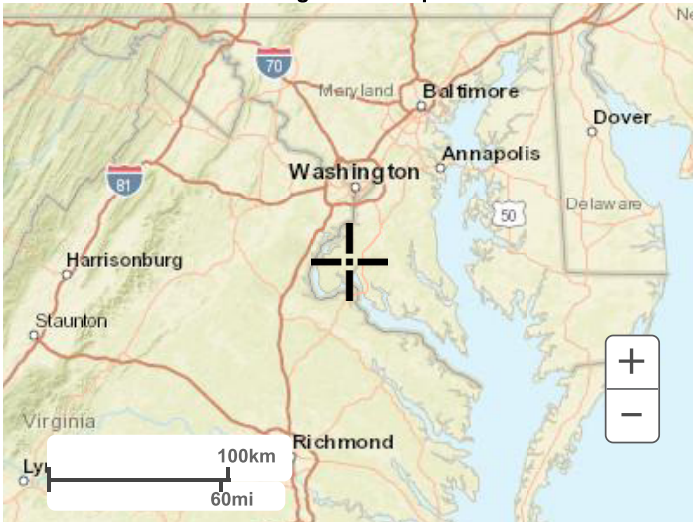
Small scale terrain



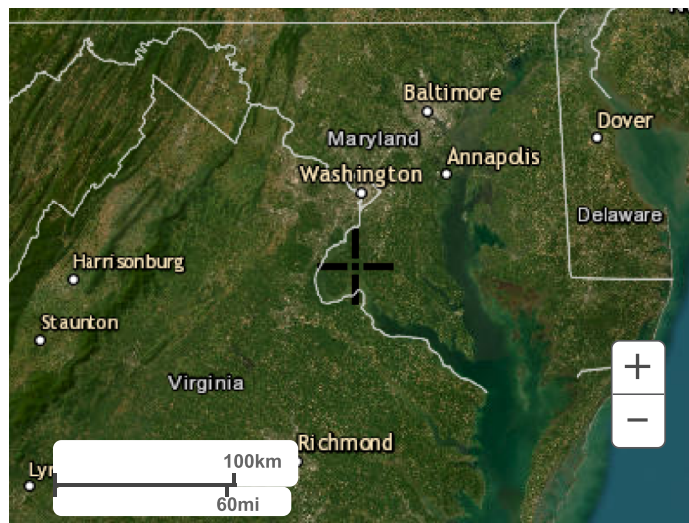
Large scale terrain



Large scale map



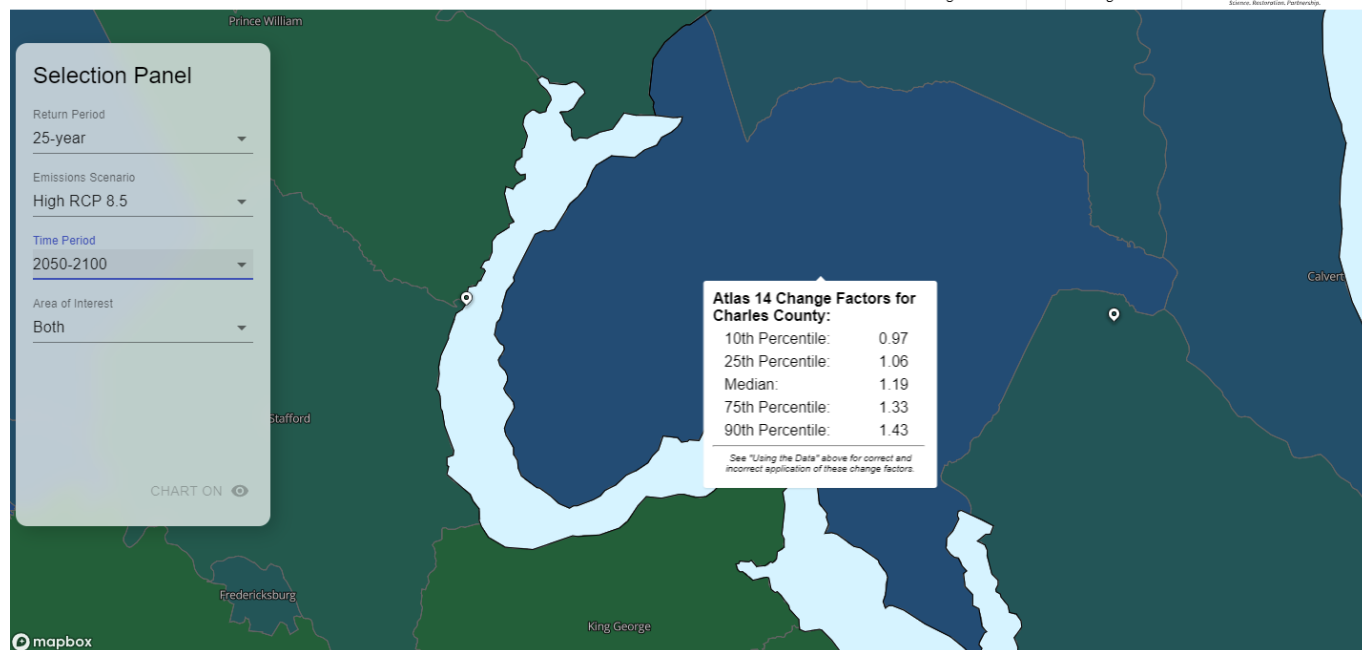
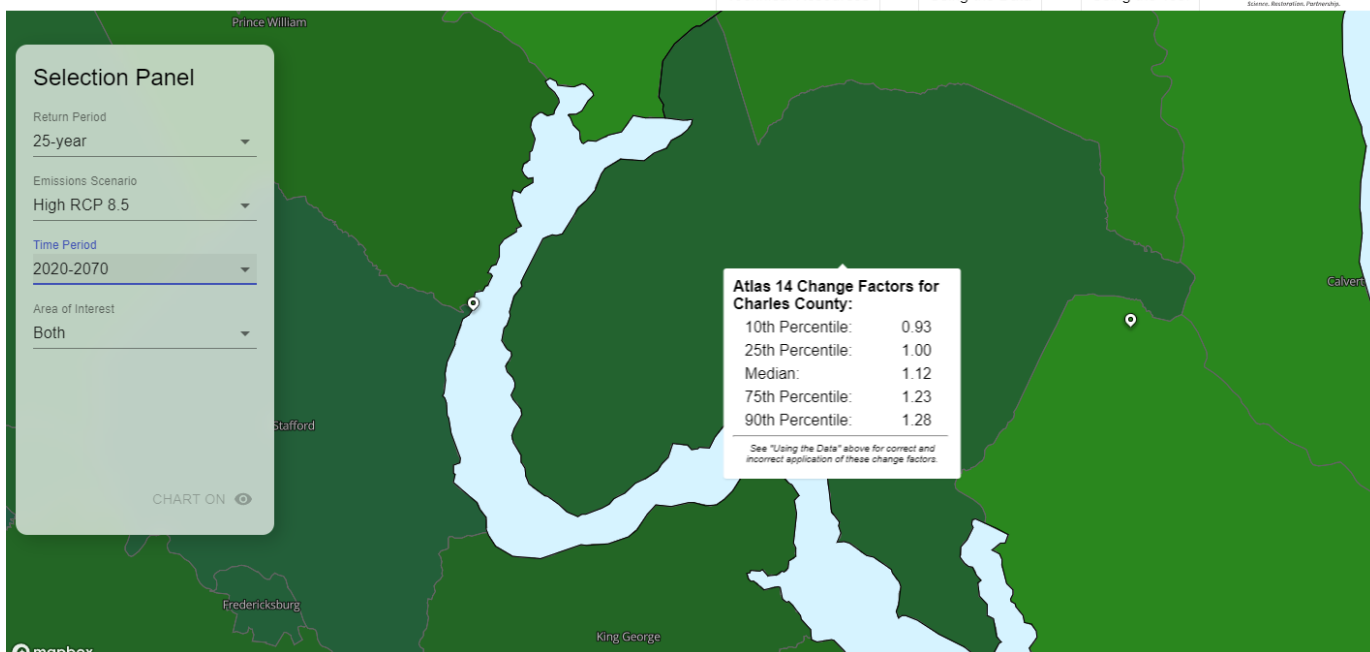
Large scale aerial

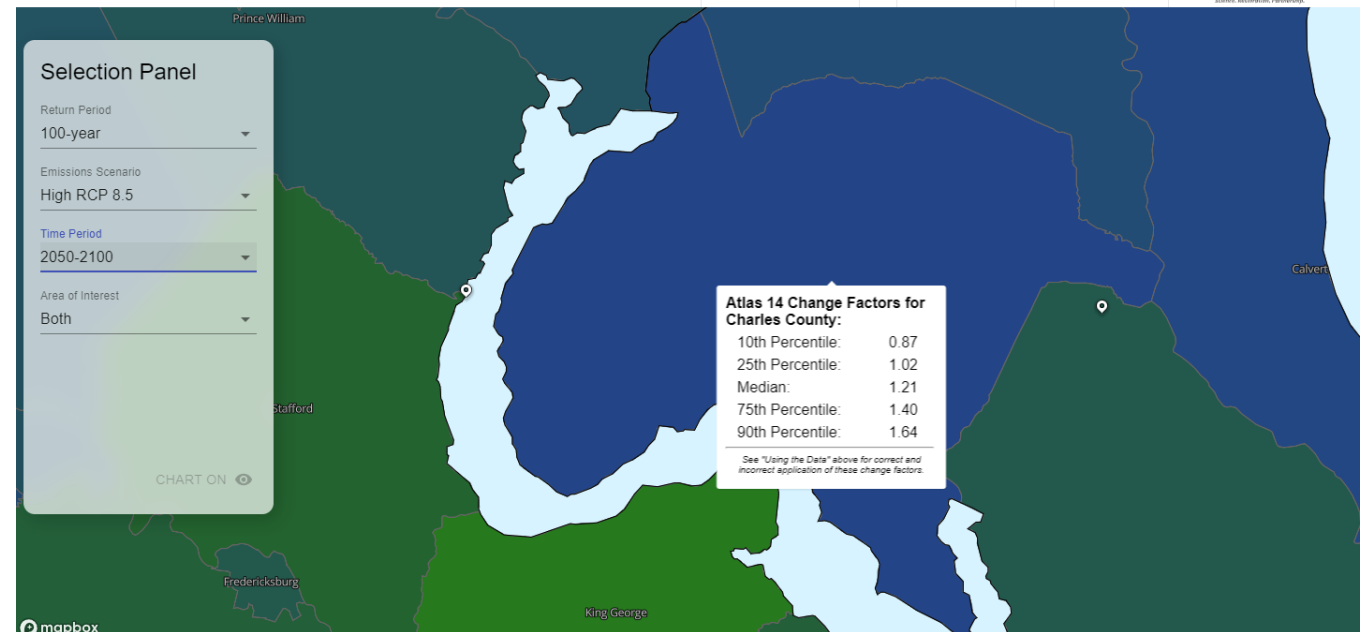
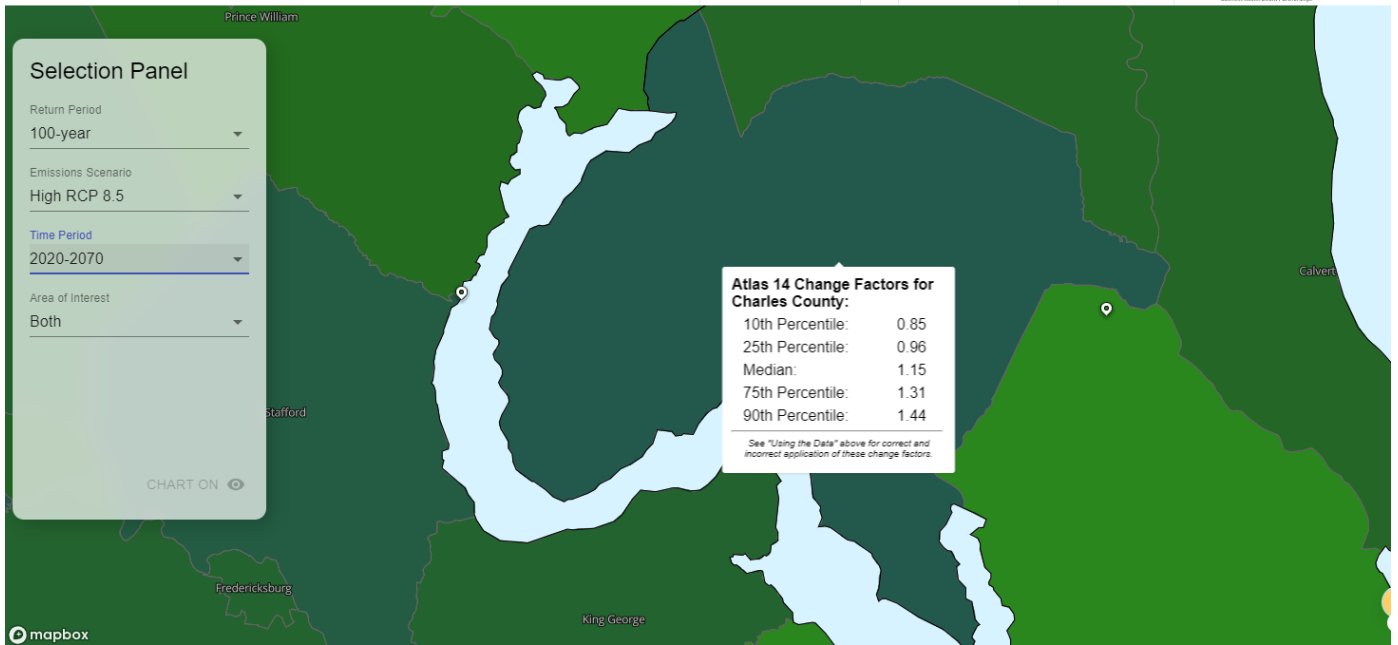


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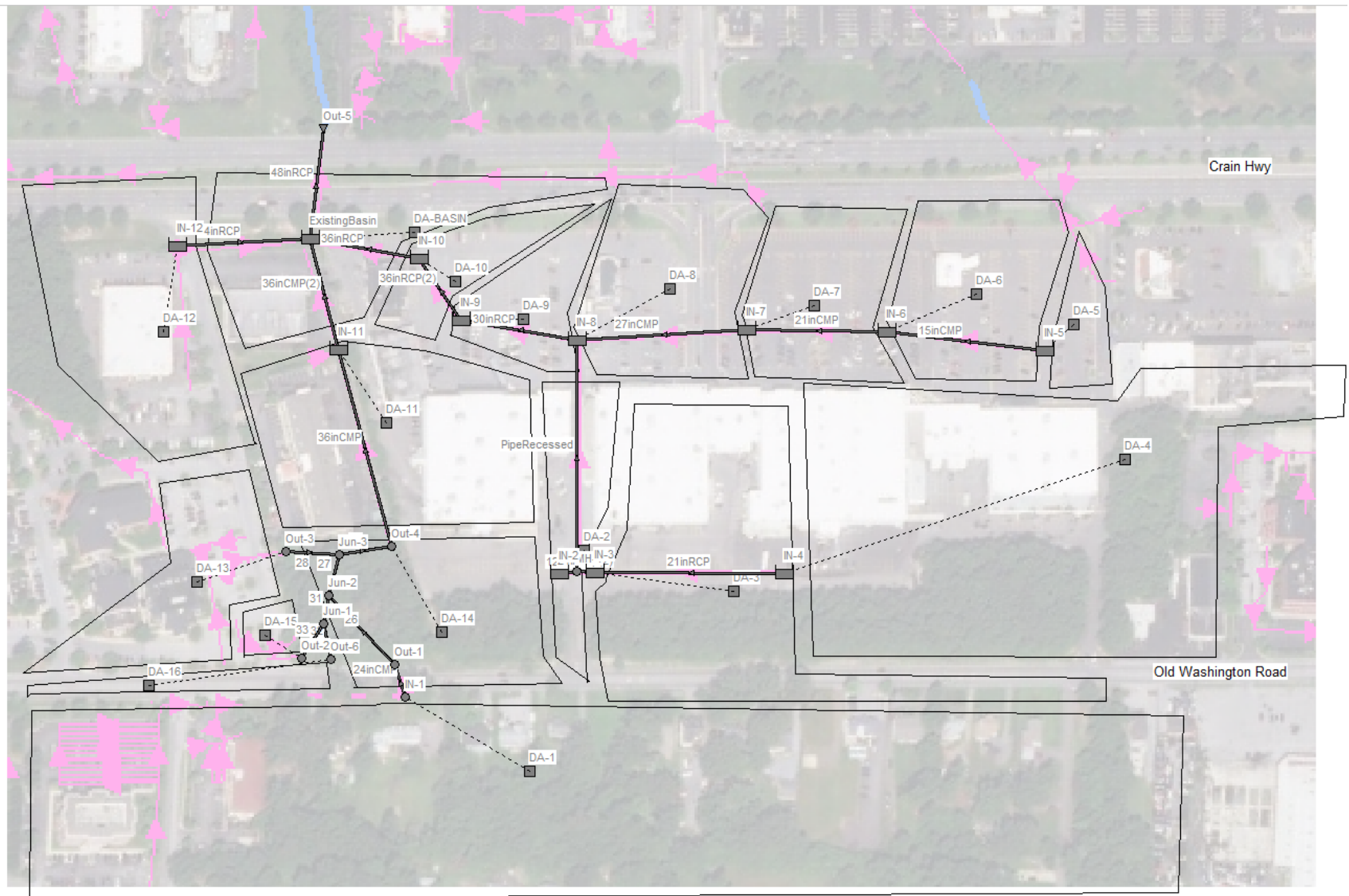
Attachment 6

HYDRAULIC ANALYSIS



Location 10: Old Washington Rd. and Shoppers World SWMM Schematic

DesignStorms



Location 10: Old Washington Rd. and Shoppers World (25-Year - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	54.673	6.303
Evaporation Loss	0.000	0.000
Infiltration Loss	6.531	0.753
Surface Runoff	47.470	5.473
Final Storage	0.758	0.087
Continuity Error (%)	-0.158	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	47.472	15.469
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	47.429	15.455
Flooding Loss	0.020	0.006
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.030	0.010
Continuity Error (%)	-0.015	

Time-Step Critical Elements

Link 24inRcp(2) (62.94%)

Link 12inRCP (27.87%)

Link 27 (5.27%)

Link 36inCMP (2.44%)


```

*****
Highest Flow Instability Indexes
*****
Link 12inRCP (15)
Link 24inRcp(2) (12)
Link PipeRecessed (7)
Link 31 (1)
Link 33 (1)

```

```

*****
Most Frequent Nonconverging Nodes
*****
Node Out-5 (0.04%)
Node IN-2 (0.02%)
Node IN-1 (0.01%)
Node MH-1 (0.01%)
Node IN-4 (0.01%)

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      :    0.50 sec
Average Time Step      :    3.71 sec
Maximum Time Step      :   20.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.04
% of Steps Not Converging :    0.04
Time Step Frequencies  :
    20.000 - 9.564 sec :    0.21 %
    9.564 - 4.573 sec :   18.50 %
    4.573 - 2.187 sec :   70.93 %
    2.187 - 1.046 sec :    9.27 %
    1.046 - 0.500 sec :    1.10 %

```

```

*****
Subcatchment Runoff Summary
*****

```

			Total	Total	Total	Total	Imperv
			Perv	Total	Total	Peak	Runoff
			Precip	Runon	Evap	Infil	Runoff
			Runoff	Runoff	Runoff	Runoff	Coeff
Subcatchment		in	in	in	in	in	in
in	in	10^6 gal	CFS				

DA-1			6.30	0.00	0.00	0.89	3.19
2.11	5.30		9.30	231.68	0.841		
DA-2			6.30	0.00	0.00	0.15	5.72
0.42	6.13		0.18	9.22	0.973		
DA-3			6.30	0.00	0.00	1.24	1.57
3.44	5.01		0.65	22.50	0.795		
DA-4			6.30	0.00	0.00	0.51	4.33
1.42	5.75		1.38	53.53	0.913		
DA-5			6.30	0.00	0.00	0.02	6.21
0.05	6.26		0.10	4.94	0.993		
DA-6			6.30	0.00	0.00	0.11	5.84
0.32	6.17		0.35	17.38	0.979		
DA-7			6.30	0.00	0.00	0.18	5.59
0.51	6.10		0.28	13.96	0.968		
DA-8			6.30	0.00	0.00	0.16	5.66

	0.46	6.12	0.40	20.16	0.971			
125	DA-9		6.30		0.00	0.00	0.11	5.84
	0.32	6.17	0.24	12.44	0.979			
126	DA-10		6.30		0.00	0.00	0.28	5.22
	0.79	6.00	0.13	6.52	0.952			
127	DA-11		6.30		0.00	0.00	0.18	5.59
	0.51	6.10	0.69	34.10	0.968			
128	DA-12		6.30		0.00	0.00	0.58	4.08
	1.62	5.70	0.55	26.24	0.904			
129	DA-13		6.30		0.00	0.00	0.40	5.28
	0.60	5.88	0.27	13.61	0.933			
130	DA-14		6.30		0.00	0.00	1.26	2.14
	2.87	5.01	0.39	15.82	0.795			
131	DA-15		6.30		0.00	0.00	0.31	5.08
	0.88	5.96	0.05	2.40	0.946			
132	DA-16		6.30		0.00	0.00	0.45	4.59
	1.25	5.83	0.08	3.60	0.925			
133	DA-BASIN		6.30		0.00	0.00	0.44	4.59
	1.25	5.84	0.43	21.48	0.926			

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	0.95	4.28	207.02	0 12:22	4.27
Out-4	JUNCTION	3.21	6.64	205.15	0 12:14	6.64
IN-1	JUNCTION	2.87	5.46	206.56	0 14:13	5.46
Out-1	JUNCTION	1.69	4.17	205.17	0 12:14	4.17
Out-3	JUNCTION	0.52	2.55	205.16	0 12:14	2.55
Out-6	JUNCTION	0.78	3.16	205.16	0 12:14	3.16
Out-2	JUNCTION	0.78	3.16	205.16	0 12:14	3.16
Jun-1	JUNCTION	1.44	4.16	205.16	0 12:14	4.16
Jun-2	JUNCTION	1.54	4.26	205.16	0 12:14	4.26
Jun-3	JUNCTION	1.69	4.76	205.16	0 12:14	4.76
Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
IN-2	STORAGE	0.60	4.18	207.28	0 12:06	4.13
IN-3	STORAGE	0.94	4.39	207.15	0 12:19	4.39
ExistingBasin	STORAGE	0.92	3.16	201.36	0 12:01	3.10
IN-4	STORAGE	0.80	5.00	208.12	0 12:26	5.00
IN-12	STORAGE	0.19	1.84	204.74	0 12:00	1.82
IN-11	STORAGE	2.08	4.47	203.10	0 12:09	4.43
IN-10	STORAGE	0.50	2.81	202.98	0 12:00	2.79
IN-9	STORAGE	0.69	3.39	203.77	0 12:00	3.38
IN-8	STORAGE	0.49	3.76	206.03	0 12:00	3.73
IN-5	STORAGE	0.21	4.15	211.44	0 12:06	4.11
IN-6	STORAGE	0.35	4.38	210.15	0 12:10	4.37
IN-7	STORAGE	0.37	4.27	208.12	0 12:06	4.19

Node Inflow Summary

Node	Type	Maximum Total Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
------	------	---	---	--	---	------

	gal	Percent						
179	-----							

180	MH-1		JUNCTION	0.00	26.33	0	12:02	0
	2.23	-0.054						
181	Out-4		JUNCTION	15.82	44.91	0	12:00	0.393
	10.1	0.038						
182	IN-1		JUNCTION	231.68	231.68	0	12:05	9.3
	9.3	-0.005						
183	Out-1		JUNCTION	0.00	27.96	0	11:38	0
	9.31	0.010						
184	Out-3		JUNCTION	13.61	13.61	0	12:00	0.272
	0.272	-0.005						
185	Out-6		JUNCTION	3.60	3.60	0	12:00	0.076
	0.0765	0.012						
186	Out-2		JUNCTION	2.40	2.40	0	12:00	0.0453
	0.0458	0.049						
187	Jun-1		JUNCTION	0.00	8.36	0	22:37	0
	0.126	0.166						
188	Jun-2		JUNCTION	0.00	27.89	0	11:40	0
	9.43	0.011						
189	Jun-3		JUNCTION	0.00	31.77	0	12:00	0
	9.7	-0.007						
190	Out-5		OUTFALL	0.00	143.11	0	12:01	0
	15.5	0.000						
191	IN-2		STORAGE	9.22	9.22	0	12:00	0.182
	0.204	0.115						
192	IN-3		STORAGE	22.50	30.40	0	12:00	0.652
	2.02	0.008						
193	ExistingBasin		STORAGE	21.48	145.48	0	12:00	0.431
	15.5	0.004						
194	IN-4		STORAGE	53.53	53.53	0	12:00	1.38
	1.38	0.047						
195	IN-12		STORAGE	26.24	26.24	0	12:00	0.549
	0.549	0.003						
196	IN-11		STORAGE	34.10	56.30	0	12:00	0.686
	10.8	0.008						
197	IN-10		STORAGE	6.52	62.96	0	12:00	0.129
	3.7	0.001						
198	IN-9		STORAGE	12.44	56.60	0	12:00	0.245
	3.58	-0.005						
199	IN-8		STORAGE	20.16	44.92	0	12:00	0.402
	3.33	0.013						
200	IN-5		STORAGE	4.94	4.94	0	12:00	0.0952
	0.0952	0.034						
201	IN-6		STORAGE	17.38	19.82	0	12:00	0.353
	0.449	0.114						
202	IN-7		STORAGE	13.96	21.76	0	12:00	0.275
	0.723	-0.037						

203
204
205 *****

206 Node Surcharge Summary
207 *****

208
209 Surcharging occurs when water rises above the top of the highest conduit.
210 -----

			Hours	Max. Height	Min. Depth
			Surcharged	Above Crown	Below Rim
	Node	Type		Feet	Feet
211	-----				
212					
213					
214	-----				
215	MH-1	JUNCTION	2.81	2.282	0.000
216	Out-4	JUNCTION	11.27	2.639	0.000
217	IN-1	JUNCTION	11.84	3.459	0.000
218	Out-1	JUNCTION	0.45	0.175	0.825
219	Jun-1	JUNCTION	0.43	0.164	0.836
220	Jun-2	JUNCTION	0.57	0.264	0.736
221	Jun-3	JUNCTION	1.17	0.758	0.242

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
MH-1	1.60	15.17	0 12:00	0.106	0.282
Out-4	11.27	22.30	0 12:00	0.216	2.639
IN-1	10.94	212.65	0 12:05	3.429	0.459
IN-4	0.15	3.39	0 12:26	0.006	0.000

Storage Volume Summary

Storage Unit hr:min	Unit CFS	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
IN-2 12:06	5.44	0.015	0	0	0	1.698	3	0
IN-3 12:19	21.00	0.156	0	0	0	7.614	15	0
ExistingBasin 12:01	143.11	0.979	6	0	0	6.740	43	0
IN-4 12:26	13.48	1.888	4	0	0	50.041	100	0
IN-12 12:00	26.09	0.002	0	0	0	0.017	0	0
IN-11 12:09	39.93	0.117	0	0	0	10.860	22	0
IN-10 12:00	62.92	0.005	0	0	0	0.025	0	0
IN-9 12:00	56.52	0.006	0	0	0	0.031	0	0
IN-8 12:00	44.33	0.004	0	0	0	0.034	0	0
IN-5 12:06	2.52	0.008	0	0	0	1.172	2	0
IN-6 12:10	11.23	0.071	0	0	0	7.449	15	0
IN-7 12:06	17.51	0.023	0	0	0	3.632	7	0

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
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-----
273 Out-5          99.80    21.00    143.11    15.454
274 -----
275 System        99.80    21.00    143.11    15.454
276

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*****
279 Link Flow Summary
280 *****

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Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.96	0	11:38	8.90	5.45	1.00
21inRCP	CONDUIT	13.48	0	13:29	5.61	2.69	1.00
12inRCP	CONDUIT	5.44	0	12:00	6.93	1.08	1.00
24inRcp(2)	CONDUIT	21.00	0	12:03	6.68	2.97	1.00
PipeRecessed	CONDUIT	20.20	0	12:20	6.75	5.30	1.00
15inCMP	CONDUIT	2.52	0	11:54	2.05	1.03	1.00
21inCMP	CONDUIT	11.23	0	12:24	4.67	1.57	1.00
27inCMP	CONDUIT	17.51	0	12:14	4.40	1.49	1.00
30inRCP	CONDUIT	44.33	0	12:00	9.03	1.20	1.00
36inRCP(2)	CONDUIT	56.52	0	12:00	8.14	2.58	0.95
36inRCP	CONDUIT	62.92	0	12:00	9.46	1.17	0.89
36inCMP(2)	CONDUIT	39.93	0	12:11	6.27	4.20	0.98
24inRCP	CONDUIT	26.09	0	12:00	8.81	1.08	0.91
48inRCP	CONDUIT	143.11	0	12:01	13.48	0.96	0.79
36inCMP	CONDUIT	30.24	0	12:40	4.28	4.65	1.00
26	CONDUIT	27.70	0	11:39	1.97	0.52	1.00
27	CONDUIT	27.03	0	11:40	2.44	0.15	1.00
28	CONDUIT	12.99	0	12:00	0.58	0.03	0.82
29	CONDUIT	29.39	0	12:00	1.08	0.10	1.00
31	CONDUIT	8.36	0	22:37	0.64	0.09	1.00
32	CONDUIT	3.06	0	12:00	0.23	0.01	0.90
33	CONDUIT	1.85	0	12:00	0.23	0.01	0.90

```

*****
312 Flow Classification Summary
313 *****

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Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.37	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.23	0.00
24inRcp(2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.74	0.00	0.00	0.25	0.30	0.00
21inCMP	1.00	0.00	0.00	0.00	0.05	0.00	0.00	0.95	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.02	0.09	0.00	0.89	0.01	0.00
36inRCP(2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP(2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.61	0.00
29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.58	0.00
31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00

341 33 1.00 0.00 0.00 0.00 1.00 0.00 0.00 0.00 0.60 0.00

342

343

344 *****

345 Conduit Surcharge Summary

346 *****

347

348 -----

349

350		-----	Hours Full	-----	Hours	Hours
351	Conduit	Both Ends	Upstream	Dnstream	Above Full	Capacity
352					Normal Flow	Limited

353	24inCMP	11.10	11.84	11.10	14.57	11.08
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354	21inRCP	2.84	2.85	2.85	2.88	2.83
-----	---------	------	------	------	------	------

355	12inRCP	3.29	3.29	5.46	0.24	0.24
-----	---------	------	------	------	------	------

356	24inRcp (2)	2.80	2.81	2.81	2.88	2.80
-----	-------------	------	------	------	------	------

357	PipeRecessed	0.37	2.81	0.37	3.75	0.37
-----	--------------	------	------	------	------	------

358	15inCMP	0.69	0.69	0.75	0.09	0.09
-----	---------	------	------	------	------	------

359	21inCMP	0.65	0.71	0.66	0.74	0.65
-----	---------	------	------	------	------	------

360	27inCMP	0.45	0.49	0.46	0.72	0.45
-----	---------	------	------	------	------	------

361	30inRCP	0.24	0.32	0.24	0.52	0.24
-----	---------	------	------	------	------	------

362	36inRCP (2)	0.01	0.20	0.01	1.77	0.01
-----	-------------	------	------	------	------	------

363	36inRCP	0.01	0.01	0.01	0.20	0.01
-----	---------	------	------	------	------	------

364	36inCMP (2)	0.01	8.56	0.01	13.05	0.01
-----	-------------	------	------	------	-------	------

365	24inRCP	0.01	0.01	0.01	0.05	0.01
-----	---------	------	------	------	------	------

366	36inCMP	8.56	8.56	11.85	14.07	0.01
-----	---------	------	------	-------	-------	------

367	26	0.45	0.45	0.57	0.01	0.01
-----	----	------	------	------	------	------

368	27	0.57	0.57	1.17	0.01	0.01
-----	----	------	------	------	------	------

369	28	0.01	0.01	1.17	0.01	0.01
-----	----	------	------	------	------	------

370	29	1.17	1.17	11.27	0.01	0.01
-----	----	------	------	-------	------	------

371	31	0.43	0.43	0.57	0.01	0.01
-----	----	------	------	------	------	------

372	32	0.01	0.01	0.43	0.01	0.01
-----	----	------	------	------	------	------

373	33	0.01	0.01	0.43	0.01	0.01
-----	----	------	------	------	------	------

374

375

376 Analysis begun on: Tue Nov 15 17:08:12 2022

377 Analysis ended on: Tue Nov 15 17:08:13 2022

378 Total elapsed time: 00:00:01

Location 10: Old Washington Rd. and Shoppers World (25-Year - 2050 - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	61.292	7.066
Evaporation Loss	0.000	0.000
Infiltration Loss	6.713	0.774
Surface Runoff	53.895	6.213
Final Storage	0.782	0.090
Continuity Error (%)	-0.162	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	53.896	17.563
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	53.599	17.466
Flooding Loss	0.278	0.090
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.032	0.010
Continuity Error (%)	-0.023	

Time-Step Critical Elements

Link 24inRcp(2) (65.29%)

Link 12inRCP (24.53%)

Link 27 (5.41%)

Link 36inCMP (2.82%)

```

*****
Highest Flow Instability Indexes
*****
Link 12inRCP (22)
Link 24inRcp(2) (19)
Link PipeRecessed (11)
Link 32 (1)
Link 33 (1)

```

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*****
Most Frequent Nonconverging Nodes
*****
Node Out-5 (0.04%)
Node IN-2 (0.01%)
Node MH-1 (0.01%)
Node IN-1 (0.01%)
Node IN-3 (0.01%)

```

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*****
Routing Time Step Summary
*****
Minimum Time Step      :    0.50 sec
Average Time Step      :    3.57 sec
Maximum Time Step      :   20.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.04
% of Steps Not Converging :    0.04
Time Step Frequencies  :
    20.000 - 9.564 sec :    0.17 %
     9.564 - 4.573 sec :   17.69 %
     4.573 - 2.187 sec :   68.30 %
     2.187 - 1.046 sec :   12.46 %
     1.046 - 0.500 sec :    1.37 %

```

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*****
Subcatchment Runoff Summary
*****

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				Total Perv Precip Runoff	Total Runon Runoff	Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
Subcatchment	in	in	10^6 gal	in	in	in	in	in
			CFS					
DA-1			7.07	0.00	0.00	0.92	3.58	
2.45	6.04	10.59	268.97	0.854				
DA-2			7.07	0.00	0.00	0.15	6.41	
0.48	6.90	0.20	10.39	0.976				
DA-3			7.07	0.00	0.00	1.27	1.76	
3.98	5.74	0.75	26.35	0.813				
DA-4			7.07	0.00	0.00	0.53	4.86	
1.65	6.51	1.56	61.68	0.921				
DA-5			7.07	0.00	0.00	0.02	6.97	
0.05	7.02	0.11	5.54	0.994				
DA-6			7.07	0.00	0.00	0.12	6.55	
0.37	6.93	0.40	19.63	0.981				
DA-7			7.07	0.00	0.00	0.19	6.27	
0.59	6.86	0.31	15.74	0.971				
DA-8			7.07	0.00	0.00	0.17	6.34	

	0.54	6.88	0.45	22.76	0.974			
125	DA-9		7.07		0.00	0.00	0.12	6.55
	0.37	6.93	0.27	14.01	0.981			
126	DA-10		7.07		0.00	0.00	0.29	5.85
	0.91	6.76	0.15	7.37	0.957			
127	DA-11		7.07		0.00	0.00	0.19	6.27
	0.59	6.86	0.77	38.53	0.971			
128	DA-12		7.07		0.00	0.00	0.59	4.58
	1.87	6.45	0.62	29.94	0.913			
129	DA-13		7.07		0.00	0.00	0.42	5.92
	0.71	6.63	0.31	15.42	0.938			
130	DA-14		7.07		0.00	0.00	1.30	2.40
	3.34	5.74	0.45	18.42	0.812			
131	DA-15		7.07		0.00	0.00	0.32	5.70
	1.02	6.72	0.05	2.70	0.951			
132	DA-16		7.07		0.00	0.00	0.46	5.15
	1.44	6.59	0.09	4.11	0.932			
133	DA-BASIN		7.07		0.00	0.00	0.46	5.15
	1.44	6.59	0.49	24.39	0.932			

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	1.00	4.35	207.09	0 12:26	4.35
Out-4	JUNCTION	3.51	6.93	205.44	0 12:13	6.92
IN-1	JUNCTION	3.21	5.57	206.67	0 14:28	5.57
Out-1	JUNCTION	1.87	4.46	205.46	0 12:12	4.45
Out-3	JUNCTION	0.62	2.84	205.45	0 12:12	2.83
Out-6	JUNCTION	0.93	3.45	205.45	0 12:12	3.44
Out-2	JUNCTION	0.92	3.45	205.45	0 12:12	3.44
Jun-1	JUNCTION	1.63	4.45	205.45	0 12:12	4.44
Jun-2	JUNCTION	1.73	4.55	205.45	0 12:12	4.54
Jun-3	JUNCTION	1.93	5.05	205.45	0 12:12	5.04
Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
IN-2	STORAGE	0.65	4.22	207.32	0 12:07	4.18
IN-3	STORAGE	0.99	4.46	207.22	0 12:22	4.45
ExistingBasin	STORAGE	0.99	3.30	201.50	0 12:01	3.24
IN-4	STORAGE	0.85	5.00	208.12	0 12:11	5.00
IN-12	STORAGE	0.20	2.62	205.52	0 12:00	2.57
IN-11	STORAGE	2.24	4.57	203.20	0 12:09	4.55
IN-10	STORAGE	0.53	3.07	203.24	0 12:00	3.03
IN-9	STORAGE	0.73	3.69	204.07	0 12:00	3.60
IN-8	STORAGE	0.52	4.01	206.28	0 12:00	3.97
IN-5	STORAGE	0.23	4.18	211.47	0 12:07	4.14
IN-6	STORAGE	0.38	4.43	210.20	0 12:10	4.43
IN-7	STORAGE	0.40	4.32	208.17	0 12:07	4.25

Node Inflow Summary

Node	Type	Maximum Total Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
------	------	---	---	--	---	------

	gal	Percent						
179	-----							

180	MH-1		JUNCTION	0.00	27.22	0	12:02	0
	2.44	-0.060						
181	Out-4		JUNCTION	18.42	49.74	0	12:03	0.45
	11.5	0.035						
182	IN-1		JUNCTION	268.97	268.97	0	12:05	10.6
	10.6	0.003						
183	Out-1		JUNCTION	0.00	27.72	0	11:35	0
	10.6	0.005						
184	Out-3		JUNCTION	15.42	15.42	0	12:00	0.306
	0.306	0.025						
185	Out-6		JUNCTION	4.11	4.11	0	12:00	0.0858
	0.0863	0.148						
186	Out-2		JUNCTION	2.70	2.70	0	12:00	0.0511
	0.0516	0.316						
187	Jun-1		JUNCTION	0.00	8.80	1	00:29	0
	0.141	-0.736						
188	Jun-2		JUNCTION	0.00	27.60	0	11:37	0
	10.7	0.005						
189	Jun-3		JUNCTION	0.00	33.75	0	12:03	0
	11	-0.021						
190	Out-5		OUTFALL	0.00	148.63	0	12:01	0
	17.5	0.000						
191	IN-2		STORAGE	10.39	10.39	0	12:00	0.204
	0.229	0.559						
192	IN-3		STORAGE	26.35	34.39	0	12:00	0.747
	2.21	0.008						
193	ExistingBasin		STORAGE	24.39	151.92	0	12:00	0.487
	17.5	0.004						
194	IN-4		STORAGE	61.68	61.68	0	12:00	1.56
	1.56	0.043						
195	IN-12		STORAGE	29.94	29.94	0	12:00	0.622
	0.622	0.003						
196	IN-11		STORAGE	38.53	62.22	0	12:00	0.771
	12.3	0.008						
197	IN-10		STORAGE	7.37	65.09	0	11:59	0.145
	4.1	0.001						
198	IN-9		STORAGE	14.01	58.51	0	12:00	0.275
	3.96	-0.003						
199	IN-8		STORAGE	22.76	45.56	0	12:00	0.452
	3.68	0.012						
200	IN-5		STORAGE	5.54	5.54	0	12:00	0.107
	0.107	0.053						
201	IN-6		STORAGE	19.63	22.06	0	12:00	0.397
	0.504	0.092						
202	IN-7		STORAGE	15.74	23.54	0	12:00	0.309
	0.813	-0.007						

203
204
205 *****
206 Node Surcharge Summary
207 *****
208

209 Surcharging occurs when water rises above the top of the highest conduit.

			Hours	Max. Height	Min. Depth
			Surcharged	Above Crown	Below Rim
	Node	Type		Feet	Feet
214	-----				
215	MH-1	JUNCTION	3.03	2.351	0.000
216	Out-4	JUNCTION	13.28	2.925	0.000
217	IN-1	JUNCTION	13.96	3.566	0.000
218	Out-1	JUNCTION	0.74	0.460	0.540
219	Jun-1	JUNCTION	0.72	0.452	0.548
220	Jun-2	JUNCTION	0.83	0.551	0.449
221	Jun-3	JUNCTION	1.46	1.045	0.000

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min		Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
MH-1	1.88	17.77	0	12:01	0.132	0.351
Out-4	13.28	24.99	0	11:59	0.239	2.925
IN-1	12.87	252.33	0	12:05	4.234	0.566
Jun-3	0.22	6.46	0	12:08	0.004	0.045
IN-4	0.47	22.31	0	12:11	0.090	0.000

Storage Volume Summary

Storage Unit hr:min	Unit CFS	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
IN-2 12:07	5.47	0.026	0	0	0	2.490	5	0
IN-3 12:22	21.88	0.248	0	0	0	10.625	21	0
ExistingBasin 12:01	148.63	1.086	7	0	0	7.289	46	0
IN-4 12:11	13.49	2.096	4	0	0	50.041	100	0
IN-12 12:00	29.68	0.002	0	0	0	0.024	0	0
IN-11 12:09	40.83	0.220	0	0	0	16.429	33	0
IN-10 12:00	65.02	0.005	0	0	0	0.028	0	0
IN-9 12:00	57.86	0.007	0	0	0	0.033	0	0
IN-8 12:00	44.54	0.005	0	0	0	0.042	0	0
IN-5 12:07	2.52	0.014	0	0	0	1.624	3	0
IN-6 12:10	11.30	0.112	0	0	0	9.436	19	0
IN-7 12:07	17.66	0.041	0	0	0	5.285	11	0

Outfall Loading Summary

Flow Freq	Avg Flow	Max Flow	Total Volume
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272	Outfall Node	Pcnt	CFS	CFS	10^6 gal
273	-----				
274	Out-5	99.81	23.58	148.63	17.465
275	-----				
276	System	99.81	23.58	148.63	17.465

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth

24inCMP	CONDUIT	27.72	0	11:35	8.82	5.40	1.00
21inRCP	CONDUIT	13.49	0	13:44	5.61	2.69	1.00
12inRCP	CONDUIT	5.47	0	11:58	6.96	1.09	1.00
24inRcp (2)	CONDUIT	21.88	0	12:03	6.96	3.09	1.00
PipeRecessed	CONDUIT	20.44	0	12:24	6.82	5.36	1.00
15inCMP	CONDUIT	2.52	0	11:53	2.05	1.03	1.00
21inCMP	CONDUIT	11.30	0	12:37	4.70	1.58	1.00
27inCMP	CONDUIT	17.66	0	12:15	4.44	1.50	1.00
30inRCP	CONDUIT	44.54	0	11:59	9.07	1.21	1.00
36inRCP (2)	CONDUIT	57.86	0	11:59	8.22	2.65	1.00
36inRCP	CONDUIT	65.02	0	12:00	9.51	1.21	0.93
36inCMP (2)	CONDUIT	40.83	0	12:12	6.39	4.30	1.00
24inRCP	CONDUIT	29.68	0	12:00	9.56	1.23	0.96
48inRCP	CONDUIT	148.63	0	12:01	13.50	1.00	0.86
36inCMP	CONDUIT	30.39	0	12:51	4.30	4.67	1.00
26	CONDUIT	27.49	0	11:36	1.91	0.51	1.00
27	CONDUIT	26.90	0	11:37	2.44	0.15	1.00
28	CONDUIT	14.69	0	12:00	0.61	0.04	0.85
29	CONDUIT	33.22	0	12:03	1.04	0.11	1.00
31	CONDUIT	8.80	1	00:29	0.68	0.10	1.00
32	CONDUIT	3.94	0	12:03	0.24	0.01	0.93
33	CONDUIT	2.23	0	11:59	0.24	0.01	0.93

Flow Classification Summary

	Adjusted	-----		Fraction of		Time in Flow Class		-----		
	/Actual		Up	Down	Sub	Sup	Up	Down	Norm	Inlet
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.36	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.21	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.75	0.00	0.00	0.24	0.37	0.00
21inCMP	1.00	0.00	0.00	0.00	0.06	0.00	0.00	0.94	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.02	0.09	0.00	0.88	0.01	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.55	0.00
29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.50	0.00
31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00

341	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.54	0.00
342	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.53	0.00

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346 Conduit Surcharge Summary

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Conduit	Hours Full		Hours		Hours	
	Both Ends	Upstream	Dnstream	Above Full	Normal Flow	Capacity Limited
24inCMP	13.10	13.96	13.11	16.75		13.00
21inRCP	3.06	3.08	3.08	3.13		3.06
12inRCP	3.65	3.65	6.20	0.25		0.25
24inRcp (2)	3.03	3.03	3.03	3.14		3.02
PipeRecessed	0.41	3.03	0.41	4.21		0.41
15inCMP	0.83	0.83	0.88	0.08		0.09
21inCMP	0.76	0.84	0.77	0.87		0.76
27inCMP	0.55	0.58	0.55	0.85		0.55
30inRCP	0.27	0.36	0.27	0.61		0.27
36inRCP (2)	0.01	0.23	0.01	2.05		0.01
36inRCP	0.01	0.03	0.01	0.24		0.01
36inCMP (2)	0.01	10.42	0.01	15.47		0.01
24inRCP	0.01	0.07	0.01	0.12		0.01
36inCMP	10.42	10.42	13.92	16.33		0.01
26	0.74	0.74	0.83	0.01		0.01
27	0.83	0.83	1.46	0.01		0.01
28	0.01	0.01	1.46	0.01		0.01
29	1.46	1.46	13.28	0.01		0.01
31	0.72	0.72	0.83	0.01		0.01
32	0.01	0.01	0.72	0.01		0.01
33	0.01	0.01	0.72	0.01		0.01

Analysis begun on: Tue Nov 15 17:10:59 2022

Analysis ended on: Tue Nov 15 17:10:59 2022

Total elapsed time: < 1 sec

Location 10: Old Washington Rd. and Shoppers World (25-Year - 2100 - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	65.386	7.538
Evaporation Loss	0.000	0.000
Infiltration Loss	6.828	0.787
Surface Runoff	57.873	6.672
Final Storage	0.795	0.092
Continuity Error (%)	-0.168	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	57.876	18.860
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	57.424	18.713
Flooding Loss	0.438	0.143
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.033	0.011
Continuity Error (%)	-0.033	

Highest Continuity Errors

Node Jun-1 (-1.06%)

Time-Step Critical Elements

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70 *****
71 Link 24inRcp(2) (57.74%)
72 Link 12inRCP (31.88%)
73 Link 27 (5.59%)
74 Link 36inCMP (2.70%)
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77 *****
78 Highest Flow Instability Indexes
79 *****
80 Link 12inRCP (14)
81 Link 24inRcp(2) (10)
82 Link PipeRecessed (6)
83 Link 33 (1)
84
85
86 *****
87 Most Frequent Nonconverging Nodes
88 *****
89 Node Out-5 (0.03%)
90 Node MH-1 (0.01%)
91 Node IN-2 (0.01%)
92 Node IN-4 (0.01%)
93 Node IN-3 (0.01%)
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96 *****
97 Routing Time Step Summary
98 *****
99 Minimum Time Step      :      0.50 sec
100 Average Time Step      :      3.51 sec
101 Maximum Time Step      :     20.00 sec
102 % of Time in Steady State :      0.00
103 Average Iterations per Step :      2.04
104 % of Steps Not Converging :      0.03
105 Time Step Frequencies :
106 20.000 - 9.564 sec      :      0.17 %
107 9.564 - 4.573 sec      :     17.15 %
108 4.573 - 2.187 sec      :     68.36 %
109 2.187 - 1.046 sec      :     12.98 %
110 1.046 - 0.500 sec      :      1.34 %
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113 *****
114 Subcatchment Runoff Summary
115 *****
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Subcatchment	in	in	10 ⁶ gal	Total Perv Precip Runoff in	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
DA-1				7.54	0.00	0.00	0.94	3.82
2.67	6.49	11.39	291.05	0.861				
DA-2				7.54	0.00	0.00	0.15	6.84
0.52	7.37	0.22	11.07	0.977				
DA-3				7.54	0.00	0.00	1.29	1.89
4.32	6.20	0.81	28.67	0.823				
DA-4				7.54	0.00	0.00	0.53	5.19
1.78	6.97	1.67	66.48	0.925				
DA-5				7.54	0.00	0.00	0.02	7.44
0.06	7.50	0.11	5.88	0.994				

127	DA-6		7.54	0.00	0.00	0.12	7.00
	0.41	7.40	0.42	20.94	0.982		
128	DA-7		7.54	0.00	0.00	0.19	6.69
	0.64	7.33	0.33	16.78	0.973		
129	DA-8		7.54	0.00	0.00	0.17	6.77
	0.58	7.35	0.48	24.26	0.975		
130	DA-9		7.54	0.00	0.00	0.12	6.99
	0.41	7.40	0.29	14.92	0.982		
131	DA-10		7.54	0.00	0.00	0.29	6.24
	0.99	7.23	0.16	7.86	0.959		
132	DA-11		7.54	0.00	0.00	0.19	6.69
	0.64	7.33	0.82	41.11	0.973		
133	DA-12		7.54	0.00	0.00	0.60	4.89
	2.02	6.91	0.67	32.10	0.917		
134	DA-13		7.54	0.00	0.00	0.43	6.32
	0.77	7.09	0.33	16.47	0.941		
135	DA-14		7.54	0.00	0.00	1.32	2.56
	3.63	6.19	0.49	19.97	0.821		
136	DA-15		7.54	0.00	0.00	0.32	6.08
	1.10	7.18	0.05	2.88	0.953		
137	DA-16		7.54	0.00	0.00	0.46	5.49
	1.56	7.05	0.09	4.40	0.936		
138	DA-BASIN		7.54	0.00	0.00	0.46	5.49
	1.56	7.05	0.52	26.08	0.936		

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141 *****
142 Node Depth Summary
143 *****
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Node	Type	Average	Maximum	Maximum	Time of Max		Reported	
		Depth	Depth	HGL	Occurrence		Max Depth	
		Feet	Feet	Feet	days	hr:min	Feet	

150	MH-1	JUNCTION	1.03	4.39	207.13	0 12:27	4.39	
151	Out-4	JUNCTION	3.66	7.04	205.55	0 12:13	7.03	
152	IN-1	JUNCTION	3.38	5.63	206.73	0 14:36	5.63	
153	Out-1	JUNCTION	1.96	4.58	205.58	0 12:11	4.57	
154	Out-3	JUNCTION	0.67	2.95	205.56	0 12:12	2.94	
155	Out-6	JUNCTION	1.00	3.57	205.57	0 12:11	3.56	
156	Out-2	JUNCTION	0.99	3.57	205.57	0 12:11	3.56	
157	Jun-1	JUNCTION	1.73	4.57	205.57	0 12:11	4.56	
158	Jun-2	JUNCTION	1.83	4.67	205.57	0 12:11	4.66	
159	Jun-3	JUNCTION	2.04	5.16	205.56	0 12:12	5.15	
160	Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00	
161	IN-2	STORAGE	0.68	4.24	207.34	0 12:07	4.21	
162	IN-3	STORAGE	1.02	4.50	207.26	0 12:23	4.49	
163	ExistingBasin	STORAGE	1.03	3.45	201.65	0 12:02	3.32	
164	IN-4	STORAGE	0.88	5.00	208.12	0 12:08	5.00	
165	IN-12	STORAGE	0.21	3.00	205.90	0 12:00	2.93	
166	IN-11	STORAGE	2.32	4.64	203.27	0 12:09	4.62	
167	IN-10	STORAGE	0.55	3.13	203.30	0 12:00	3.12	
168	IN-9	STORAGE	0.75	3.77	204.15	0 12:00	3.77	
169	IN-8	STORAGE	0.54	4.06	206.33	0 12:01	4.04	
170	IN-5	STORAGE	0.24	4.19	211.48	0 12:07	4.16	
171	IN-6	STORAGE	0.39	4.46	210.23	0 12:11	4.46	
172	IN-7	STORAGE	0.42	4.35	208.20	0 12:07	4.29	

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175 *****
176 Node Inflow Summary
177 *****
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180		Maximum	Maximum	Lateral
		Total	Flow	

181				Lateral	Total	Time of Max		Inflow	
182				Inflow	Balance	Inflow Occurrence		Volume	
183	Node		Type	Volume	Error	days hr:min		10^6 gal	10^6
184	gal	Percent		CFS	CFS				
185	MH-1		JUNCTION	0.00	27.75	0	12:01	0	
	2.57	-0.045							
186	Out-4		JUNCTION	19.97	52.38	0	12:02	0.485	
	12.4	0.034							
187	IN-1		JUNCTION	291.05	291.05	0	12:05	11.4	
	11.4	0.004							
188	Out-1		JUNCTION	0.00	27.59	0	11:32	0	
	11.4	0.006							
189	Out-3		JUNCTION	16.47	16.47	0	12:00	0.327	
	0.327	0.030							
190	Out-6		JUNCTION	4.40	4.40	0	12:00	0.0919	
	0.0925	0.188							
191	Out-2		JUNCTION	2.88	2.88	0	12:00	0.0546	
	0.0551	0.371							
192	Jun-1		JUNCTION	0.00	9.33	1	01:33	0	
	0.151	-1.048							
193	Jun-2		JUNCTION	0.00	27.37	0	11:33	0	
	11.5	0.001							
194	Jun-3		JUNCTION	0.00	34.05	0	12:02	0	
	11.9	-0.023							
195	Out-5		OUTFALL	0.00	149.61	0	12:04	0	
	18.7	0.000							
196	IN-2		STORAGE	11.07	11.07	0	12:00	0.218	
	0.235	0.371							
197	IN-3		STORAGE	28.67	36.78	0	12:00	0.807	
	2.33	0.006							
198	ExistingBasin		STORAGE	26.08	156.01	0	12:00	0.521	
	18.7	0.004							
199	IN-4		STORAGE	66.48	66.48	0	12:00	1.67	
	1.67	-0.019							
200	IN-12		STORAGE	32.10	32.10	0	12:00	0.666	
	0.666	0.004							
201	IN-11		STORAGE	41.11	65.69	0	12:00	0.824	
	13.2	0.008							
202	IN-10		STORAGE	7.86	66.12	0	12:00	0.155	
	4.35	0.001							
203	IN-9		STORAGE	14.92	58.53	0	11:59	0.293	
	4.2	-0.003							
204	IN-8		STORAGE	24.26	46.16	0	12:00	0.483	
	3.9	0.013							
205	IN-5		STORAGE	5.88	5.88	0	12:00	0.114	
	0.114	0.019							
206	IN-6		STORAGE	20.94	23.36	0	12:00	0.424	
	0.538	0.091							
207	IN-7		STORAGE	16.78	24.57	0	12:00	0.33	
	0.868	-0.030							
208									
209									
210	*****								
211	Node Surcharge Summary								
212	*****								
213									
214	Surcharging occurs when water rises above the top of the highest conduit.								
215	-----								
216					Max. Height	Min. Depth			
217				Hours	Above Crown	Below Rim			
218	Node		Type	Surcharged	Feet	Feet			
219	-----								
220	MH-1		JUNCTION	3.16	2.391	0.000			
221	Out-4		JUNCTION	14.41	3.043	0.000			

222	IN-1	JUNCTION	15.15	3.631	0.000
223	Out-1	JUNCTION	0.90	0.577	0.423
224	Jun-1	JUNCTION	0.88	0.570	0.430
225	Jun-2	JUNCTION	0.99	0.669	0.331
226	Jun-3	JUNCTION	1.65	1.163	0.000

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
MH-1	2.05	18.63	0 12:01	0.147	0.391
Out-4	14.41	26.34	0 12:02	0.249	3.043
IN-1	13.99	275.76	0 12:05	4.722	0.631
Jun-3	0.44	11.73	0 12:05	0.014	0.163
IN-4	0.56	35.70	0 12:08	0.143	0.000

Storage Volume Summary

Storage Unit hr:min	CFS	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
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IN-2		0.033	0	0	0	2.995	6	0
12:07	5.47							
IN-3		0.310	1	0	0	12.563	25	0
12:23	22.39							
ExistingBasin		1.138	7	0	0	7.920	50	0
12:02	149.61							
IN-4		2.195	4	0	0	50.041	100	0
12:08	13.50							
IN-12		0.002	0	0	0	0.027	0	0
12:00	31.79							
IN-11		0.292	0	0	0	20.250	40	0
12:09	41.34							
IN-10		0.005	0	0	0	0.028	0	0
12:00	66.16							
IN-9		0.007	0	0	0	0.034	0	0
12:00	58.33							
IN-8		0.005	0	0	0	0.228	0	0
12:01	45.26							
IN-5		0.018	0	0	0	1.905	4	0
12:07	2.52							
IN-6		0.135	0	0	0	10.626	21	0
12:11	11.34							
IN-7		0.051	0	0	0	6.328	13	0
12:07	17.69							

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.81	24.83	149.61	18.711
System	99.81	24.83	149.61	18.711

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.59	0 11:32	8.78	5.38	1.00
21inRCP	CONDUIT	13.50	0 13:54	5.61	2.69	1.00
12inRCP	CONDUIT	5.47	0 11:58	6.96	1.09	1.00
24inRcp (2)	CONDUIT	22.39	0 12:02	7.13	3.16	1.00
PipeRecessed	CONDUIT	20.58	0 12:26	6.86	5.40	1.00
15inCMP	CONDUIT	2.52	0 11:52	2.07	1.03	1.00
21inCMP	CONDUIT	11.34	0 12:40	4.72	1.59	1.00
27inCMP	CONDUIT	17.69	0 12:16	4.45	1.50	1.00
30inRCP	CONDUIT	45.26	0 12:03	9.22	1.23	1.00
36inRCP (2)	CONDUIT	58.33	0 12:00	8.25	2.67	1.00
36inRCP	CONDUIT	66.16	0 12:00	9.64	1.23	0.93
36inCMP (2)	CONDUIT	41.34	0 12:11	6.45	4.35	1.00
24inRCP	CONDUIT	31.79	0 12:00	10.21	1.32	0.97
48inRCP	CONDUIT	149.61	0 12:04	13.53	1.01	0.88
36inCMP	CONDUIT	30.47	0 12:59	4.31	4.68	1.00
26	CONDUIT	27.35	0 11:33	1.91	0.51	1.00
27	CONDUIT	26.66	0 11:33	2.44	0.14	1.00
28	CONDUIT	16.02	0 12:00	0.64	0.04	0.87
29	CONDUIT	33.69	0 12:02	1.02	0.11	1.00
31	CONDUIT	9.33	1 01:33	0.73	0.10	1.00
32	CONDUIT	3.94	0 12:05	0.25	0.01	0.95
33	CONDUIT	2.29	0 12:01	0.25	0.01	0.95

Flow Classification Summary

	Adjusted	Fraction of Time in Flow Class								
	/Actual	Up		Down	Sub	Sup	Up	Down	Norm	Inlet
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.34	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.20	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.76	0.00	0.00	0.23	0.40	0.00
21inCMP	1.00	0.00	0.00	0.00	0.06	0.00	0.00	0.94	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.02	0.10	0.00	0.88	0.01	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

341	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
342	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
343	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.51	0.00
344	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.46	0.00
345	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
346	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.50	0.00
347	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.49	0.00

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Conduit Surcharge Summary

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356		-----	Hours Full	-----	Hours	Hours
357	Conduit	Both Ends	Upstream	Dnstream	Above Full	Capacity
358					Normal Flow	Limited
359	24inCMP	14.22	15.15	14.24	18.31	14.15
360	21inRCP	3.22	3.25	3.24	3.32	3.22
361	12inRCP	3.89	3.89	6.70	0.25	0.25
362	24inRcp (2)	3.16	3.17	3.16	3.34	3.16
363	PipeRecessed	0.44	3.16	0.44	4.53	0.44
364	15inCMP	0.91	0.91	0.96	0.09	0.09
365	21inCMP	0.83	0.92	0.83	0.95	0.82
366	27inCMP	0.61	0.64	0.62	0.93	0.61
367	30inRCP	0.28	0.39	0.28	0.67	0.28
368	36inRCP (2)	0.03	0.24	0.03	2.21	0.03
369	36inRCP	0.01	0.07	0.01	0.25	0.01
370	36inCMP (2)	0.09	11.81	0.09	16.76	0.09
371	24inRCP	0.01	0.11	0.01	0.15	0.01
372	48inRCP	0.01	0.01	0.01	0.06	0.01
373	36inCMP	11.81	11.81	15.10	17.76	0.01
374	26	0.90	0.90	0.99	0.01	0.01
375	27	0.99	0.99	1.65	0.01	0.01
376	28	0.01	0.01	1.65	0.01	0.01
377	29	1.65	1.65	14.41	0.01	0.01
378	31	0.88	0.88	0.99	0.01	0.01
379	32	0.01	0.01	0.88	0.01	0.01
380	33	0.01	0.01	0.88	0.01	0.01

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Analysis begun on: Tue Nov 15 17:11:33 2022

384

Analysis ended on: Tue Nov 15 17:11:34 2022

385

Total elapsed time: 00:00:01

Location 10: Old Washington Rd. and Shoppers World (100-Year - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	75.621	8.718
Evaporation Loss	0.000	0.000
Infiltration Loss	7.050	0.813
Surface Runoff	67.880	7.826
Final Storage	0.818	0.094
Continuity Error (%)	-0.169	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	67.882	22.120
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	67.006	21.835
Flooding Loss	0.873	0.285
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.034	0.011
Continuity Error (%)	-0.046	

Highest Continuity Errors

Node Jun-1 (-2.29%)

Time-Step Critical Elements

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70 *****
71 Link 24inRcp(2) (52.42%)
72 Link 12inRCP (34.63%)
73 Link 27 (8.54%)
74 Link 36inCMP (1.92%)
75 Link 24inCMP (1.04%)
76
77
78 *****
79 Highest Flow Instability Indexes
80 *****
81 Link 12inRCP (10)
82 Link 24inRcp(2) (8)
83 Link PipeRecessed (5)
84
85
86 *****
87 Most Frequent Nonconverging Nodes
88 *****
89 Node Out-5 (0.03%)
90 Node IN-1 (0.01%)
91 Node Out-1 (0.01%)
92 Node MH-1 (0.01%)
93 Node Jun-2 (0.00%)
94
95
96 *****
97 Routing Time Step Summary
98 *****
99 Minimum Time Step      :      0.50 sec
100 Average Time Step      :      3.37 sec
101 Maximum Time Step      :     20.00 sec
102 % of Time in Steady State :      0.00
103 Average Iterations per Step :      2.04
104 % of Steps Not Converging :      0.03
105 Time Step Frequencies  :
106 20.000 - 9.564 sec      :      0.14 %
107 9.564 - 4.573 sec      :     16.95 %
108 4.573 - 2.187 sec      :     66.28 %
109 2.187 - 1.046 sec      :     14.92 %
110 1.046 - 0.500 sec      :      1.71 %
111
112
113 *****
114 Subcatchment Runoff Summary
115 *****
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Subcatchment	in	in	10 ⁶ gal	Total Perv Precip Runoff in CFS	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
DA-1	3.21	7.64	13.41	351.90	0.876	0.00	0.97	4.43
DA-2	0.62	8.54	0.25	12.90	0.980	0.00	0.16	7.92
DA-3	5.16	7.34	0.95	34.98	0.842	0.00	1.33	2.18
DA-4	2.13	8.14	1.95	79.58	0.933	0.00	0.55	6.00
DA-5	0.07	8.68	0.13	6.82	0.995	0.00	0.02	8.61

127	DA-6		8.72	0.00	0.00	0.12	8.10
	0.49	8.58	0.49	24.47	0.984		
128	DA-7		8.72	0.00	0.00	0.19	7.75
	0.76	8.51	0.38	19.57	0.976		
129	DA-8		8.72	0.00	0.00	0.18	7.83
	0.69	8.53	0.56	28.34	0.978		
130	DA-9		8.72	0.00	0.00	0.12	8.09
	0.48	8.58	0.34	17.38	0.984		
131	DA-10		8.72	0.00	0.00	0.30	7.22
	1.18	8.40	0.18	9.20	0.964		
132	DA-11		8.72	0.00	0.00	0.19	7.75
	0.76	8.51	0.96	48.07	0.976		
133	DA-12		8.72	0.00	0.00	0.62	5.66
	2.42	8.08	0.78	37.96	0.927		
134	DA-13		8.72	0.00	0.00	0.45	7.31
	0.94	8.25	0.38	19.32	0.947		
135	DA-14		8.72	0.00	0.00	1.36	2.96
	4.36	7.32	0.57	24.20	0.840		
136	DA-15		8.72	0.00	0.00	0.33	7.04
	1.32	8.35	0.06	3.35	0.958		
137	DA-16		8.72	0.00	0.00	0.48	6.35
	1.87	8.22	0.11	5.19	0.943		
138	DA-BASIN		8.72	0.00	0.00	0.48	6.35
	1.87	8.22	0.61	30.65	0.943		

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141 *****
142 Node Depth Summary
143 *****
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		Average	Maximum	Maximum	Time of Max	Reported
		Depth	Depth	HGL	Occurrence	Max Depth
Node	Type	Feet	Feet	Feet	days hr:min	Feet
MH-1	JUNCTION	1.10	4.49	207.23	0 12:31	4.49
Out-4	JUNCTION	3.96	7.36	205.87	0 12:11	7.34
IN-1	JUNCTION	3.73	5.81	206.91	0 14:55	5.81
Out-1	JUNCTION	2.15	4.89	205.89	0 12:10	4.87
Out-3	JUNCTION	0.79	3.27	205.88	0 12:10	3.25
Out-6	JUNCTION	1.14	3.88	205.88	0 12:10	3.86
Out-2	JUNCTION	1.14	3.88	205.88	0 12:10	3.86
Jun-1	JUNCTION	1.93	4.88	205.88	0 12:10	4.86
Jun-2	JUNCTION	2.03	4.98	205.88	0 12:10	4.96
Jun-3	JUNCTION	2.27	5.48	205.88	0 12:10	5.46
Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
IN-2	STORAGE	0.75	4.30	207.40	0 12:08	4.28
IN-3	STORAGE	1.09	4.60	207.36	0 12:25	4.60
ExistingBasin	STORAGE	1.10	3.72	201.92	0 12:01	3.63
IN-4	STORAGE	0.95	5.00	208.12	0 12:04	5.00
IN-12	STORAGE	0.23	4.03	206.93	0 12:00	4.02
IN-11	STORAGE	2.49	4.77	203.40	0 12:10	4.76
IN-10	STORAGE	0.59	3.28	203.45	0 12:00	3.27
IN-9	STORAGE	0.80	3.96	204.34	0 12:00	3.95
IN-8	STORAGE	0.58	4.17	206.44	0 12:03	4.12
IN-5	STORAGE	0.26	4.23	211.52	0 12:08	4.21
IN-6	STORAGE	0.42	4.53	210.30	0 12:12	4.53
IN-7	STORAGE	0.45	4.43	208.28	0 12:08	4.38

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174
175 *****
176 Node Inflow Summary
177 *****
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180		Maximum	Maximum	Lateral
		Total	Flow	

181				Lateral	Total	Time of Max		Inflow	
182				Inflow	Balance	Inflow Occurrence		Volume	
183	Node		Type	Volume	Error	days hr:min		10^6 gal	10^6
184	gal	Percent		CFS	CFS				
185	MH-1		JUNCTION	0.00	29.02	0	12:02	0	
	2.88	-0.039							
186	Out-4		JUNCTION	24.20	63.44	0	11:59	0.575	
	14.5	0.029							
187	IN-1		JUNCTION	351.90	351.90	0	12:05	13.4	
	13.4	0.003							
188	Out-1		JUNCTION	0.00	27.50	0	11:20	0	
	13.4	0.001							
189	Out-3		JUNCTION	19.32	19.32	0	12:00	0.381	
	0.381	0.032							
190	Out-6		JUNCTION	5.19	5.19	0	12:00	0.107	
	0.108	0.317							
191	Out-2		JUNCTION	3.35	3.35	0	12:00	0.0635	
	0.0641	0.552							
192	Jun-1		JUNCTION	0.00	9.95	1	04:03	0	
	0.175	-2.239							
193	Jun-2		JUNCTION	0.00	27.26	0	11:21	0	
	13.6	-0.010							
194	Jun-3		JUNCTION	0.00	41.36	0	11:59	0	
	14	-0.020							
195	Out-5		OUTFALL	0.00	161.47	0	12:02	0	
	21.8	0.000							
196	IN-2		STORAGE	12.90	12.90	0	12:00	0.253	
	0.265	0.276							
197	IN-3		STORAGE	34.98	43.27	0	12:00	0.955	
	2.62	0.011							
198	ExistingBasin		STORAGE	30.65	165.77	0	12:00	0.607	
	21.8	0.002							
199	IN-4		STORAGE	79.58	79.58	0	12:00	1.95	
	1.95	0.002							
200	IN-12		STORAGE	37.96	37.96	0	12:00	0.779	
	0.779	0.021							
201	IN-11		STORAGE	48.07	75.08	0	12:00	0.957	
	15.5	0.009							
202	IN-10		STORAGE	9.20	68.82	0	12:00	0.18	
	4.96	0.006							
203	IN-9		STORAGE	17.38	59.89	0	12:00	0.34	
	4.78	-0.003							
204	IN-8		STORAGE	28.34	49.69	0	12:00	0.56	
	4.44	0.015							
205	IN-5		STORAGE	6.82	6.82	0	12:00	0.132	
	0.132	0.069							
206	IN-6		STORAGE	24.47	26.87	0	12:00	0.492	
	0.623	0.031							
207	IN-7		STORAGE	19.57	27.37	0	12:00	0.384	
	1.01	-0.018							
208									
209									
210	*****								
211	Node Surcharge Summary								
212	*****								
213									
214	Surcharging occurs when water rises above the top of the highest conduit.								
215	-----								
216					Max. Height	Min. Depth			
217				Hours	Above Crown	Below Rim			
218	Node		Type	Surcharged	Feet	Feet			
219	-----								
220	MH-1		JUNCTION	3.55	2.488	0.000			
221	Out-4		JUNCTION	17.16	3.359	0.000			

222	IN-1	JUNCTION	18.06	3.810	0.000
223	Out-1	JUNCTION	1.31	0.886	0.114
224	Jun-1	JUNCTION	1.29	0.881	0.119
225	Jun-2	JUNCTION	1.38	0.980	0.020
226	Jun-3	JUNCTION	2.20	1.476	0.000

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230 Node Flooding Summary

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233 Flooding refers to all water that overflows a node, whether it ponds or not.

234	-----						
235						Total	Maximum
236			Maximum	Time of Max		Flood	Ponded
237		Hours	Rate	Occurrence		Volume	Depth
238	Node	Flooded	CFS	days hr:min		10^6 gal	Feet
239	-----						
240	MH-1	2.47	20.27	0	12:01	0.183	0.488
241	Out-4	17.16	37.17	0	11:59	0.275	3.359
242	IN-1	16.68	338.90	0	12:05	6.062	0.810
243	Jun-3	0.84	23.92	0	12:01	0.041	0.476
244	IN-4	0.76	62.58	0	12:04	0.284	0.000

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248 Storage Volume Summary

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252			Average	Avg	Evap	Exfil	Maximum	Max	Time of
			Max	Maximum					
253			Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
			Occurrence		Outflow				
254	Storage Unit		1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
	hr:min	CFS							
255									

IN-2		0.064	0	0	0	4.414	9	0
12:08	5.47							
IN-3		0.501	1	0	0	17.927	36	0
12:25	23.71							
ExistingBasin		1.251	8	0	0	9.047	58	0
12:01	161.47							
IN-4		2.438	5	0	0	50.041	100	0
12:04	13.49							
IN-12		0.002	0	0	0	0.094	0	0
12:00	36.37							
IN-11		0.513	1	0	0	29.872	60	0
12:10	42.45							
IN-10		0.005	0	0	0	0.030	0	0
12:00	68.73							
IN-9		0.007	0	0	0	0.036	0	0
12:00	59.65							
IN-8		0.010	0	0	0	1.491	3	0
12:03	47.98							
IN-5		0.028	0	0	0	2.667	5	0
12:08	2.51							
IN-6		0.207	0	0	0	13.944	28	0
12:12	11.41							
IN-7		0.082	0	0	0	9.288	19	0
12:08	17.70							

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271 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.83	27.51	161.47	21.833
System	99.83	27.51	161.47	21.833

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.50	0 11:20	8.75	5.36	1.00
21inRCP	CONDUIT	13.49	0 14:17	5.61	2.69	1.00
12inRCP	CONDUIT	5.47	0 11:57	6.97	1.09	1.00
24inRcp (2)	CONDUIT	23.71	0 12:03	7.55	3.35	1.00
PipeRecessed	CONDUIT	20.91	0 12:34	6.95	5.48	1.00
15inCMP	CONDUIT	2.51	0 11:51	2.08	1.02	1.00
21inCMP	CONDUIT	11.41	0 12:38	4.74	1.60	1.00
27inCMP	CONDUIT	17.70	0 12:23	4.45	1.50	1.00
30inRCP	CONDUIT	47.98	0 12:07	9.77	1.30	1.00
36inRCP (2)	CONDUIT	59.65	0 12:00	8.44	2.73	1.00
36inRCP	CONDUIT	68.73	0 12:00	9.94	1.27	0.95
36inCMP (2)	CONDUIT	42.45	0 12:12	6.59	4.47	1.00
24inRCP	CONDUIT	36.37	0 12:01	11.58	1.51	1.00
48inRCP	CONDUIT	161.47	0 12:02	13.55	1.09	0.92
36inCMP	CONDUIT	30.67	0 13:17	4.34	4.71	1.00
26	CONDUIT	27.25	0 11:21	1.90	0.51	1.00
27	CONDUIT	26.95	0 16:51	2.43	0.15	1.00
28	CONDUIT	18.79	0 12:01	0.67	0.05	0.91
29	CONDUIT	40.69	0 11:59	1.13	0.14	1.00
31	CONDUIT	9.95	1 04:03	0.88	0.11	1.00
32	CONDUIT	5.02	0 12:02	0.31	0.02	0.99
33	CONDUIT	3.15	0 12:02	0.31	0.01	0.99

Flow Classification Summary

	Adjusted	Fraction of Time in Flow Class								
	/Actual	Up	Down	Sub	Sup	Up	Down	Norm	Inlet	
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.31	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.19	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.77	0.00	0.00	0.22	0.45	0.00
21inCMP	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.92	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.03	0.11	0.00	0.86	0.01	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.07	0.01	0.00	0.91	0.08	0.00
36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

341	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
342	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
343	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.42	0.00
344	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
345	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
346	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.40	0.00
347	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.40	0.00

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Conduit Surcharge Summary

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355

Conduit	Hours Full			Hours	Hours
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
24inCMP	16.93	18.05	16.95	21.95	16.88
21inRCP	3.70	3.72	3.71	3.78	3.69
12inRCP	4.46	4.46	8.50	0.26	0.26
24inRcp (2)	3.55	3.56	3.55	3.81	3.55
PipeRecessed	0.59	3.55	0.59	5.42	0.59
15inCMP	1.13	1.13	1.17	0.09	0.09
21inCMP	1.01	1.14	1.01	1.17	1.01
27inCMP	0.76	0.79	0.77	1.15	0.76
30inRCP	0.31	0.46	0.31	0.82	0.31
36inRCP (2)	0.12	0.28	0.12	2.63	0.12
36inRCP	0.01	0.15	0.01	0.29	0.01
36inCMP (2)	0.17	13.24	0.17	19.75	0.17
24inRCP	0.05	0.17	0.05	0.21	0.05
48inRCP	0.01	0.01	0.01	0.15	0.01
36inCMP	13.24	13.24	17.96	21.34	0.01
26	1.31	1.31	1.38	0.01	0.01
27	1.38	1.38	2.20	0.01	0.01
28	0.01	0.01	2.20	0.01	0.01
29	2.20	2.20	17.16	0.01	0.01
31	1.29	1.29	1.38	0.01	0.01
32	0.01	0.01	1.29	0.01	0.01
33	0.01	0.01	1.29	0.01	0.01

381

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383

Analysis begun on: Tue Nov 15 17:12:01 2022

384

Analysis ended on: Tue Nov 15 17:12:01 2022

385

Total elapsed time: < 1 sec

Location 10: Old Washington Rd. and Shoppers World (100-Year - 2050 - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	86.759	10.002
Evaporation Loss	0.000	0.000
Infiltration Loss	7.243	0.835
Surface Runoff	78.827	9.088
Final Storage	0.840	0.097
Continuity Error (%)	-0.174	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	78.824	25.686
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	75.473	24.594
Flooding Loss	1.378	0.449
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	1.995	0.650
Continuity Error (%)	-0.028	

Highest Continuity Errors

Node Jun-1 (3.29%)

Time-Step Critical Elements

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70 *****
71 Link 24inRcp(2) (45.50%)
72 Link 12inRCP (37.69%)
73 Link 27 (9.71%)
74 Link 36inCMP (4.46%)
75
76
77 *****
78 Highest Flow Instability Indexes
79 *****
80 Link 12inRCP (9)
81 Link 24inRcp(2) (7)
82 Link PipeRecessed (5)
83
84
85 *****
86 Most Frequent Nonconverging Nodes
87 *****
88 Node Out-5 (0.03%)
89 Node Out-1 (0.01%)
90 Node MH-1 (0.01%)
91 Node IN-2 (0.01%)
92 Node IN-6 (0.01%)
93
94

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95 *****
96 Routing Time Step Summary
97 *****
98 Minimum Time Step      :      0.50 sec
99 Average Time Step      :      3.21 sec
100 Maximum Time Step     :     20.00 sec
101 % of Time in Steady State :      0.00
102 Average Iterations per Step :      2.03
103 % of Steps Not Converging :      0.03
104 Time Step Frequencies :
105     20.000 - 9.564 sec :      0.13 %
106     9.564 - 4.573 sec :     16.36 %
107     4.573 - 2.187 sec :     62.89 %
108     2.187 - 1.046 sec :     18.75 %
109     1.046 - 0.500 sec :      1.87 %
110
111

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112 *****
113 Subcatchment Runoff Summary
114 *****
115
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Subcatchment	in	in	10^6 gal	Total Perv Precip Runoff in	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
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DA-1			10.00	0.00	0.00	0.99	5.08
3.81	8.89	15.61	420.35	0.889			
DA-2			10.00	0.00	0.00	0.16	9.09
0.74	9.83	0.29	14.91	0.983			
DA-3			10.00	0.00	0.00	1.37	2.50
6.09	8.59	1.12	42.13	0.859			
DA-4			10.00	0.00	0.00	0.56	6.89
2.52	9.41	2.25	94.18	0.941			
DA-5			10.00	0.00	0.00	0.02	9.88
0.08	9.96	0.15	7.85	0.996			
DA-6			10.00	0.00	0.00	0.13	9.29

	0.57	9.87	0.57	28.35	0.986			
127	DA-7		10.00		0.00	0.00	0.20	8.89
	0.90	9.79	0.44	22.64	0.979			
128	DA-8		10.00		0.00	0.00	0.18	8.99
	0.82	9.81	0.64	32.79	0.981			
129	DA-9		10.00		0.00	0.00	0.13	9.29
	0.57	9.86	0.39	20.06	0.986			
130	DA-10		10.00		0.00	0.00	0.31	8.29
	1.39	9.68	0.21	10.66	0.968			
131	DA-11		10.00		0.00	0.00	0.20	8.89
	0.90	9.79	1.10	55.69	0.979			
132	DA-12		10.00		0.00	0.00	0.64	6.50
	2.85	9.35	0.90	44.41	0.935			
133	DA-13		10.00		0.00	0.00	0.47	8.39
	1.13	9.52	0.44	22.45	0.952			
134	DA-14		10.00		0.00	0.00	1.40	3.40
	5.17	8.57	0.67	28.96	0.857			
135	DA-15		10.00		0.00	0.00	0.34	8.08
	1.55	9.63	0.07	3.86	0.963			
136	DA-16		10.00		0.00	0.00	0.49	7.29
	2.20	9.50	0.12	6.07	0.950			
137	DA-BASIN		10.00		0.00	0.00	0.49	7.29
	2.20	9.50	0.70	35.67	0.950			

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139
140 *****
141 Node Depth Summary
142 *****
143

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	1.14	4.59	207.33	0 12:34	4.58
Out-4	JUNCTION	4.22	7.54	206.05	0 12:11	7.51
IN-1	JUNCTION	4.04	6.02	207.12	0 15:17	6.02
Out-1	JUNCTION	2.32	5.06	206.06	0 12:11	5.05
Out-3	JUNCTION	0.90	3.44	206.05	0 12:12	3.43
Out-6	JUNCTION	1.28	4.05	206.05	0 12:09	4.05
Out-2	JUNCTION	1.28	4.05	206.05	0 12:09	4.05
Jun-1	JUNCTION	2.11	5.05	206.05	0 12:09	5.05
Jun-2	JUNCTION	2.21	5.15	206.05	0 12:10	5.15
Jun-3	JUNCTION	2.48	5.65	206.05	0 12:12	5.64
Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
IN-2	STORAGE	0.80	4.35	207.45	0 12:09	4.34
IN-3	STORAGE	1.14	4.70	207.46	0 12:27	4.70
ExistingBasin	STORAGE	1.16	3.91	202.11	0 12:02	3.83
IN-4	STORAGE	1.00	5.00	208.12	0 12:01	5.00
IN-12	STORAGE	0.24	4.17	207.07	0 12:03	4.11
IN-11	STORAGE	2.63	4.90	203.53	0 12:11	4.89
IN-10	STORAGE	0.61	3.43	203.60	0 12:01	3.40
IN-9	STORAGE	0.83	4.09	204.47	0 12:02	4.06
IN-8	STORAGE	0.61	4.28	206.55	0 12:05	4.20
IN-5	STORAGE	0.28	4.27	211.56	0 12:08	4.25
IN-6	STORAGE	0.45	4.59	210.36	0 12:13	4.59
IN-7	STORAGE	0.47	4.50	208.35	0 12:10	4.47

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173
174 *****
175 Node Inflow Summary
176 *****
177

	Maximum Total Lateral	Maximum Flow Total	Time of Max	Lateral Inflow
179				
180				

181				Inflow Inflow Volume CFS	Balance Inflow CFS	Occurrence Error days hr:min	Volume 10^6 gal	10^6
182	Node gal	Percent	Type					
183								
184	MH-1 3.22	-0.018	JUNCTION	0.00	30.37	0 12:02	0	
185	Out-4 16.4	0.159	JUNCTION	28.96	65.06	0 11:58	0.672	
186	IN-1 15.6	0.005	JUNCTION	420.35	420.35	0 12:05	15.6	
187	Out-1 15.2	0.086	JUNCTION	0.00	27.34	0 11:07	0	
188	Out-3 0.44	0.380	JUNCTION	22.45	22.45	0 12:00	0.44	
189	Out-6 0.124	2.039	JUNCTION	6.07	6.07	0 12:00	0.124	
190	Out-2 0.0732	3.595	JUNCTION	3.86	3.86	0 12:00	0.0732	
191	Jun-1 0.204	3.404	JUNCTION	0.00	14.15	0 12:06	0	
192	Jun-2 15.4	0.139	JUNCTION	0.00	27.34	0 17:31	0	
193	Jun-3 15.8	0.133	JUNCTION	0.00	43.46	0 11:58	0	
194	Out-5 24.6	0.000	OUTFALL	0.00	165.74	0 12:02	0	
195	IN-2 0.302	0.223	STORAGE	14.91	14.91	0 12:00	0.291	
196	IN-3 2.92	0.010	STORAGE	42.13	50.57	0 12:00	1.12	
197	ExistingBasin 24.6	0.016	STORAGE	35.67	171.05	0 12:00	0.701	
198	IN-4 2.25	-0.060	STORAGE	94.18	94.18	0 12:00	2.25	
199	IN-12 0.901	0.012	STORAGE	44.41	44.41	0 12:00	0.901	
200	IN-11 17.4	0.105	STORAGE	55.69	84.14	0 12:00	1.1	
201	IN-10 5.61	0.011	STORAGE	10.66	69.65	0 12:00	0.208	
202	IN-9 5.41	0.002	STORAGE	20.06	62.18	0 12:00	0.391	
203	IN-8 5.02	0.023	STORAGE	32.79	53.76	0 12:00	0.645	
204	IN-5 0.151	0.080	STORAGE	7.85	7.85	0 12:00	0.151	
205	IN-6 0.716	0.050	STORAGE	28.35	30.72	0 12:00	0.565	
206	IN-7 1.16	-0.016	STORAGE	22.64	30.44	0 12:00	0.441	
207								
208								
209	*****							
210	Node Surge Summary							
211	*****							
212								
213	Surcharging occurs when water rises above the top of the highest conduit.							
214	-----							
215				Hours	Max. Height	Min. Depth		
216				Surcharged	Above Crown	Below Rim		
217	Node		Type		Feet	Feet		
218	-----							
219	MH-1		JUNCTION	4.06	2.586	0.000		
220	Out-4		JUNCTION	19.26	3.539	0.000		
221	IN-1		JUNCTION	20.67	4.016	0.000		

222	Out-1	JUNCTION	1.74	1.056	0.000
223	Out-6	JUNCTION	0.40	0.050	0.950
224	Out-2	JUNCTION	0.39	0.050	0.950
225	Jun-1	JUNCTION	1.72	1.050	0.000
226	Jun-2	JUNCTION	1.83	1.154	0.000
227	Jun-3	JUNCTION	3.06	1.652	0.000

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230 *****
231 Node Flooding Summary
232 *****
233

234 Flooding refers to all water that overflows a node, whether it ponds or not.
235 -----

		Maximum	Time of Max	Total	Maximum	
	Hours	Rate	Occurrence	Flood	Ponded	
Node	Flooded	CFS	days hr:min	Volume 10^6 gal	Depth Feet	
240	-----	-----	-----	-----	-----	
241	MH-1	2.90	21.93	0 12:02	0.220	0.586
242	Out-4	19.26	37.32	0 11:58	0.293	3.539
243	IN-1	18.88	409.44	0 12:05	7.602	1.016
244	Out-1	0.41	5.32	0 12:06	0.005	0.056
245	Jun-1	0.40	14.13	0 12:06	0.021	0.050
246	Jun-2	0.57	15.20	0 12:04	0.018	0.154
247	Jun-3	1.25	31.83	0 11:59	0.061	0.652
248	IN-4	0.95	81.14	0 12:01	0.449	0.000

249
250

251 *****
252 Storage Volume Summary
253 *****
254

255

		Average	Avg	Evap	Exfil	Maximum	Max	Time of
		Max	Maximum					
		Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
		Occurrence	Outflow					
Storage Unit		1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
hr:min	CFS							

259

260	IN-2	0.122	0	0	0	6.073	12	0
	12:09	5.46						
261	IN-3	0.757	2	0	0	24.359	49	0
	12:27	25.11						
262	ExistingBasin	1.342	9	0	0	9.932	63	0
	12:02	165.74						
263	IN-4	2.674	5	0	0	50.041	100	0
	12:01	13.44						
264	IN-12	0.006	0	0	0	1.449	3	0
	12:03	37.03						
265	IN-11	0.820	2	0	0	40.434	81	0
	12:11	43.42						
266	IN-10	0.005	0	0	0	0.031	0	0
	12:01	69.48						
267	IN-9	0.008	0	0	0	0.454	1	0
	12:02	60.52						
268	IN-8	0.021	0	0	0	3.936	8	0
	12:05	49.91						
269	IN-5	0.044	0	0	0	3.558	7	0
	12:08	2.51						
270	IN-6	0.313	1	0	0	17.714	35	0
	12:13	11.47						
271	IN-7	0.131	0	0	0	12.378	25	0
	12:10	17.74						

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.85	29.65	165.74	24.592
System	99.85	29.65	165.74	24.592

 Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.34	0 11:07	8.70	5.33	1.00
21inRCP	CONDUIT	13.44	0 14:41	5.59	2.68	1.00
12inRCP	CONDUIT	5.46	0 11:56	6.95	1.08	1.00
24inRcp (2)	CONDUIT	25.11	0 12:03	7.99	3.55	1.00
PipeRecessed	CONDUIT	21.23	0 12:42	7.04	5.57	1.00
15inCMP	CONDUIT	2.51	0 11:49	2.08	1.02	1.00
21inCMP	CONDUIT	11.47	0 12:46	4.77	1.61	1.00
27inCMP	CONDUIT	17.74	0 12:29	4.46	1.51	1.00
30inRCP	CONDUIT	49.91	0 12:10	10.17	1.36	1.00
36inRCP (2)	CONDUIT	60.52	0 12:05	8.56	2.77	1.00
36inRCP	CONDUIT	69.48	0 12:00	9.99	1.29	0.99
36inCMP (2)	CONDUIT	43.42	0 12:13	6.71	4.57	1.00
24inRCP	CONDUIT	37.03	0 12:03	11.79	1.53	1.00
48inRCP	CONDUIT	165.74	0 12:02	13.58	1.12	0.95
36inCMP	CONDUIT	30.94	0 13:38	4.38	4.76	1.00
26	CONDUIT	27.17	0 17:55	1.89	0.51	1.00
27	CONDUIT	27.37	0 17:30	2.44	0.15	1.00
28	CONDUIT	21.89	0 12:00	0.73	0.05	0.93
29	CONDUIT	40.88	0 11:56	1.14	0.14	1.00
31	CONDUIT	9.32	0 12:03	0.26	0.10	1.00
32	CONDUIT	5.82	0 11:58	0.18	0.02	1.00
33	CONDUIT	3.95	0 11:58	0.18	0.01	1.00

 Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.27	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.18	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.04	0.00	0.00	0.96	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.78	0.00	0.00	0.22	0.56	0.00
21inCMP	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.91	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.90	0.00
30inRCP	1.00	0.00	0.00	0.00	0.03	0.12	0.00	0.84	0.01	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.14	0.01	0.00	0.85	0.14	0.00

341	36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
342	24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
343	48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
344	36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
345	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
346	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
347	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
348	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.28	0.00
349	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
350	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
351	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00

352
353
354 *****
355 Conduit Surcharge Summary
356 *****

357		-----				
358			Hours Full		Hours	Hours
359		-----	Upstream	-----	Above Full	Capacity
360	Conduit	Both Ends		Dnstream	Normal Flow	Limited
361						
362						
363	24inCMP	19.13	20.67	19.13	24.89	19.13
364	21inRCP	4.21	4.23	4.22	4.31	4.20
365	12inRCP	5.13	5.13	9.98	0.29	0.29
366	24inRcp (2)	4.05	4.06	4.05	4.35	4.05
367	PipeRecessed	0.75	4.05	0.75	6.44	0.75
368	15inCMP	1.36	1.36	1.41	0.09	0.09
369	21inCMP	1.23	1.38	1.24	1.40	1.23
370	27inCMP	0.93	0.96	0.94	1.38	0.93
371	30inRCP	0.38	0.63	0.38	0.99	0.38
372	36inRCP (2)	0.18	0.35	0.18	3.07	0.18
373	36inRCP	0.01	0.21	0.01	0.36	0.01
374	36inCMP (2)	0.22	15.32	0.22	22.27	0.22
375	24inRCP	0.17	0.23	0.17	0.26	0.17
376	48inRCP	0.01	0.01	0.01	0.22	0.01
377	36inCMP	15.32	15.32	20.18	23.92	0.01
378	26	1.74	1.74	1.83	0.01	0.01
379	27	1.83	1.83	3.06	0.01	0.01
380	28	0.01	0.01	3.06	0.01	0.01
381	29	3.06	3.06	19.26	0.01	0.01
382	31	1.72	1.72	1.83	0.01	0.01
383	32	0.39	0.39	1.72	0.01	0.01
384	33	0.39	0.39	1.72	0.01	0.01

385
386
387 Analysis begun on: Tue Nov 15 17:12:35 2022
388 Analysis ended on: Tue Nov 15 17:12:35 2022
389 Total elapsed time: < 1 sec

Location 10: Old Washington Rd. and Shoppers World (100-Year - 2100 - EXISTING)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	91.495	10.548
Evaporation Loss	0.000	0.000
Infiltration Loss	7.310	0.843
Surface Runoff	83.493	9.625
Final Storage	0.852	0.098
Continuity Error (%)	-0.175	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	83.490	27.206
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	77.569	25.277
Flooding Loss	1.589	0.518
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	4.353	1.418
Continuity Error (%)	-0.025	

Highest Continuity Errors

Node Jun-1 (3.02%)

Time-Step Critical Elements

```

70 *****
71 Link 24inRcp(2) (43.21%)
72 Link 12inRCP (39.82%)
73 Link 27 (9.38%)
74 Link 36inCMP (4.54%)
75
76
77 *****
78 Highest Flow Instability Indexes
79 *****
80 Link 12inRCP (8)
81 Link 24inRcp(2) (7)
82 Link PipeRecessed (5)
83
84
85 *****
86 Most Frequent Nonconverging Nodes
87 *****
88 Node Out-5 (0.03%)
89 Node IN-2 (0.01%)
90 Node MH-1 (0.01%)
91 Node IN-12 (0.01%)
92 Node Out-1 (0.00%)
93
94

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95 *****
96 Routing Time Step Summary
97 *****
98 Minimum Time Step      :      0.50 sec
99 Average Time Step      :      3.16 sec
100 Maximum Time Step     :     20.00 sec
101 % of Time in Steady State :      0.00
102 Average Iterations per Step :      2.03
103 % of Steps Not Converging :      0.03
104 Time Step Frequencies :
105     20.000 - 9.564 sec :      0.12 %
106     9.564 - 4.573 sec :     16.30 %
107     4.573 - 2.187 sec :     61.31 %
108     2.187 - 1.046 sec :     20.26 %
109     1.046 - 0.500 sec :      2.02 %
110
111

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112 *****
113 Subcatchment Runoff Summary
114 *****
115
116

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			Total Perv Precip Runoff	Total Total Runon Runoff	Total Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
Subcatchment	in	10^6 gal	in	in	in	in	in

121	DA-1		10.55	0.00	0.00	1.00	5.36
	4.07	9.43	16.55	448.55	0.894		
122	DA-2		10.55	0.00	0.00	0.16	9.59
	0.78	10.37	0.31	15.72	0.983		
123	DA-3		10.55	0.00	0.00	1.38	2.63
	6.49	9.13	1.19	45.07	0.865		
124	DA-4		10.55	0.00	0.00	0.57	7.27
	2.68	9.95	2.38	100.15	0.944		
125	DA-5		10.55	0.00	0.00	0.02	10.42
	0.09	10.51	0.16	8.26	0.996		
126	DA-6		10.55	0.00	0.00	0.13	9.80

	0.61	10.41	0.60	29.92	0.987		
127	DA-7		10.55		0.00	0.00	9.38
	0.96	10.34	0.47	23.87	0.980		
128	DA-8		10.55		0.00	0.00	9.49
	0.87	10.36	0.68	34.60	0.982		
129	DA-9		10.55		0.00	0.00	9.80
	0.61	10.41	0.41	21.15	0.987		
130	DA-10		10.55		0.00	0.00	8.75
	1.48	10.23	0.22	11.24	0.970		
131	DA-11		10.55		0.00	0.00	9.38
	0.96	10.34	1.16	58.77	0.980		
132	DA-12		10.55		0.00	0.00	6.85
	3.04	9.89	0.95	47.02	0.938		
133	DA-13		10.55		0.00	0.00	8.85
	1.21	10.06	0.46	23.71	0.954		
134	DA-14		10.55		0.00	0.00	3.58
	5.52	9.10	0.71	30.91	0.863		
135	DA-15		10.55		0.00	0.00	8.52
	1.65	10.17	0.08	4.07	0.964		
136	DA-16		10.55		0.00	0.00	7.69
	2.35	10.04	0.13	6.42	0.952		
137	DA-BASIN		10.55		0.00	0.00	7.69
	2.35	10.04	0.74	37.70	0.952		

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	1.17	4.62	207.36	0 12:35	4.62
Out-4	JUNCTION	4.28	7.58	206.09	0 12:10	7.57
IN-1	JUNCTION	4.11	6.10	207.20	0 15:23	6.10
Out-1	JUNCTION	2.37	5.10	206.10	0 12:14	5.10
Out-3	JUNCTION	0.94	3.48	206.09	0 12:11	3.47
Out-6	JUNCTION	1.32	4.09	206.09	0 12:12	4.08
Out-2	JUNCTION	1.32	4.09	206.09	0 12:12	4.08
Jun-1	JUNCTION	2.16	5.09	206.09	0 12:12	5.08
Jun-2	JUNCTION	2.26	5.19	206.09	0 12:13	5.19
Jun-3	JUNCTION	2.53	5.69	206.09	0 12:11	5.68
Out-5	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
IN-2	STORAGE	0.83	4.37	207.47	0 12:09	4.36
IN-3	STORAGE	1.17	4.74	207.50	0 12:27	4.74
ExistingBasin	STORAGE	1.18	4.02	202.22	0 12:02	3.90
IN-4	STORAGE	1.03	5.00	208.12	0 12:01	5.00
IN-12	STORAGE	0.25	4.21	207.11	0 12:04	4.15
IN-11	STORAGE	2.66	4.95	203.58	0 12:11	4.94
IN-10	STORAGE	0.63	3.53	203.70	0 12:02	3.45
IN-9	STORAGE	0.85	4.15	204.53	0 12:04	4.09
IN-8	STORAGE	0.62	4.32	206.59	0 12:05	4.23
IN-5	STORAGE	0.29	4.28	211.57	0 12:08	4.27
IN-6	STORAGE	0.46	4.62	210.39	0 12:13	4.62
IN-7	STORAGE	0.49	4.52	208.37	0 12:10	4.51

Node Inflow Summary

Maximum Total Lateral	Maximum Flow Total	Time of Max	Lateral Inflow
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181				Inflow Inflow Volume CFS	Balance Inflow CFS	Occurrence Error days hr:min	Volume 10^6 gal	10^6
182	Node gal	Percent	Type					
183								
184	MH-1 3.37	-0.019	JUNCTION	0.00	30.88	0 12:02	0	
185	Out-4 16.7	0.156	JUNCTION	30.91	65.74	0 11:57	0.714	
186	IN-1 16.5	0.004	JUNCTION	448.55	448.55	0 12:05	16.5	
187	Out-1 15.4	0.087	JUNCTION	0.00	27.32	0 17:57	0	
188	Out-3 0.464	0.391	JUNCTION	23.71	23.71	0 12:00	0.464	
189	Out-6 0.131	2.038	JUNCTION	6.42	6.42	0 12:00	0.131	
190	Out-2 0.0774	3.468	JUNCTION	4.07	4.07	0 12:00	0.0773	
191	Jun-1 0.224	3.111	JUNCTION	0.00	22.92	0 12:04	0	
192	Jun-2 15.6	0.140	JUNCTION	0.00	27.51	0 17:33	0	
193	Jun-3 16	0.138	JUNCTION	0.00	45.22	0 12:00	0	
194	Out-5 25.3	0.000	OUTFALL	0.00	165.64	0 12:00	0	
195	IN-2 0.318	0.207	STORAGE	15.72	15.72	0 12:00	0.307	
196	IN-3 3.05	0.007	STORAGE	45.07	53.57	0 12:00	1.19	
197	ExistingBasin 25.3	0.016	STORAGE	37.70	172.78	0 12:00	0.742	
198	IN-4 2.38	-0.037	STORAGE	100.15	100.15	0 12:00	2.38	
199	IN-12 0.953	0.058	STORAGE	47.02	47.02	0 12:00	0.953	
200	IN-11 17.7	0.104	STORAGE	58.77	87.65	0 12:00	1.16	
201	IN-10 5.89	0.012	STORAGE	11.24	69.71	0 11:59	0.219	
202	IN-9 5.67	0.004	STORAGE	21.15	63.26	0 12:00	0.413	
203	IN-8 5.26	0.021	STORAGE	34.60	55.43	0 12:00	0.68	
204	IN-5 0.16	0.018	STORAGE	8.26	8.26	0 12:00	0.16	
205	IN-6 0.756	0.069	STORAGE	29.92	32.28	0 12:00	0.596	
206	IN-7 1.22	-0.014	STORAGE	23.87	31.68	0 12:00	0.466	
207								
208								
209	*****							
210	Node Surge Summary							
211	*****							
212								
213	Surcharging occurs when water rises above the top of the highest conduit.							
214	-----							
215					Max. Height	Min. Depth		
216				Hours	Above Crown	Below Rim		
217	Node		Type	Surcharged	Feet	Feet		
218	-----							
219	MH-1		JUNCTION	4.25	2.624	0.000		
220	Out-4		JUNCTION	19.38	3.582	0.000		
221	IN-1		JUNCTION	20.88	4.102	0.000		

222	Out-1	JUNCTION	1.94	1.098	0.000
223	Out-6	JUNCTION	0.59	0.093	0.907
224	Out-2	JUNCTION	0.59	0.093	0.907
225	Jun-1	JUNCTION	1.92	1.093	0.000
226	Jun-2	JUNCTION	2.03	1.192	0.000
227	Jun-3	JUNCTION	3.60	1.689	0.000

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230 *****
231 Node Flooding Summary
232 *****
233

234 Flooding refers to all water that overflows a node, whether it ponds or not.
235 -----

		Maximum	Time of Max	Total	Maximum
	Hours	Rate	Occurrence	Flood	Ponded
Node	Flooded	CFS	days hr:min	Volume 10^6 gal	Depth Feet
240	-----				
241	MH-1	3.07	22.54	0 12:02	0.234
242	Out-4	19.38	37.90	0 11:57	0.298
243	IN-1	18.97	437.87	0 12:05	8.243
244	Out-1	0.62	7.62	0 12:04	0.010
245	Jun-1	0.59	22.90	0 12:04	0.037
246	Jun-2	0.75	15.52	0 12:03	0.021
247	Jun-3	1.45	32.09	0 11:58	0.066
248	IN-4	1.03	88.73	0 12:01	0.517

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251 *****
252 Storage Volume Summary
253 *****
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255

		Average	Avg	Evap	Exfil	Maximum	Max	Time of
		Max	Maximum					
		Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
		Occurrence	Outflow					
Storage Unit		1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
hr:min	CFS							

259

260	IN-2		0.156	0	0	0	6.773	14	0
	12:09	5.45							
261	IN-3		0.884	2	0	0	27.142	54	0
	12:27	25.63							
262	ExistingBasin		1.374	9	0	0	10.425	66	0
	12:02	165.64							
263	IN-4		2.797	6	0	0	50.041	100	0
	12:01	13.42							
264	IN-12		0.010	0	0	0	2.341	5	0
	12:04	37.26							
265	IN-11		0.975	2	0	0	44.969	90	0
	12:11	43.76							
266	IN-10		0.006	0	0	0	0.032	0	0
	12:02	69.56							
267	IN-9		0.011	0	0	0	1.171	2	0
	12:04	62.26							
268	IN-8		0.029	0	0	0	5.033	10	0
	12:05	50.40							
269	IN-5		0.052	0	0	0	3.939	8	0
	12:08	2.52							
270	IN-6		0.366	1	0	0	19.220	38	0
	12:13	11.49							
271	IN-7		0.157	0	0	0	13.601	27	0
	12:10	17.76							

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.85	30.35	165.64	25.275
System	99.85	30.35	165.64	25.275

 Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.32	0 17:57	8.70	5.32	1.00
21inRCP	CONDUIT	13.42	0 14:51	5.58	2.67	1.00
12inRCP	CONDUIT	5.45	0 11:56	6.94	1.08	1.00
24inRcp (2)	CONDUIT	25.63	0 12:03	8.16	3.62	1.00
PipeRecessed	CONDUIT	21.34	0 12:46	7.06	5.60	1.00
15inCMP	CONDUIT	2.52	0 11:48	2.08	1.03	1.00
21inCMP	CONDUIT	11.49	0 12:50	4.78	1.61	1.00
27inCMP	CONDUIT	17.76	0 12:34	4.47	1.51	1.00
30inRCP	CONDUIT	50.40	0 12:10	10.27	1.37	1.00
36inRCP (2)	CONDUIT	62.26	0 12:07	8.81	2.85	1.00
36inRCP	CONDUIT	69.56	0 11:59	10.01	1.29	1.00
36inCMP (2)	CONDUIT	43.76	0 12:14	6.76	4.61	1.00
24inRCP	CONDUIT	37.26	0 12:04	11.86	1.54	1.00
48inRCP	CONDUIT	165.64	0 12:00	13.59	1.11	0.96
36inCMP	CONDUIT	31.08	0 13:46	4.40	4.78	1.00
26	CONDUIT	27.33	0 17:55	1.89	0.51	1.00
27	CONDUIT	27.53	0 17:30	2.44	0.15	1.00
28	CONDUIT	23.17	0 12:00	0.77	0.06	0.94
29	CONDUIT	41.33	0 11:55	1.15	0.14	1.00
31	CONDUIT	15.56	0 12:04	0.43	0.17	1.00
32	CONDUIT	6.28	0 12:00	0.20	0.02	1.00
33	CONDUIT	4.19	0 11:55	0.19	0.01	1.00

 Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
21inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.25	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.17	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.04	0.00	0.00	0.96	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.78	0.00	0.00	0.21	0.61	0.00
21inCMP	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.90	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.04	0.13	0.00	0.83	0.01	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.14	0.01	0.00	0.84	0.15	0.00

341	36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
342	24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
343	48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
344	36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
345	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
346	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
347	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
348	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.28	0.00
349	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
350	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
351	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.32	0.00

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355 Conduit Surcharge Summary

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359		-----	Hours Full	-----	Hours	Hours
360	Conduit	Both Ends	Upstream	Dnstream	Above Full	Capacity
361					Normal Flow	Limited
362		-----	-----	-----	-----	-----
363	24inCMP	19.24	20.88	19.24	25.15	19.24
364	21inRCP	4.42	4.44	4.43	4.53	4.41
365	12inRCP	5.39	5.39	10.64	0.30	0.30
366	24inRcp (2)	4.25	4.26	4.25	4.58	4.25
367	PipeRecessed	0.81	4.25	0.81	6.96	0.81
368	15inCMP	1.46	1.46	1.51	0.09	0.09
369	21inCMP	1.33	1.48	1.33	1.50	1.32
370	27inCMP	1.00	1.03	1.01	1.48	1.00
371	30inRCP	0.42	0.69	0.42	1.07	0.42
372	36inRCP (2)	0.23	0.39	0.23	3.28	0.23
373	36inRCP	0.05	0.23	0.05	0.40	0.05
374	36inCMP (2)	0.25	16.49	0.25	22.68	0.25
375	24inRCP	0.21	0.26	0.21	0.28	0.21
376	48inRCP	0.01	0.04	0.01	0.24	0.01
377	36inCMP	16.49	16.49	20.43	24.34	0.01
378	26	1.94	1.94	2.03	0.01	0.01
379	27	2.03	2.03	3.60	0.01	0.01
380	28	0.01	0.01	3.60	0.01	0.01
381	29	3.60	3.60	19.38	0.01	0.01
382	31	1.92	1.92	2.03	0.01	0.01
383	32	0.59	0.59	1.92	0.01	0.01
384	33	0.59	0.59	1.92	0.01	0.01

385

386

387 Analysis begun on: Tue Nov 15 17:13:01 2022

388 Analysis ended on: Tue Nov 15 17:13:02 2022

389 Total elapsed time: 00:00:01

Location 10: Old Washington Rd. and Shoppers World (25-Year -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	54.673	6.303
Evaporation Loss	0.000	0.000
Infiltration Loss	6.531	0.753
Surface Runoff	47.470	5.473
Final Storage	0.758	0.087
Continuity Error (%)	-0.158	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	47.466	15.468
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	44.919	14.637
Flooding Loss	1.862	0.607
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.658	0.214
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.031	0.010
Continuity Error (%)	-0.007	

Time-Step Critical Elements

Link 34 (74.95%)

Link 38 (13.06%)

Link 12inRCP (5.61%)

Link 24inRcp(2) (1.83%)

Link 36 (1.50%)

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*****
Highest Flow Instability Indexes
*****
Link 12inRCP (11)
Link 24inRcp(2) (8)
Link PipeRecessed (5)
Link 28 (2)
Link 31 (1)

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*****
Most Frequent Nonconverging Nodes
*****
Node IN-1 (0.01%)
Node Out-5 (0.01%)

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*****
Routing Time Step Summary
*****
Minimum Time Step      :      0.50 sec
Average Time Step      :      2.77 sec
Maximum Time Step      :     20.00 sec
% of Time in Steady State :      0.00
Average Iterations per Step :      2.01
% of Steps Not Converging :      0.01
Time Step Frequencies  :
    20.000 - 9.564 sec :      0.16 %
     9.564 - 4.573 sec :      7.75 %
     4.573 - 2.187 sec :     60.40 %
     2.187 - 1.046 sec :     28.72 %
     1.046 - 0.500 sec :      2.98 %

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*****
Subcatchment Runoff Summary
*****

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		Total		Total	Total	Total	Imperv
		Perv	Total	Total	Peak	Runoff	
		Precip	Runon	Evap	Infil	Runoff	
		Runoff	Runoff	Runoff	Runoff	Coeff	
Subcatchment		in	in	in	in		in
in	in	10^6 gal	CFS				
DA-1		6.30	0.00	0.00	0.89	3.19	
2.11	5.30	9.30	231.68	0.841			
DA-2		6.30	0.00	0.00	0.15	5.72	
0.42	6.13	0.18	9.22	0.973			
DA-3		6.30	0.00	0.00	1.24	1.57	
3.44	5.01	0.65	22.50	0.795			
DA-4		6.30	0.00	0.00	0.51	4.33	
1.42	5.75	1.38	53.53	0.913			
DA-5		6.30	0.00	0.00	0.02	6.21	
0.05	6.26	0.10	4.94	0.993			
DA-6		6.30	0.00	0.00	0.11	5.84	
0.32	6.17	0.35	17.38	0.979			
DA-7		6.30	0.00	0.00	0.18	5.59	
0.51	6.10	0.28	13.96	0.968			
DA-8		6.30	0.00	0.00	0.16	5.66	
0.46	6.12	0.40	20.16	0.971			
DA-9		6.30	0.00	0.00	0.11	5.84	

	0.32	6.17	0.24	12.44	0.979			
124	DA-10		6.30		0.00	0.00	0.28	5.22
	0.79	6.00	0.13	6.52	0.952			
125	DA-11		6.30		0.00	0.00	0.18	5.59
	0.51	6.10	0.69	34.10	0.968			
126	DA-12		6.30		0.00	0.00	0.58	4.08
	1.62	5.70	0.55	26.24	0.904			
127	DA-13		6.30		0.00	0.00	0.40	5.28
	0.60	5.88	0.27	13.61	0.933			
128	DA-14		6.30		0.00	0.00	1.26	2.14
	2.87	5.01	0.39	15.82	0.795			
129	DA-15		6.30		0.00	0.00	0.31	5.08
	0.88	5.96	0.05	2.40	0.946			
130	DA-16		6.30		0.00	0.00	0.45	4.59
	1.25	5.83	0.08	3.60	0.925			
131	DA-BASIN		6.30		0.00	0.00	0.44	4.59
	1.25	5.84	0.43	21.48	0.926			

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	0.99	3.75	206.49	0 12:00	3.74
Out-4	JUNCTION	3.46	6.17	204.68	0 12:26	6.16
IN-1	JUNCTION	3.14	5.45	206.55	0 14:14	5.45
Out-1	JUNCTION	1.86	3.73	204.73	0 12:26	3.70
Out-3	JUNCTION	0.64	2.09	204.70	0 12:26	2.06
Out-6	JUNCTION	0.94	2.71	204.71	0 12:26	2.68
Out-2	JUNCTION	0.93	2.71	204.71	0 12:26	2.68
Jun-1	JUNCTION	1.63	3.71	204.71	0 12:26	3.68
Jun-2	JUNCTION	1.73	3.81	204.71	0 12:26	3.78
Jun-3	JUNCTION	1.91	4.30	204.70	0 12:26	4.27
Out-5	OUTFALL	1.00	3.14	199.78	0 12:01	3.07
IN-2	STORAGE	0.65	4.09	207.19	0 12:02	4.07
IN-3	STORAGE	0.98	3.73	206.49	0 12:00	3.72
ExistingBasin	STORAGE	1.00	3.14	201.34	0 12:01	3.09
IN-12	STORAGE	0.22	1.84	204.74	0 12:00	1.82
IN-11	STORAGE	2.23	4.41	203.04	0 12:07	4.34
IN-10	STORAGE	0.57	2.76	202.93	0 12:00	2.74
IN-9	STORAGE	0.77	3.34	203.72	0 12:00	3.33
IN-8	STORAGE	0.56	3.61	205.88	0 12:00	3.59
IN-5	STORAGE	0.30	4.15	211.44	0 12:06	4.11
IN-6	STORAGE	0.46	4.38	210.15	0 12:09	4.37
IN-7	STORAGE	0.47	4.25	208.10	0 12:06	4.18
BMP1	STORAGE	0.37	3.00	208.00	0 11:55	3.00
BMP2	STORAGE	0.41	3.00	207.50	0 11:56	3.00
BMP3	STORAGE	0.51	3.00	207.00	0 11:53	3.00
BMP4	STORAGE	0.73	3.00	206.50	0 11:48	3.00
BMP5	STORAGE	0.40	1.69	204.69	0 12:24	1.66

Node Inflow Summary

	Maximum Total Lateral Inflow	Maximum Flow Total Balance Inflow	Time of Max Occurrence	Lateral Inflow Volume
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180	Node		Type	Volume	Error				
	gal	Percent		CFS	CFS	days	hr:min	10^6 gal	10^6
181	-----								
182	MH-1		JUNCTION	0.00	14.85	0	11:51	0	
	1.63	-0.070							
183	Out-4		JUNCTION	0.00	42.41	0	12:05	0	
	10.2	0.036							
184	IN-1		JUNCTION	231.68	231.68	0	12:05	9.3	
	9.3	-0.009							
185	Out-1		JUNCTION	0.00	28.03	0	11:39	0	
	9.3	0.010							
186	Out-3		JUNCTION	13.61	13.61	0	12:00	0.271	
	0.272	-0.017							
187	Out-6		JUNCTION	3.60	3.60	0	12:00	0.076	
	0.0779	0.000							
188	Out-2		JUNCTION	2.40	2.40	0	12:00	0.0453	
	0.0482	0.004							
189	Jun-1		JUNCTION	0.00	8.21	0	22:27	0	
	0.148	0.151							
190	Jun-2		JUNCTION	0.00	28.28	0	11:57	0	
	9.45	0.012							
191	Jun-3		JUNCTION	0.00	38.86	0	11:58	0	
	9.7	0.006							
192	Out-5		OUTFALL	0.00	142.38	0	12:01	0	
	14.6	0.000							
193	IN-2		STORAGE	9.22	9.22	0	12:00	0.182	
	0.211	0.702							
194	IN-3		STORAGE	0.00	12.68	0	12:40	0	
	1.42	0.009							
195	ExistingBasin		STORAGE	21.48	144.50	0	12:00	0.431	
	14.6	0.005							
196	IN-12		STORAGE	26.24	26.24	0	12:00	0.549	
	0.549	0.001							
197	IN-11		STORAGE	34.10	53.47	0	12:00	0.686	
	10.6	0.009							
198	IN-10		STORAGE	6.52	62.03	0	12:00	0.129	
	3.1	0.002							
199	IN-9		STORAGE	12.44	55.68	0	12:00	0.245	
	2.97	0.002							
200	IN-8		STORAGE	20.16	43.97	0	12:00	0.402	
	2.73	0.020							
201	IN-5		STORAGE	4.94	4.94	0	12:00	0.0952	
	0.0952	0.022							
202	IN-6		STORAGE	17.38	19.83	0	12:00	0.353	
	0.449	0.050							
203	IN-7		STORAGE	13.96	21.78	0	12:00	0.275	
	0.723	-0.064							
204	BMP1		STORAGE	53.53	53.53	0	12:00	1.38	
	1.38	0.000							
205	BMP2		STORAGE	0.00	35.04	0	11:56	0	
	1.31	-0.001							
206	BMP3		STORAGE	22.50	57.13	0	12:00	0.652	
	1.96	0.000							
207	BMP4		STORAGE	0.00	34.66	0	12:04	0	
	1.82	0.002							
208	BMP5		STORAGE	15.82	21.91	0	12:00	0.393	
	0.673	0.005							
209									
210									
211	*****								
212	Node Surcharge Summary								
213	*****								
214									
215	Surcharging occurs when water rises above the top of the highest conduit.								
216	-----								
217					Max. Height	Min. Depth			

218			Hours	Above Crown	Below Rim
219	Node	Type	Surcharged	Feet	Feet
220	-----				
221	MH-1	JUNCTION	1.41	1.753	0.247
222	Out-4	JUNCTION	11.10	2.174	0.000
223	IN-1	JUNCTION	11.71	3.450	0.000
224	Jun-3	JUNCTION	1.00	0.300	0.700

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

233					Total	Maximum
234			Maximum	Time of Max	Flood	Ponded
235		Hours	Rate	Occurrence	Volume	Depth
236	Node	Flooded	CFS	days hr:min	10^6 gal	Feet
237	-----					
238	Out-4	11.10	21.09	0 12:05	0.343	2.174
239	IN-1	10.78	209.09	0 12:05	3.367	0.450
240	BMP1	0.21	18.79	0 12:00	0.069	0.000
241	BMP2	0.01	0.35	0 11:56	0.000	0.000
242	BMP3	0.35	22.42	0 12:00	0.142	0.000
243	BMP4	0.86	32.39	0 12:01	0.396	0.000

Storage Volume Summary

251		Average	Avg	Evap	Exfil	Maximum	Max	Time of
252		Max	Maximum					
253	Storage Unit	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
254	hr:min CFS	Occurrence	Outflow					
		1000 ft3	Full	Loss	Loss	1000 ft3	Full	days

255	IN-2		0.008	0	0	0	0.460	1	0
256	12:02	7.92							
257	IN-3		0.009	0	0	0	0.034	0	0
258	12:00	12.68							
259	ExistingBasin		1.123	7	0	0	6.680	43	0
260	12:01	142.38							
261	IN-12		0.002	0	0	0	0.017	0	0
262	12:00	26.08							
263	IN-11		0.157	0	0	0	8.415	17	0
264	12:07	39.40							
265	IN-10		0.005	0	0	0	0.025	0	0
266	12:00	62.05							
267	IN-9		0.007	0	0	0	0.030	0	0
	12:00	55.61							
	IN-8		0.005	0	0	0	0.032	0	0
	12:00	43.41							
	IN-5		0.017	0	0	0	1.167	2	0
	12:06	2.52							
	IN-6		0.166	0	0	0	7.376	15	0
	12:09	11.27							
	IN-7		0.037	0	0	0	3.242	6	0
	12:06	19.26							
	BMP1		0.054	5	0	0	1.125	100	0
	11:55	35.09							
	BMP2		0.069	6	0	0	1.125	100	0

268	11:56	34.70							
	BMP3		0.097	9	0	0	1.125	100	0
269	11:53	34.71							
	BMP4		0.154	14	0	0	1.125	100	0
270	11:48	12.72							
	BMP5		4.034	13	0	31	16.913	56	0
	12:24	17.10							

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.84	24.54	142.38	14.636
System	99.84	24.54	142.38	14.636

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	28.03	0 11:39	8.92	5.46	1.00
12inRCP	CONDUIT	7.92	0 12:07	10.08	1.57	1.00
24inRcp (2)	CONDUIT	12.68	0 12:41	4.04	1.79	1.00
PipeRecessed	CONDUIT	14.83	0 11:51	4.94	3.89	1.00
15inCMP	CONDUIT	2.52	0 11:54	2.07	1.03	1.00
21inCMP	CONDUIT	11.27	0 12:20	4.69	1.58	1.00
27inCMP	CONDUIT	19.26	0 12:13	4.94	1.63	1.00
30inRCP	CONDUIT	43.41	0 12:00	8.84	1.18	1.00
36inRCP (2)	CONDUIT	55.61	0 12:00	8.04	2.54	0.94
36inRCP	CONDUIT	62.05	0 12:00	9.41	1.15	0.88
36inCMP (2)	CONDUIT	39.40	0 12:09	6.19	4.15	0.97
24inRCP	CONDUIT	26.08	0 12:00	8.81	1.08	0.91
48inRCP	CONDUIT	142.38	0 12:01	13.46	0.96	0.78
36inCMP	CONDUIT	29.35	0 12:44	4.15	4.51	1.00
26	CONDUIT	27.79	0 11:39	2.01	0.52	0.94
27	CONDUIT	30.32	0 12:56	2.49	0.16	0.98
28	CONDUIT	13.31	0 12:00	0.71	0.03	0.76
29	CONDUIT	37.68	0 11:58	1.15	0.13	1.00
31	CONDUIT	8.21	0 22:27	0.61	0.09	0.94
32	CONDUIT	3.35	0 12:00	0.22	0.01	0.80
33	CONDUIT	2.14	0 12:00	0.22	0.01	0.80
34	CONDUIT	35.04	0 11:56	11.15	1.01	1.00
35	CONDUIT	34.65	0 11:56	11.03	1.00	1.00
36	CONDUIT	34.66	0 12:04	11.03	1.00	1.00
37	CONDUIT	12.68	0 12:40	4.03	1.20	1.00
38	CONDUIT	16.64	0 12:05	6.08	0.16	0.92

Flow Classification Summary

Conduit	Adjusted /Actual Length	Up Dry	Down Dry	Fraction of Time in Flow Class Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
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333	24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
334	12inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.23	0.00
335	24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
336	PipeRecessed	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
337	15inCMP	1.00	0.00	0.00	0.00	0.74	0.00	0.00	0.25	0.30	0.00
338	21inCMP	1.00	0.00	0.00	0.00	0.05	0.00	0.00	0.95	0.00	0.00
339	27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
340	30inRCP	1.00	0.00	0.00	0.00	0.01	0.05	0.00	0.93	0.02	0.00
341	36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
342	36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
343	36inCMP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
344	24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
345	48inRCP	1.00	0.00	0.00	0.00	0.01	0.99	0.00	0.00	0.39	0.00
346	36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
347	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
348	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.01	0.00
349	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.62	0.00
350	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.58	0.00
351	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
352	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.61	0.00
353	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00
354	34	1.00	0.00	0.00	0.00	0.04	0.95	0.00	0.00	0.42	0.00
355	35	1.00	0.00	0.00	0.00	0.05	0.94	0.00	0.00	0.82	0.00
356	36	1.00	0.00	0.00	0.00	0.24	0.75	0.00	0.00	0.53	0.00
357	37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.90	0.00
358	38	1.00	0.00	0.55	0.00	0.44	0.00	0.00	0.00	0.31	0.00

Conduit Surcharge Summary

Conduit	----- Hours Full -----			Hours	Hours	
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited	

24inCMP	10.97	11.71	10.97	14.57	10.96	
12inRCP	2.59	2.59	5.46	0.25	0.25	
24inRcp (2)	1.41	1.42	1.41	1.44	1.17	
PipeRecessed	0.26	1.41	0.26	3.56	0.26	
15inCMP	0.67	0.67	0.73	0.09	0.09	
21inCMP	0.63	0.69	0.63	0.72	0.63	
27inCMP	0.28	0.43	0.28	0.70	0.28	
30inRCP	0.21	0.25	0.21	0.38	0.21	
36inRCP (2)	0.01	0.17	0.01	0.86	0.01	
36inRCP	0.01	0.01	0.01	0.18	0.01	
36inCMP (2)	0.01	7.76	0.01	12.81	0.01	
24inRCP	0.01	0.01	0.01	0.05	0.01	
36inCMP	7.76	7.76	11.66	13.83	0.01	
27	0.01	0.01	1.00	0.01	0.01	
28	0.01	0.01	1.00	0.01	0.01	
29	1.00	1.00	11.10	0.01	0.01	
34	0.50	0.50	0.96	0.22	0.21	
35	0.96	0.96	1.16	0.01	0.01	
36	1.16	1.16	1.32	0.01	0.01	
37	1.32	1.32	1.42	0.93	0.94	
38	0.01	0.01	12.71	0.01	0.01	

Analysis begun on: Mon Nov 28 15:00:46 2022
Analysis ended on: Mon Nov 28 15:00:47 2022
Total elapsed time: 00:00:01

Location 10: Old Washington Rd. and Shoppers World (25-Year (2050) -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
*****	-----	-----
Total Precipitation	61.292	7.066
Evaporation Loss	0.000	0.000
Infiltration Loss	6.713	0.774
Surface Runoff	53.895	6.213
Final Storage	0.782	0.090
Continuity Error (%)	-0.162	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	53.888	17.560
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	50.832	16.564
Flooding Loss	2.301	0.750
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.725	0.236
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.033	0.011
Continuity Error (%)	-0.005	

Time-Step Critical Elements

Link 34 (70.85%)

Link 38 (15.19%)

Link 12inRCP (6.33%)

Link 24inRcp(2) (2.31%)

Link 35 (1.63%)

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*****
Highest Flow Instability Indexes
*****
Link 12inRCP (11)
Link 24inRcp(2) (8)
Link PipeRecessed (5)
Link 28 (2)
Link 31 (1)

```

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*****
Most Frequent Nonconverging Nodes
*****
Node Out-5 (0.01%)
Node IN-1 (0.01%)
Node MH-1 (0.00%)
Node IN-5 (0.00%)

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      :      0.50 sec
Average Time Step      :      2.67 sec
Maximum Time Step      :     20.00 sec
% of Time in Steady State :      0.00
Average Iterations per Step :      2.01
% of Steps Not Converging :      0.01
Time Step Frequencies  :
    20.000 - 9.564 sec :      0.13 %
     9.564 - 4.573 sec :      7.35 %
     4.573 - 2.187 sec :     58.30 %
     2.187 - 1.046 sec :     31.02 %
     1.046 - 0.500 sec :      3.20 %

```

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*****
Subcatchment Runoff Summary
*****

```

		Total		Total	Total	Total	Imperv
		Perv		Total	Total	Peak	Runoff
		Precip		Runon	Evap	Infil	Runoff
		Runoff		Runoff	Runoff	Runoff	Coeff
Subcatchment		in		in	in	in	in
in	in	10^6 gal	CFS				
DA-1		7.07	0.00	0.00	0.92	3.58	
2.45	6.04	10.59	268.97	0.854			
DA-2		7.07	0.00	0.00	0.15	6.41	
0.48	6.90	0.20	10.39	0.976			
DA-3		7.07	0.00	0.00	1.27	1.76	
3.98	5.74	0.75	26.35	0.813			
DA-4		7.07	0.00	0.00	0.53	4.86	
1.65	6.51	1.56	61.68	0.921			
DA-5		7.07	0.00	0.00	0.02	6.97	
0.05	7.02	0.11	5.54	0.994			
DA-6		7.07	0.00	0.00	0.12	6.55	
0.37	6.93	0.40	19.63	0.981			
DA-7		7.07	0.00	0.00	0.19	6.27	
0.59	6.86	0.31	15.74	0.971			
DA-8		7.07	0.00	0.00	0.17	6.34	

	0.54	6.88	0.45	22.76	0.974			
125	DA-9		7.07		0.00	0.00	0.12	6.55
	0.37	6.93	0.27	14.01	0.981			
126	DA-10		7.07		0.00	0.00	0.29	5.85
	0.91	6.76	0.15	7.37	0.957			
127	DA-11		7.07		0.00	0.00	0.19	6.27
	0.59	6.86	0.77	38.53	0.971			
128	DA-12		7.07		0.00	0.00	0.59	4.58
	1.87	6.45	0.62	29.94	0.913			
129	DA-13		7.07		0.00	0.00	0.42	5.92
	0.71	6.63	0.31	15.42	0.938			
130	DA-14		7.07		0.00	0.00	1.30	2.40
	3.34	5.74	0.45	18.42	0.812			
131	DA-15		7.07		0.00	0.00	0.32	5.70
	1.02	6.72	0.05	2.70	0.951			
132	DA-16		7.07		0.00	0.00	0.46	5.15
	1.44	6.59	0.09	4.11	0.932			
133	DA-BASIN		7.07		0.00	0.00	0.46	5.15
	1.44	6.59	0.49	24.39	0.932			

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	1.04	3.80	206.54	0 12:00	3.79
Out-4	JUNCTION	3.75	6.38	204.89	0 12:26	6.38
IN-1	JUNCTION	3.45	5.56	206.66	0 14:30	5.56
Out-1	JUNCTION	2.03	3.93	204.93	0 12:26	3.92
Out-3	JUNCTION	0.74	2.30	204.91	0 12:26	2.29
Out-6	JUNCTION	1.08	2.91	204.91	0 12:26	2.91
Out-2	JUNCTION	1.08	2.91	204.91	0 12:26	2.91
Jun-1	JUNCTION	1.82	3.91	204.91	0 12:26	3.91
Jun-2	JUNCTION	1.92	4.01	204.91	0 12:26	4.01
Jun-3	JUNCTION	2.14	4.51	204.91	0 12:26	4.50
Out-5	OUTFALL	1.06	3.28	199.92	0 12:01	3.22
IN-2	STORAGE	0.69	4.14	207.24	0 12:04	4.10
IN-3	STORAGE	1.03	3.78	206.54	0 12:00	3.77
ExistingBasin	STORAGE	1.07	3.28	201.48	0 12:01	3.23
IN-12	STORAGE	0.24	2.62	205.52	0 12:00	2.58
IN-11	STORAGE	2.38	4.51	203.14	0 12:08	4.46
IN-10	STORAGE	0.60	3.00	203.17	0 12:00	2.94
IN-9	STORAGE	0.81	3.56	203.94	0 12:00	3.51
IN-8	STORAGE	0.59	3.84	206.11	0 12:00	3.82
IN-5	STORAGE	0.34	4.18	211.47	0 12:07	4.14
IN-6	STORAGE	0.51	4.43	210.20	0 12:10	4.42
IN-7	STORAGE	0.50	4.31	208.16	0 12:07	4.22
BMP1	STORAGE	0.39	3.00	208.00	0 11:54	3.00
BMP2	STORAGE	0.43	3.00	207.50	0 11:54	3.00
BMP3	STORAGE	0.53	3.00	207.00	0 11:51	3.00
BMP4	STORAGE	0.77	3.00	206.50	0 11:47	3.00
BMP5	STORAGE	0.49	1.90	204.90	0 12:27	1.90

Node Inflow Summary

	Maximum Total Lateral	Maximum Flow Total	Time of Max	Lateral Inflow
--	-----------------------------	--------------------------	-------------	-------------------

				Inflow Inflow Volume CFS	Balance Inflow CFS	Occurrence Error days hr:min	Volume 10^6 gal	10^6
	Node gal	Percent	Type					
181								
182								
183								
184	MH-1 1.78	-0.059	JUNCTION	0.00	14.79	0 11:50	0	
185	Out-4 11.5	0.033	JUNCTION	0.00	47.52	0 12:01	0	
186	IN-1 10.6	-0.002	JUNCTION	268.97	268.97	0 12:05	10.6	
187	Out-1 10.6	0.009	JUNCTION	0.00	27.83	0 11:35	0	
188	Out-3 0.306	-0.017	JUNCTION	15.42	15.42	0 12:00	0.306	
189	Out-6 0.0878	-0.002	JUNCTION	4.11	4.11	0 12:00	0.0858	
190	Out-2 0.0538	0.000	JUNCTION	2.70	2.70	0 12:00	0.0511	
191	Jun-1 0.161	0.162	JUNCTION	0.00	8.76	1 00:18	0	
192	Jun-2 10.7	0.011	JUNCTION	0.00	28.36	0 16:27	0	
193	Jun-3 11	0.006	JUNCTION	0.00	39.00	0 12:04	0	
194	Out-5 16.6	0.000	OUTFALL	0.00	148.63	0 12:01	0	
195	IN-2 0.232	0.612	STORAGE	10.39	10.39	0 12:00	0.204	
196	IN-3 1.55	0.009	STORAGE	0.00	12.66	0 12:45	0	
197	ExistingBasin 16.6	0.004	STORAGE	24.39	151.66	0 12:00	0.487	
198	IN-12 0.622	0.002	STORAGE	29.94	29.94	0 12:00	0.622	
199	IN-11 12	0.008	STORAGE	38.53	58.35	0 12:00	0.771	
200	IN-10 3.44	0.002	STORAGE	7.37	64.86	0 12:00	0.145	
201	IN-9 3.29	0.002	STORAGE	14.01	57.80	0 12:00	0.275	
202	IN-8 3.02	0.018	STORAGE	22.76	44.65	0 12:00	0.452	
203	IN-5 0.107	0.036	STORAGE	5.54	5.54	0 12:00	0.107	
204	IN-6 0.504	0.033	STORAGE	19.63	22.06	0 12:00	0.397	
205	IN-7 0.813	-0.103	STORAGE	15.74	23.56	0 12:00	0.309	
206	BMP1 1.56	0.001	STORAGE	61.68	61.68	0 12:00	1.56	
207	BMP2 1.45	-0.001	STORAGE	0.00	35.04	0 11:54	0	
208	BMP3 2.19	0.002	STORAGE	26.35	60.99	0 12:00	0.747	
209	BMP4 2.01	0.003	STORAGE	0.00	34.66	0 11:59	0	
210	BMP5 0.699	0.004	STORAGE	18.42	25.33	0 12:03	0.45	
211								
212								
213	*****							
214	Node Surcharge Summary							
215	*****							
216								
217	Surcharging occurs when water rises above the top of the highest conduit.							

			Hours	Max. Height	Min. Depth
			Surcharged	Above Crown	Below Rim
	Node	Type		Feet	Feet
223	MH-1	JUNCTION	1.54	1.803	0.197
224	Out-4	JUNCTION	13.10	2.385	0.000
225	IN-1	JUNCTION	13.78	3.556	0.000
226	Jun-2	JUNCTION	0.20	0.013	0.987
227	Jun-3	JUNCTION	1.46	0.506	0.494

230 *****
 231 Node Flooding Summary
 232 *****

233
 234 Flooding refers to all water that overflows a node, whether it ponds or not.
 235

					Total	Maximum
		Hours	Maximum	Time of Max	Flood	Ponded
	Node	Flooded	Rate	Occurrence	Volume	Depth
			CFS	days hr:min	10^6 gal	Feet
241	Out-4	13.10	26.90	0 12:01	0.337	2.385
242	IN-1	12.69	247.64	0 12:05	4.160	0.556
243	BMP1	0.25	26.93	0 12:00	0.112	0.000
244	BMP2	0.01	0.33	0 11:54	0.000	0.000
245	BMP3	0.39	26.28	0 12:00	0.183	0.000
246	BMP4	0.96	33.95	0 12:01	0.455	0.000

249 *****
 250 Storage Volume Summary
 251 *****

		Average	Avg	Evap	Exfil	Maximum	Max	Time of
		Max	Maximum					
		Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
		Occurrence	Outflow					
256	Storage Unit	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
	hr:min CFS							

258	IN-2	0.013	0	0	0	0.984	2	0
	12:04 8.38							
259	IN-3	0.009	0	0	0	0.034	0	0
	12:00 13.28							
260	ExistingBasin	1.225	8	0	0	7.225	46	0
	12:01 148.63							
261	IN-12	0.002	0	0	0	0.024	0	0
	12:00 29.69							
262	IN-11	0.320	1	0	0	12.969	26	0
	12:08 40.24							
263	IN-10	0.005	0	0	0	0.027	0	0
	12:00 64.27							
264	IN-9	0.007	0	0	0	0.032	0	0
	12:00 57.56							
265	IN-8	0.005	0	0	0	0.035	0	0
	12:00 43.84							
266	IN-5	0.028	0	0	0	1.615	3	0
	12:07 2.52							
267	IN-6	0.265	1	0	0	9.351	19	0
	12:10 11.33							
268	IN-7	0.064	0	0	0	4.809	10	0
	12:07 19.48							

269	BMP1		0.059	5	0	0	1.125	100	0
	11:54	35.09							
270	BMP2		0.075	7	0	0	1.125	100	0
	11:54	34.70							
271	BMP3		0.105	9	0	0	1.125	100	0
	11:51	34.71							
272	BMP4		0.164	15	0	0	1.125	100	0
	11:47	12.71							
273	BMP5		4.893	16	0	33	18.987	63	0
	12:27	16.94							

274
275
276 *****
277 Outfall Loading Summary
278 *****

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.85	27.04	148.63	16.563
System	99.85	27.04	148.63	16.563

288
289
290 *****
291 Link Flow Summary
292 *****

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/Full Flow	Max/Full Depth
24inCMP	CONDUIT	27.83	0 11:35	8.86	5.42	1.00
12inRCP	CONDUIT	8.38	0 12:09	10.67	1.67	1.00
24inRcp(2)	CONDUIT	13.28	0 12:10	4.23	1.88	1.00
PipeRecessed	CONDUIT	14.76	0 11:50	4.95	3.87	1.00
15inCMP	CONDUIT	2.52	0 11:53	2.08	1.03	1.00
21inCMP	CONDUIT	11.33	0 12:25	4.71	1.59	1.00
27inCMP	CONDUIT	19.48	0 12:15	5.00	1.65	1.00
30inRCP	CONDUIT	43.84	0 12:00	8.93	1.19	1.00
36inRCP(2)	CONDUIT	57.56	0 12:00	8.19	2.63	0.99
36inRCP	CONDUIT	64.27	0 12:00	9.51	1.19	0.93
36inCMP(2)	CONDUIT	40.24	0 12:10	6.30	4.24	1.00
24inRCP	CONDUIT	29.69	0 12:00	9.56	1.23	0.96
48inRCP	CONDUIT	148.63	0 12:01	13.48	1.00	0.86
36inCMP	CONDUIT	30.03	0 12:40	4.25	4.62	1.00
26	CONDUIT	27.61	0 11:36	1.95	0.52	0.99
27	CONDUIT	30.84	0 13:33	2.49	0.17	1.00
28	CONDUIT	15.01	0 12:00	0.75	0.04	0.79
29	CONDUIT	38.47	0 12:04	1.09	0.13	1.00
31	CONDUIT	8.76	1 00:18	0.66	0.10	0.99
32	CONDUIT	3.73	0 12:00	0.24	0.01	0.85
33	CONDUIT	2.32	0 12:00	0.23	0.01	0.85
34	CONDUIT	35.04	0 11:54	11.15	1.01	1.00
35	CONDUIT	34.65	0 11:55	11.03	1.00	1.00
36	CONDUIT	34.66	0 11:59	11.03	1.00	1.00
37	CONDUIT	12.66	0 12:45	4.03	1.20	1.00
38	CONDUIT	16.48	0 12:01	6.08	0.16	0.97

325
326
327 *****
328 Flow Classification Summary
329 *****

Adjusted	Fraction of Time in Flow Class
----------	--------------------------------

		/Actual		Up	Down	Sub	Sup	Up	Down	Norm	Inlet
	Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
333											
334											
335											
336	24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
337	12inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.22	0.00
338	24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
339	PipeRecessed	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.97	0.00	0.00
340	15inCMP	1.00	0.00	0.00	0.00	0.75	0.00	0.00	0.24	0.37	0.00
341	21inCMP	1.00	0.00	0.00	0.00	0.06	0.00	0.00	0.94	0.00	0.00
342	27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
343	30inRCP	1.00	0.00	0.00	0.00	0.02	0.05	0.00	0.93	0.02	0.00
344	36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
345	36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
346	36inCMP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
347	24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
348	48inRCP	1.00	0.00	0.00	0.00	0.00	0.99	0.00	0.00	0.39	0.00
349	36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
350	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
351	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
352	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.55	0.00
353	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.51	0.00
354	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
355	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.54	0.00
356	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.54	0.00
357	34	1.00	0.00	0.00	0.00	0.05	0.95	0.00	0.00	0.44	0.00
358	35	1.00	0.00	0.00	0.00	0.06	0.94	0.00	0.00	0.79	0.00
359	36	1.00	0.00	0.00	0.00	0.25	0.74	0.00	0.00	0.43	0.00
360	37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.89	0.00
361	38	1.00	0.00	0.49	0.00	0.51	0.00	0.00	0.00	0.26	0.00
362											
363											

Conduit Surcharge Summary

			Hours Full		Hours	Hours
	Conduit	----- Both Ends	Upstream	----- Dnstream	Above Full Normal Flow	Capacity Limited
368						
369						
370						
371						
372						
373	24inCMP	12.91	13.78	12.93	16.57	12.80
374	12inRCP	2.98	2.98	6.20	0.31	0.31
375	24inRcp (2)	1.54	1.55	1.54	1.58	1.24
376	PipeRecessed	0.30	1.54	0.30	4.14	0.30
377	15inCMP	0.80	0.80	0.86	0.09	0.09
378	21inCMP	0.74	0.82	0.74	0.85	0.74
379	27inCMP	0.32	0.51	0.32	0.83	0.32
380	30inRCP	0.24	0.28	0.24	0.41	0.24
381	36inRCP (2)	0.01	0.20	0.01	0.98	0.01
382	36inRCP	0.01	0.01	0.01	0.21	0.01
383	36inCMP (2)	0.01	9.44	0.01	15.13	0.01
384	24inRCP	0.01	0.07	0.01	0.12	0.01
385	36inCMP	9.44	9.44	13.71	16.06	0.01
386	26	0.01	0.01	0.20	0.01	0.01
387	27	0.20	0.20	1.46	0.01	0.01
388	28	0.01	0.01	1.46	0.01	0.01
389	29	1.46	1.46	13.10	0.01	0.01
390	31	0.01	0.01	0.20	0.01	0.01
391	34	0.57	0.57	1.06	0.26	0.25
392	35	1.06	1.06	1.28	0.01	0.01
393	36	1.28	1.28	1.44	0.01	0.01
394	37	1.44	1.44	1.55	1.01	1.03
395	38	0.01	0.01	14.86	0.01	0.01
396						
397						

Analysis begun on: Mon Nov 28 15:00:13 2022
Analysis ended on: Mon Nov 28 15:00:13 2022
Total elapsed time: < 1 sec

Location 10: Old Washington Rd. and Shoppers World (25-Year (2100) -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
*****	-----	-----
Runoff Quantity Continuity		

Total Precipitation	65.386	7.538
Evaporation Loss	0.000	0.000
Infiltration Loss	6.828	0.787
Surface Runoff	57.873	6.672
Final Storage	0.795	0.092
Continuity Error (%)	-0.168	

	Volume acre-feet	Volume 10^6 gal
*****	-----	-----
Flow Routing Continuity		

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	57.868	18.857
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	54.493	17.757
Flooding Loss	2.571	0.838
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.774	0.252
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.034	0.011
Continuity Error (%)	-0.006	

Time-Step Critical Elements

Link 34 (68.11%)

Link 38 (16.53%)

Link 12inRCP (6.69%)

Link 24inRcp(2) (3.13%)

Link 36inCMP (1.62%)

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*****
Highest Flow Instability Indexes
*****
Link 12inRCP (10)
Link 24inRcp(2) (8)
Link PipeRecessed (4)
Link 28 (2)
Link 31 (1)

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*****
Most Frequent Nonconverging Nodes
*****
Node Out-5 (0.01%)
Node IN-1 (0.01%)
Node MH-1 (0.00%)

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*****
Routing Time Step Summary
*****
Minimum Time Step      :      0.50 sec
Average Time Step      :      2.57 sec
Maximum Time Step      :     20.00 sec
% of Time in Steady State :      0.00
Average Iterations per Step :      2.01
% of Steps Not Converging :      0.01
Time Step Frequencies  :
20.000 - 9.564 sec    :      0.13 %
9.564 - 4.573 sec    :      6.72 %
4.573 - 2.187 sec    :     57.11 %
2.187 - 1.046 sec    :     30.27 %
1.046 - 0.500 sec    :      5.77 %

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*****
Subcatchment Runoff Summary
*****

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		Total		Total	Total	Total	Imperv
		Perv	Total	Total	Peak	Runoff	
		Precip	Runon	Evap	Infil	Runoff	
		Runoff	Runoff	Runoff	Runoff	Coeff	
Subcatchment		in	in	in	in		in
in	in	10^6 gal	CFS				
DA-1		7.54	0.00	0.00	0.94	3.82	
2.67	6.49	11.39	291.05	0.861			
DA-2		7.54	0.00	0.00	0.15	6.84	
0.52	7.37	0.22	11.07	0.977			
DA-3		7.54	0.00	0.00	1.29	1.89	
4.32	6.20	0.81	28.67	0.823			
DA-4		7.54	0.00	0.00	0.53	5.19	
1.78	6.97	1.67	66.48	0.925			
DA-5		7.54	0.00	0.00	0.02	7.44	
0.06	7.50	0.11	5.88	0.994			
DA-6		7.54	0.00	0.00	0.12	7.00	
0.41	7.40	0.42	20.94	0.982			
DA-7		7.54	0.00	0.00	0.19	6.69	
0.64	7.33	0.33	16.78	0.973			
DA-8		7.54	0.00	0.00	0.17	6.77	
0.58	7.35	0.48	24.26	0.975			

124	DA-9		7.54	0.00	0.00	0.12	6.99
	0.41	7.40	0.29	14.92	0.982		
125	DA-10		7.54	0.00	0.00	0.29	6.24
	0.99	7.23	0.16	7.86	0.959		
126	DA-11		7.54	0.00	0.00	0.19	6.69
	0.64	7.33	0.82	41.11	0.973		
127	DA-12		7.54	0.00	0.00	0.60	4.89
	2.02	6.91	0.67	32.10	0.917		
128	DA-13		7.54	0.00	0.00	0.43	6.32
	0.77	7.09	0.33	16.47	0.941		
129	DA-14		7.54	0.00	0.00	1.32	2.56
	3.63	6.19	0.49	19.97	0.821		
130	DA-15		7.54	0.00	0.00	0.32	6.08
	1.10	7.18	0.05	2.88	0.953		
131	DA-16		7.54	0.00	0.00	0.46	5.49
	1.56	7.05	0.09	4.40	0.936		
132	DA-BASIN		7.54	0.00	0.00	0.46	5.49
	1.56	7.05	0.52	26.08	0.936		

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135 *****

136 Node Depth Summary

137 *****

			Average	Maximum	Maximum	Time of Max		Reported	
			Depth	Depth	HGL	Occurrence		Max	Depth
	Node	Type	Feet	Feet	Feet	days	hr:min		Feet
139									
140									
141									
142									
143									
144	MH-1	JUNCTION	1.08	3.84	206.58	0	12:00		3.83
145	Out-4	JUNCTION	3.92	6.52	205.03	0	12:25		6.51
146	IN-1	JUNCTION	3.63	5.62	206.72	0	14:37		5.62
147	Out-1	JUNCTION	2.14	4.06	205.06	0	12:25		4.05
148	Out-3	JUNCTION	0.81	2.43	205.04	0	12:25		2.42
149	Out-6	JUNCTION	1.17	3.04	205.04	0	12:25		3.04
150	Out-2	JUNCTION	1.17	3.04	205.04	0	12:25		3.04
151	Jun-1	JUNCTION	1.94	4.04	205.04	0	12:24		4.04
152	Jun-2	JUNCTION	2.04	4.14	205.04	0	12:25		4.14
153	Jun-3	JUNCTION	2.28	4.64	205.04	0	12:25		4.63
154	Out-5	OUTFALL	1.11	3.58	200.22	0	12:01		3.28
155	IN-2	STORAGE	0.74	4.16	207.26	0	12:04		4.12
156	IN-3	STORAGE	1.07	3.82	206.58	0	12:00		3.80
157	ExistingBasin	STORAGE	1.11	3.43	201.63	0	12:02		3.31
158	IN-12	STORAGE	0.25	2.99	205.89	0	12:00		2.94
159	IN-11	STORAGE	2.48	4.57	203.20	0	12:08		4.53
160	IN-10	STORAGE	0.62	3.11	203.28	0	12:00		3.09
161	IN-9	STORAGE	0.84	3.75	204.13	0	12:00		3.73
162	IN-8	STORAGE	0.62	4.01	206.28	0	12:00		3.98
163	IN-5	STORAGE	0.37	4.19	211.48	0	12:07		4.16
164	IN-6	STORAGE	0.55	4.46	210.23	0	12:11		4.45
165	IN-7	STORAGE	0.54	4.34	208.19	0	12:07		4.25
166	BMP1	STORAGE	0.41	3.00	208.00	0	11:53		3.00
167	BMP2	STORAGE	0.46	3.00	207.50	0	11:54		3.00
168	BMP3	STORAGE	0.57	3.00	207.00	0	11:51		3.00
169	BMP4	STORAGE	0.81	3.00	206.50	0	11:46		3.00
170	BMP5	STORAGE	0.55	2.03	205.03	0	12:25		2.03

171

172

173 *****

174 Node Inflow Summary

175 *****

176

177

178		Maximum	Maximum		Lateral
		Total	Flow		
179		Lateral	Total	Time of Max	Inflow
		Inflow	Balance		

180				Inflow	Inflow	Occurrence	Volume	
181	Node		Type	Volume	Error			
	gal	Percent		CFS	CFS	days hr:min	10^6 gal	10^6
182								
183	MH-1		JUNCTION	0.00	15.65	0 12:11	0	
	1.88	-0.052						
184	Out-4		JUNCTION	0.00	48.99	0 11:59	0	
	12.3	0.032						
185	IN-1		JUNCTION	291.05	291.05	0 12:05	11.4	
	11.4	-0.006						
186	Out-1		JUNCTION	0.00	27.70	0 11:32	0	
	11.4	0.008						
187	Out-3		JUNCTION	16.47	16.47	0 12:00	0.327	
	0.328	-0.019						
188	Out-6		JUNCTION	4.40	4.40	0 12:00	0.0919	
	0.0939	-0.022						
189	Out-2		JUNCTION	2.88	2.88	0 12:00	0.0546	
	0.0574	-0.030						
190	Jun-1		JUNCTION	0.00	9.51	1 01:22	0	
	0.17	0.224						
191	Jun-2		JUNCTION	0.00	28.66	0 14:17	0	
	11.6	0.011						
192	Jun-3		JUNCTION	0.00	41.44	0 12:02	0	
	11.9	0.007						
193	Out-5		OUTFALL	0.00	149.10	0 12:01	0	
	17.8	0.000						
194	IN-2		STORAGE	11.07	11.07	0 12:00	0.218	
	0.244	0.558						
195	IN-3		STORAGE	0.00	12.65	0 12:47	0	
	1.64	0.010						
196	ExistingBasin		STORAGE	26.08	155.20	0 12:00	0.521	
	17.8	0.004						
197	IN-12		STORAGE	32.10	32.10	0 12:00	0.666	
	0.666	0.003						
198	IN-11		STORAGE	41.11	62.13	0 12:00	0.824	
	12.9	0.008						
199	IN-10		STORAGE	7.86	65.78	0 12:00	0.155	
	3.65	0.002						
200	IN-9		STORAGE	14.92	58.26	0 11:59	0.293	
	3.5	0.002						
201	IN-8		STORAGE	24.26	44.80	0 11:59	0.483	
	3.2	0.016						
202	IN-5		STORAGE	5.88	5.88	0 12:00	0.114	
	0.114	0.036						
203	IN-6		STORAGE	20.94	23.36	0 12:00	0.424	
	0.538	0.028						
204	IN-7		STORAGE	16.78	24.59	0 12:00	0.33	
	0.868	-0.090						
205	BMP1		STORAGE	66.48	66.48	0 12:00	1.67	
	1.67	0.002						
206	BMP2		STORAGE	0.00	35.06	0 11:53	0	
	1.53	-0.001						
207	BMP3		STORAGE	28.67	63.31	0 12:00	0.807	
	2.34	0.005						
208	BMP4		STORAGE	0.00	35.44	0 12:01	0	
	2.13	-0.002						
209	BMP5		STORAGE	19.97	27.99	0 12:01	0.485	
	0.727	0.003						
210								
211								
212	*****							
213	Node Surcharge Summary							
214	*****							
215								
216	Surcharging occurs when water rises above the top of the highest conduit.							
217	-----							

			Hours	Max. Height	Min. Depth
			Surcharged	Above Crown	Below Rim
	Node	Type		Feet	Feet
221	-----	-----	-----	-----	-----
222	MH-1	JUNCTION	1.61	1.841	0.159
223	Out-4	JUNCTION	14.22	2.518	0.000
224	IN-1	JUNCTION	14.98	3.621	0.000
225	Out-1	JUNCTION	0.43	0.058	0.942
226	Jun-1	JUNCTION	0.37	0.045	0.955
227	Jun-2	JUNCTION	0.65	0.145	0.855
228	Jun-3	JUNCTION	1.66	0.638	0.362

231 *****

232 Node Flooding Summary

233 *****

235 Flooding refers to all water that overflows a node, whether it ponds or not.

					Total	Maximum
		Hours	Maximum	Time of Max	Flood	Ponded
		Flooded	Rate	Occurrence	Volume	Depth
	Node		CFS	days hr:min	10^6 gal	Feet
241	-----	-----	-----	-----	-----	-----
242	Out-4	14.22	28.70	0 11:59	0.342	2.518
243	IN-1	13.81	270.27	0 12:05	4.642	0.621
244	BMP1	0.28	31.74	0 12:00	0.140	0.000
245	BMP2	0.01	0.37	0 11:54	0.000	0.000
246	BMP3	0.42	28.60	0 12:00	0.209	0.000
247	BMP4	1.01	35.39	0 12:01	0.489	0.000

250 *****

251 Storage Volume Summary

252 *****

		Average	Avg	Evap	Exfil	Maximum	Max	Time of
		Max	Maximum					
		Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
		Occurrence	Outflow					
257	Storage Unit	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
258	hr:min CFS							

259	IN-2	0.018	0	0	0	1.336	3	0
	12:04 8.65							
260	IN-3	0.010	0	0	0	0.034	0	0
	12:00 14.81							
261	ExistingBasin	1.300	8	0	0	7.823	50	0
	12:02 149.10							
262	IN-12	0.002	0	0	0	0.027	0	0
	12:00 31.77							
263	IN-11	0.494	1	0	0	16.297	33	0
	12:08 40.76							
264	IN-10	0.006	0	0	0	0.028	0	0
	12:00 65.84							
265	IN-9	0.008	0	0	0	0.034	0	0
	12:00 58.06							
266	IN-8	0.006	0	0	0	0.046	0	0
	12:00 43.82							
267	IN-5	0.040	0	0	0	1.889	4	0
	12:07 2.52							
268	IN-6	0.339	1	0	0	10.528	21	0
	12:11 11.36							
269	IN-7	0.100	0	0	0	5.788	12	0

270	12:07	19.57						
	BMP1		0.065	6	0	0	1.125	100
	11:53	35.11						0
271	BMP2		0.083	7	0	0	1.125	100
	11:54	34.70						0
272	BMP3		0.116	10	0	0	1.125	100
	11:51	34.71						0
273	BMP4		0.179	16	0	0	1.125	100
	11:46	12.70						0
274	BMP5		5.513	18	0	34	20.346	68
	12:25	16.43						0

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.86	28.81	149.10	17.756
System	99.86	28.81	149.10	17.756

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.70	0 11:32	8.82	5.40	1.00
12inRCP	CONDUIT	8.65	0 12:11	11.02	1.72	1.00
24inRcp(2)	CONDUIT	14.81	0 12:11	4.71	2.09	1.00
PipeRecessed	CONDUIT	15.67	0 12:11	5.01	4.11	1.00
15inCMP	CONDUIT	2.52	0 11:52	2.08	1.03	1.00
21inCMP	CONDUIT	11.36	0 12:25	4.72	1.59	1.00
27inCMP	CONDUIT	19.57	0 12:15	5.01	1.66	1.00
30inRCP	CONDUIT	43.82	0 11:59	8.93	1.19	1.00
36inRCP(2)	CONDUIT	58.06	0 12:00	8.21	2.65	1.00
36inRCP	CONDUIT	65.84	0 12:00	9.60	1.22	0.93
36inCMP(2)	CONDUIT	40.76	0 12:10	6.37	4.29	1.00
24inRCP	CONDUIT	31.77	0 12:00	10.21	1.32	0.97
48inRCP	CONDUIT	149.10	0 12:01	13.48	1.00	0.88
36inCMP	CONDUIT	30.32	0 12:47	4.29	4.66	1.00
26	CONDUIT	27.48	0 11:33	1.95	0.51	1.00
27	CONDUIT	30.99	0 13:54	2.49	0.17	1.00
28	CONDUIT	15.79	0 12:00	0.74	0.04	0.80
29	CONDUIT	41.25	0 12:02	1.15	0.14	1.00
31	CONDUIT	9.51	1 01:22	0.71	0.11	1.00
32	CONDUIT	4.05	0 12:01	0.26	0.01	0.88
33	CONDUIT	2.52	0 12:01	0.26	0.01	0.88
34	CONDUIT	35.06	0 11:53	11.16	1.01	1.00
35	CONDUIT	34.65	0 11:54	11.03	1.00	1.00
36	CONDUIT	34.66	0 12:13	11.03	1.00	1.00
37	CONDUIT	12.65	0 12:47	4.03	1.20	1.00
38	CONDUIT	15.97	0 14:06	6.06	0.15	1.00

Flow Classification Summary

		Adjusted	Fraction of Time in Flow Class								
		/Actual	Up		Down		Sub	Sup	Up	Down	Inlet
		Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
Conduit											
24inCMP	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
12inRCP	1.00	0.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.21	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.00	0.76	0.00	0.00	0.23	0.40	0.00
21inCMP	1.00	0.00	0.00	0.00	0.00	0.06	0.00	0.00	0.94	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.00	0.02	0.06	0.00	0.92	0.02	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
36inCMP (2)	1.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.99	0.00	0.00	0.40	0.00
36inCMP	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
26	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.00	0.02	0.00
28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.52	0.00
29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.47	0.00
31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.02	0.00
32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.50	0.00
33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.50	0.00
34	1.00	0.00	0.00	0.00	0.05	0.95	0.00	0.00	0.00	0.41	0.00
35	1.00	0.00	0.00	0.00	0.06	0.94	0.00	0.00	0.00	0.78	0.00
36	1.00	0.00	0.00	0.00	0.26	0.74	0.00	0.00	0.00	0.40	0.00
37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.89	0.00
38	1.00	0.00	0.45	0.00	0.55	0.00	0.00	0.00	0.00	0.22	0.00

Conduit Surcharge Summary

		Hours Full		Hours		Hours
		Both Ends	Upstream	Dnstream	Above Full	Capacity
Conduit					Normal Flow	Limited
24inCMP	14.03	14.98	14.06	18.13	13.96	
12inRCP	3.20	3.20	6.71	0.34	0.34	
24inRcp (2)	1.61	1.63	1.61	1.70	1.29	
PipeRecessed	0.32	1.61	0.32	4.51	0.32	
15inCMP	0.88	0.88	0.93	0.08	0.09	
21inCMP	0.80	0.90	0.80	0.93	0.80	
27inCMP	0.34	0.56	0.34	0.91	0.34	
30inRCP	0.26	0.30	0.26	0.45	0.26	
36inRCP (2)	0.02	0.22	0.02	1.05	0.02	
36inRCP	0.01	0.05	0.01	0.23	0.01	
36inCMP (2)	0.08	10.73	0.08	16.50	0.08	
24inRCP	0.01	0.11	0.01	0.15	0.01	
48inRCP	0.01	0.01	0.01	0.06	0.01	
36inCMP	10.73	10.73	14.88	17.38	0.01	
26	0.43	0.43	0.65	0.01	0.01	
27	0.65	0.65	1.66	0.01	0.01	
28	0.01	0.01	1.66	0.01	0.01	
29	1.66	1.66	14.22	0.01	0.01	
31	0.37	0.37	0.65	0.01	0.01	
32	0.01	0.01	0.37	0.01	0.01	
33	0.01	0.01	0.37	0.01	0.01	
34	0.61	0.61	1.12	0.28	0.27	
35	1.12	1.12	1.34	0.01	0.01	
36	1.34	1.34	1.51	0.01	0.01	
37	1.51	1.51	1.63	1.05	1.07	
38	0.32	0.32	16.07	0.01	0.01	

```
402 Analysis begun on: Mon Nov 28 14:59:30 2022
403 Analysis ended on: Mon Nov 28 14:59:30 2022
404 Total elapsed time: < 1 sec
```

Location 10: Old Washington Rd. and Shoppers World (100-Year -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume acre-feet	Depth inches
Runoff Quantity Continuity		
Total Precipitation	75.621	8.718
Evaporation Loss	0.000	0.000
Infiltration Loss	7.050	0.813
Surface Runoff	67.880	7.826
Final Storage	0.818	0.094
Continuity Error (%)	-0.169	

	Volume acre-feet	Volume 10^6 gal
Flow Routing Continuity		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	67.908	22.129
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	63.661	20.745
Flooding Loss	3.314	1.080
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.894	0.291
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.035	0.011
Continuity Error (%)	0.006	

Time-Step Critical Elements

Link 34 (65.31%)

Link 38 (18.93%)

Link 12inRCP (7.34%)

Link 24inRcp(2) (4.03%)

Link 36 (1.38%)

```

*****
Highest Flow Instability Indexes
*****
Link 12inRCP (8)
Link 24inRcp(2) (6)
Link PipeRecessed (4)
Link 28 (1)
Link 31 (1)

```

```

*****
Most Frequent Nonconverging Nodes
*****
Node Out-5 (0.02%)
Node IN-1 (0.01%)
Node MH-1 (0.00%)
Node IN-2 (0.00%)
Node IN-3 (0.00%)

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      :      0.50 sec
Average Time Step      :      2.44 sec
Maximum Time Step      :     20.00 sec
% of Time in Steady State :      0.00
Average Iterations per Step :      2.01
% of Steps Not Converging :      0.02
Time Step Frequencies  :
    20.000 -  9.564 sec :      0.11 %
     9.564 -  4.573 sec :      3.31 %
     4.573 -  2.187 sec :     59.72 %
     2.187 -  1.046 sec :     32.42 %
     1.046 -  0.500 sec :      4.45 %

```

```

*****
Subcatchment Runoff Summary
*****

```

		Total Perv Precip Runoff		Total Runon Runoff	Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
Subcatchment	in	10^6 gal	in	in	in	in	in
DA-1		8.72	0.00	0.00	0.97	4.43	
3.21	7.64	13.41	351.90	0.876			
DA-2		8.72	0.00	0.00	0.16	7.92	
0.62	8.54	0.25	12.90	0.980			
DA-3		8.72	0.00	0.00	1.33	2.18	
5.16	7.34	0.95	34.98	0.842			
DA-4		8.72	0.00	0.00	0.55	6.00	
2.13	8.14	1.95	79.58	0.933			
DA-5		8.72	0.00	0.00	0.02	8.61	
0.07	8.68	0.13	6.82	0.995			
DA-6		8.72	0.00	0.00	0.12	8.10	
0.49	8.58	0.49	24.47	0.984			
DA-7		8.72	0.00	0.00	0.19	7.75	
0.76	8.51	0.38	19.57	0.976			

125	DA-8		8.72	0.00	0.00	0.18	7.83
	0.69	8.53	0.56	28.34	0.978		
126	DA-9		8.72	0.00	0.00	0.12	8.09
	0.48	8.58	0.34	17.38	0.984		
127	DA-10		8.72	0.00	0.00	0.30	7.22
	1.18	8.40	0.18	9.20	0.964		
128	DA-11		8.72	0.00	0.00	0.19	7.75
	0.76	8.51	0.96	48.07	0.976		
129	DA-12		8.72	0.00	0.00	0.62	5.66
	2.42	8.08	0.78	37.96	0.927		
130	DA-13		8.72	0.00	0.00	0.45	7.31
	0.94	8.25	0.38	19.32	0.947		
131	DA-14		8.72	0.00	0.00	1.36	2.96
	4.36	7.32	0.57	24.20	0.840		
132	DA-15		8.72	0.00	0.00	0.33	7.04
	1.32	8.35	0.06	3.35	0.958		
133	DA-16		8.72	0.00	0.00	0.48	6.35
	1.87	8.22	0.11	5.19	0.943		
134	DA-BASIN		8.72	0.00	0.00	0.48	6.35
	1.87	8.22	0.61	30.65	0.943		

Node Depth Summary

		Average	Maximum	Maximum	Time of Max		Reported
		Depth	Depth	HGL	Occurrence		Max Depth
Node	Type	Feet	Feet	Feet	days	hr:min	Feet
MH-1	JUNCTION	1.07	3.85	206.59	0	11:58	3.82
Out-4	JUNCTION	4.18	6.86	205.37	0	12:21	6.84
IN-1	JUNCTION	3.96	5.80	206.90	0	14:57	5.80
Out-1	JUNCTION	2.31	4.40	205.40	0	12:21	4.37
Out-3	JUNCTION	0.90	2.77	205.38	0	12:21	2.75
Out-6	JUNCTION	1.30	3.39	205.39	0	12:20	3.37
Out-2	JUNCTION	1.29	3.39	205.39	0	12:21	3.37
Jun-1	JUNCTION	2.11	4.39	205.39	0	12:20	4.37
Jun-2	JUNCTION	2.21	4.49	205.39	0	12:21	4.47
Jun-3	JUNCTION	2.48	4.98	205.38	0	12:21	4.96
Out-5	OUTFALL	1.16	3.67	200.31	0	12:01	3.64
IN-2	STORAGE	0.74	4.22	207.32	0	12:05	4.17
IN-3	STORAGE	1.07	3.82	206.58	0	11:58	3.79
ExistingBasin	STORAGE	1.16	3.71	201.91	0	12:01	3.63
IN-12	STORAGE	0.26	4.04	206.94	0	12:00	4.02
IN-11	STORAGE	2.62	4.71	203.34	0	12:09	4.69
IN-10	STORAGE	0.62	3.27	203.44	0	12:00	3.26
IN-9	STORAGE	0.84	3.94	204.32	0	12:00	3.94
IN-8	STORAGE	0.61	4.11	206.38	0	12:01	4.09
IN-5	STORAGE	0.33	4.23	211.52	0	12:08	4.21
IN-6	STORAGE	0.51	4.53	210.30	0	12:12	4.52
IN-7	STORAGE	0.50	4.41	208.26	0	12:08	4.36
BMP1	STORAGE	0.39	3.00	208.00	0	11:52	3.00
BMP2	STORAGE	0.43	3.00	207.50	0	11:52	3.00
BMP3	STORAGE	0.55	3.00	207.00	0	11:49	3.00
BMP4	STORAGE	0.80	3.00	206.50	0	11:44	3.00
BMP5	STORAGE	0.63	2.39	205.39	0	12:21	2.37

Node Inflow Summary

		Maximum	Maximum	Lateral
		Total	Flow	

181				Lateral	Total	Time of Max	Inflow	
182				Inflow	Balance			
				Inflow	Inflow	Occurrence	Volume	
183	Node		Type	Volume	Error			
	gal			CFS	CFS	days hr:min	10^6 gal	10^6
184	Percent							

185	MH-1		JUNCTION	0.00	16.01	0 12:14	0	
	2.1	-0.045						
186	Out-4		JUNCTION	0.00	48.05	0 11:55	0	
	14.5	0.029						
187	IN-1		JUNCTION	351.90	351.90	0 12:05	13.4	
	13.4	-0.001						
188	Out-1		JUNCTION	0.00	27.61	0 11:21	0	
	13.4	0.007						
189	Out-3		JUNCTION	19.32	19.32	0 12:00	0.381	
	0.381	-0.031						
190	Out-6		JUNCTION	5.19	5.19	0 12:00	0.107	
	0.109	-0.086						
191	Out-2		JUNCTION	3.35	3.35	0 12:00	0.0635	
	0.0661	-0.125						
192	Jun-1		JUNCTION	0.00	9.90	1 03:51	0	
	0.193	0.685						
193	Jun-2		JUNCTION	0.00	29.76	0 14:39	0	
	13.6	0.013						
194	Jun-3		JUNCTION	0.00	45.10	0 11:59	0	
	14	0.013						
195	Out-5		OUTFALL	0.00	161.17	0 12:01	0	
	20.7	0.000						
196	IN-2		STORAGE	12.90	12.90	0 12:00	0.253	
	0.274	0.517						
197	IN-3		STORAGE	0.00	12.63	0 12:53	0	
	1.83	0.008						
198	ExistingBasin		STORAGE	30.65	165.21	0 12:00	0.608	
	20.7	0.004						
199	IN-12		STORAGE	37.96	37.96	0 12:00	0.779	
	0.779	0.005						
200	IN-11		STORAGE	48.07	70.30	0 12:00	0.957	
	15.2	0.007						
201	IN-10		STORAGE	9.20	68.64	0 12:00	0.18	
	4.16	0.007						
202	IN-9		STORAGE	17.38	59.69	0 12:00	0.34	
	3.98	0.003						
203	IN-8		STORAGE	28.34	46.80	0 12:00	0.561	
	3.64	0.014						
204	IN-5		STORAGE	6.82	6.82	0 12:00	0.132	
	0.132	0.035						
205	IN-6		STORAGE	24.47	26.87	0 12:00	0.492	
	0.624	0.039						
206	IN-7		STORAGE	19.57	27.38	0 12:00	0.384	
	1.01	-0.052						
207	BMP1		STORAGE	79.58	79.58	0 12:00	1.95	
	1.95	-0.019						
208	BMP2		STORAGE	0.00	35.10	0 11:52	0	
	1.73	-0.000						
209	BMP3		STORAGE	34.98	69.62	0 12:00	0.955	
	2.68	-0.013						
210	BMP4		STORAGE	0.00	37.15	0 12:03	0	
	2.41	-0.010						
211	BMP5		STORAGE	24.20	30.67	0 11:58	0.575	
	0.811	0.002						
212								
213								
214	*****							
215	Node Surcharge Summary							
216	*****							
217								

218 Surcharging occurs when water rises above the top of the highest conduit.

219 -----

Node	Type	Hours Surcharged	Max. Height	Min. Depth
			Above Crown Feet	Below Rim Feet

223 -----

MH-1	JUNCTION	1.83	1.848	0.152
Out-4	JUNCTION	16.94	2.861	0.000
IN-1	JUNCTION	17.87	3.798	0.000
Out-1	JUNCTION	1.07	0.398	0.602
Jun-1	JUNCTION	1.04	0.387	0.613
Jun-2	JUNCTION	1.19	0.487	0.513
Jun-3	JUNCTION	2.28	0.981	0.019

233 *****

234 Node Flooding Summary

235 *****

237 Flooding refers to all water that overflows a node, whether it ponds or not.

238 -----

Node	Hours Flooded	Maximum	Time of Max Occurrence days hr:min	Total	Maximum
		Rate CFS		Flood Volume 10^6 gal	Ponded Depth Feet

243 -----

Out-4	16.94	27.44	0 11:55	0.356	2.861
IN-1	16.49	333.22	0 12:05	5.971	0.798
BMP1	0.33	44.82	0 12:00	0.222	0.000
BMP2	0.01	0.43	0 11:52	0.000	0.000
BMP3	0.51	34.90	0 12:00	0.278	0.000
BMP4	1.15	37.11	0 12:03	0.578	0.000

252 *****

253 Storage Volume Summary

254 *****

257			Average	Avg	Evap	Exfil		Maximum	Max	Time of
			Max	Maximum						
258			Volume	Pcnt	Pcnt	Pcnt		Volume	Pcnt	
			Occurrence		Outflow					
259	Storage Unit		1000 ft3	Full	Loss	Loss		1000 ft3	Full	days
	hr:min	CFS								

271	12:12	11.44							
	IN-7		0.079	0	0	0	8.603	17	0
272	12:08	19.87							
	BMP1		0.055	5	0	0	1.125	100	0
273	11:52	35.15							
	BMP2		0.072	6	0	0	1.125	100	0
274	11:52	34.70							
	BMP3		0.104	9	0	0	1.125	100	0
275	11:49	34.71							
	BMP4		0.169	15	0	0	1.125	100	0
276	11:44	12.68							
	BMP5		6.277	21	0	35	23.855	80	0
	12:21	16.07							

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.87	30.15	161.17	20.743
System	99.87	30.15	161.17	20.743

 Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.61	0 11:21	8.79	5.38	1.00
12inRCP	CONDUIT	8.92	0 12:12	11.36	1.77	1.00
24inRcp(2)	CONDUIT	14.92	0 12:14	4.75	2.11	1.00
PipeRecessed	CONDUIT	16.06	0 12:14	5.16	4.21	1.00
15inCMP	CONDUIT	2.52	0 11:51	2.10	1.03	1.00
21inCMP	CONDUIT	11.44	0 12:32	4.75	1.60	1.00
27inCMP	CONDUIT	19.87	0 12:15	5.09	1.69	1.00
30inRCP	CONDUIT	45.17	0 12:04	9.20	1.23	1.00
36inRCP(2)	CONDUIT	59.47	0 12:00	8.41	2.72	1.00
36inRCP	CONDUIT	68.54	0 12:00	9.92	1.27	0.95
36inCMP(2)	CONDUIT	41.94	0 12:11	6.52	4.41	1.00
24inRCP	CONDUIT	36.38	0 12:01	11.58	1.51	1.00
48inRCP	CONDUIT	161.17	0 12:01	13.48	1.08	0.92
36inCMP	CONDUIT	30.75	0 13:07	4.35	4.73	1.00
26	CONDUIT	27.57	0 16:24	1.94	0.52	1.00
27	CONDUIT	32.09	0 14:39	2.49	0.17	1.00
28	CONDUIT	19.15	0 12:00	0.81	0.05	0.85
29	CONDUIT	44.84	0 11:59	1.25	0.15	1.00
31	CONDUIT	9.90	1 03:51	0.74	0.11	1.00
32	CONDUIT	4.89	0 11:59	0.26	0.02	0.92
33	CONDUIT	3.15	0 11:58	0.26	0.01	0.92
34	CONDUIT	35.10	0 11:52	11.17	1.01	1.00
35	CONDUIT	34.65	0 11:53	11.03	1.00	1.00
36	CONDUIT	34.66	0 11:59	11.03	1.00	1.00
37	CONDUIT	12.63	0 12:53	4.02	1.20	1.00
38	CONDUIT	15.61	0 14:52	5.98	0.15	1.00

 Flow Classification Summary

333											
334											
335		Adjusted	----- Fraction of Time in Flow Class -----								
336		/Actual									
337	Conduit	Length	Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
338											
339	24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
340	12inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.19	0.00
341	24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
342	PipeRecessed	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
343	15inCMP	1.00	0.00	0.00	0.00	0.77	0.00	0.00	0.22	0.46	0.00
344	21inCMP	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.92	0.00	0.00
345	27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
346	30inRCP	1.00	0.00	0.00	0.00	0.02	0.07	0.00	0.91	0.02	0.00
347	36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
348	36inRCP	1.00	0.00	0.00	0.00	0.06	0.01	0.00	0.92	0.07	0.00
349	36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
350	24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
351	48inRCP	1.00	0.00	0.00	0.00	0.01	0.99	0.00	0.00	0.37	0.00
352	36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
353	26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
354	27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
355	28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.43	0.00
356	29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.36	0.00
357	31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
358	32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.41	0.00
359	33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.41	0.00
360	34	1.00	0.00	0.00	0.00	0.06	0.94	0.00	0.00	0.41	0.00
361	35	1.00	0.00	0.00	0.00	0.07	0.93	0.00	0.00	0.72	0.00
362	36	1.00	0.00	0.00	0.00	0.28	0.72	0.00	0.00	0.36	0.00
363	37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.87	0.00
364	38	1.00	0.00	0.34	0.00	0.66	0.00	0.00	0.00	0.16	0.00
365											
366											
367	*****										
368	Conduit Surcharge Summary										
369	*****										
370											
371											
372											
373			Hours Full			Hours		Hours			
374	Conduit	Both Ends	Upstream	Dnstream		Above Full	Normal Flow	Capacity			Limited
375											
376	24inCMP	16.72	17.87	16.75		21.76		16.67			
377	12inRCP	3.80	3.80	8.50		0.41		0.41			
378	24inRcp (2)	1.83	1.85	1.83		2.00		1.48			
379	PipeRecessed	0.36	1.83	0.36		5.42		0.36			
380	15inCMP	1.09	1.09	1.14		0.09		0.09			
381	21inCMP	0.97	1.11	0.97		1.13		0.97			
382	27inCMP	0.40	0.69	0.40		1.11		0.40			
383	30inRCP	0.29	0.33	0.29		0.57		0.29			
384	36inRCP (2)	0.10	0.25	0.10		1.26		0.10			
385	36inRCP	0.01	0.14	0.01		0.26		0.01			
386	36inCMP (2)	0.16	12.87	0.16		19.45		0.16			
387	24inRCP	0.05	0.18	0.05		0.21		0.05			
388	48inRCP	0.01	0.01	0.01		0.14		0.01			
389	36inCMP	12.87	12.87	17.70		20.96		0.01			
390	26	1.07	1.07	1.19		0.01		0.01			
391	27	1.19	1.19	2.28		0.01		0.01			
392	28	0.01	0.01	2.28		0.01		0.01			
393	29	2.28	2.28	16.94		0.01		0.01			
394	31	1.04	1.04	1.19		0.01		0.01			
395	32	0.01	0.01	1.04		0.01		0.01			
396	33	0.01	0.01	1.04		0.01		0.01			
397	34	0.70	0.70	1.26		0.34		0.33			
398	35	1.26	1.26	1.50		0.01		0.01			
399	36	1.50	1.50	1.70		0.01		0.01			
400	37	1.70	1.70	1.85		1.13		1.13			
401	38	1.03	1.03	19.36		0.01		0.01			

402
403
404 Analysis begun on: Mon Nov 28 14:58:59 2022
405 Analysis ended on: Mon Nov 28 14:59:00 2022
406 Total elapsed time: 00:00:01

Location 10: Old Washington Rd. and Shoppers World (100-Year (2050) -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	86.759	10.002
Evaporation Loss	0.000	0.000
Infiltration Loss	7.243	0.835
Surface Runoff	78.827	9.088
Final Storage	0.840	0.097
Continuity Error (%)	-0.174	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	78.864	25.699
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	72.094	23.493
Flooding Loss	4.155	1.354
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.975	0.318
Initial Stored Volume	0.000	0.000
Final Stored Volume	1.628	0.531
Continuity Error (%)	0.015	

Highest Continuity Errors

Node Jun-1 (6.36%)

Time-Step Critical Elements

```

70 *****
71 Link 34 (60.31%)
72 Link 38 (21.96%)
73 Link 12inRCP (8.90%)
74 Link 24inRcp(2) (2.76%)
75 Link 36 (2.01%)
76
77
78 *****
79 Highest Flow Instability Indexes
80 *****
81 Link 12inRCP (6)
82 Link 24inRcp(2) (5)
83 Link PipeRecessed (3)
84
85
86 *****
87 Most Frequent Nonconverging Nodes
88 *****
89 Node Out-5 (0.01%)
90 Node MH-1 (0.00%)
91 Node IN-2 (0.00%)
92 Node IN-3 (0.00%)
93 Node IN-12 (0.00%)
94
95

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96 *****
97 Routing Time Step Summary
98 *****
99 Minimum Time Step      :      0.50 sec
100 Average Time Step      :      2.30 sec
101 Maximum Time Step      :     20.00 sec
102 % of Time in Steady State :      0.00
103 Average Iterations per Step :      2.01
104 % of Steps Not Converging :      0.01
105 Time Step Frequencies  :
106 20.000 - 9.564 sec      :      0.10 %
107 9.564 - 4.573 sec      :      1.28 %
108 4.573 - 2.187 sec      :     59.20 %
109 2.187 - 1.046 sec      :     34.82 %
110 1.046 - 0.500 sec      :      4.59 %
111
112

```

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113 *****
114 Subcatchment Runoff Summary
115 *****
116
117

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Subcatchment		Total Perv Precip Runoff in	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
118	10^6 gal	CFS				
119						
120						
121						
122	DA-1	10.00	0.00	0.00	0.99	5.08
	3.81	8.89	15.61	420.35	0.889	
123	DA-2	10.00	0.00	0.00	0.16	9.09
	0.74	9.83	0.29	14.91	0.983	
124	DA-3	10.00	0.00	0.00	1.37	2.50
	6.09	8.59	1.12	42.13	0.859	
125	DA-4	10.00	0.00	0.00	0.56	6.89
	2.52	9.41	2.25	94.18	0.941	
126	DA-5	10.00	0.00	0.00	0.02	9.88
	0.08	9.96	0.15	7.85	0.996	

127	DA-6		10.00	0.00	0.00	0.13	9.29
	0.57	9.87	0.57	28.35	0.986		
128	DA-7		10.00	0.00	0.00	0.20	8.89
	0.90	9.79	0.44	22.64	0.979		
129	DA-8		10.00	0.00	0.00	0.18	8.99
	0.82	9.81	0.64	32.79	0.981		
130	DA-9		10.00	0.00	0.00	0.13	9.29
	0.57	9.86	0.39	20.06	0.986		
131	DA-10		10.00	0.00	0.00	0.31	8.29
	1.39	9.68	0.21	10.66	0.968		
132	DA-11		10.00	0.00	0.00	0.20	8.89
	0.90	9.79	1.10	55.69	0.979		
133	DA-12		10.00	0.00	0.00	0.64	6.50
	2.85	9.35	0.90	44.41	0.935		
134	DA-13		10.00	0.00	0.00	0.47	8.39
	1.13	9.52	0.44	22.45	0.952		
135	DA-14		10.00	0.00	0.00	1.40	3.40
	5.17	8.57	0.67	28.96	0.857		
136	DA-15		10.00	0.00	0.00	0.34	8.08
	1.55	9.63	0.07	3.86	0.963		
137	DA-16		10.00	0.00	0.00	0.49	7.29
	2.20	9.50	0.12	6.07	0.950		
138	DA-BASIN		10.00	0.00	0.00	0.49	7.29
	2.20	9.50	0.70	35.67	0.950		

139
140
141 *****
142 Node Depth Summary
143 *****
144

			Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
Node	Type						
MH-1	JUNCTION		1.09	3.86	206.60	0 11:56	3.83
Out-4	JUNCTION		4.44	7.15	205.66	0 12:19	7.14
IN-1	JUNCTION		4.28	6.00	207.10	0 15:18	6.00
Out-1	JUNCTION		2.49	4.69	205.69	0 12:19	4.67
Out-3	JUNCTION		1.03	3.06	205.67	0 12:20	3.05
Out-6	JUNCTION		1.44	3.68	205.68	0 12:20	3.66
Out-2	JUNCTION		1.44	3.68	205.68	0 12:19	3.66
Jun-1	JUNCTION		2.30	4.68	205.68	0 12:19	4.66
Jun-2	JUNCTION		2.39	4.79	205.69	0 12:19	4.76
Jun-3	JUNCTION		2.69	5.27	205.67	0 12:20	5.26
Out-5	OUTFALL		1.21	3.70	200.34	0 12:02	3.69
IN-2	STORAGE		0.76	4.28	207.38	0 12:06	4.21
IN-3	STORAGE		1.09	3.83	206.59	0 11:56	3.81
ExistingBasin	STORAGE		1.21	3.90	202.10	0 12:02	3.83
IN-12	STORAGE		0.26	4.17	207.07	0 12:03	4.12
IN-11	STORAGE		2.76	4.85	203.48	0 12:10	4.84
IN-10	STORAGE		0.64	3.42	203.59	0 12:01	3.40
IN-9	STORAGE		0.86	4.08	204.46	0 12:02	4.05
IN-8	STORAGE		0.63	4.21	206.48	0 12:03	4.16
IN-5	STORAGE		0.36	4.27	211.56	0 12:08	4.25
IN-6	STORAGE		0.54	4.59	210.36	0 12:13	4.59
IN-7	STORAGE		0.53	4.49	208.34	0 12:08	4.45
BMP1	STORAGE		0.40	3.00	208.00	0 11:51	3.00
BMP2	STORAGE		0.44	3.00	207.50	0 11:51	3.00
BMP3	STORAGE		0.56	3.00	207.00	0 11:47	3.00
BMP4	STORAGE		0.82	3.00	206.50	0 11:42	3.00
BMP5	STORAGE		0.74	2.68	205.68	0 12:17	2.68

177
178
179 *****
180 Node Inflow Summary
181 *****
182
183

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
MH-1	JUNCTION	2.16	1.856	0.144
Out-4	JUNCTION	19.21	3.148	0.000
IN-1	JUNCTION	20.67	4.003	0.000
Out-1	JUNCTION	1.59	0.693	0.307
Jun-1	JUNCTION	1.56	0.678	0.322
Jun-2	JUNCTION	1.72	0.786	0.214
Jun-3	JUNCTION	3.15	1.268	0.000

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
Out-4	19.21	27.39	0 11:58	0.332	3.148
IN-1	18.87	404.06	0 12:05	7.501	1.003
Jun-3	0.94	12.16	0 12:06	0.023	0.268
BMP1	0.38	59.44	0 12:00	0.321	0.000
BMP2	0.01	0.48	0 11:51	0.000	0.000
BMP3	0.59	42.05	0 12:00	0.361	0.000
BMP4	1.30	38.18	0 12:05	0.671	0.000

Storage Volume Summary

Storage Unit hr:min	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full Loss	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
IN-2 12:06 9.98	0.029	0	0	0	3.869	8	0
IN-3 11:56 15.12	0.010	0	0	0	0.034	0	0
ExistingBasin 12:02 165.66	1.442	9	0	0	9.886	63	0
IN-12 12:03 37.04	0.007	0	0	0	1.456	3	0
IN-11 12:10 43.03	1.052	2	0	0	36.039	72	0
IN-10 12:01 69.45	0.006	0	0	0	0.031	0	0
IN-9 12:02 60.17	0.008	0	0	0	0.372	1	0

273	IN-8		0.014	0	0	0	2.272	5	0
	12:03	47.89							
274	IN-5		0.052	0	0	0	3.566	7	0
	12:08	2.52							
275	IN-6		0.463	1	0	0	17.644	35	0
	12:13	11.52							
276	IN-7		0.101	0	0	0	11.934	24	0
	12:08	19.95							
277	BMP1		0.057	5	0	0	1.125	100	0
	11:51	35.20							
278	BMP2		0.073	7	0	0	1.125	100	0
	11:51	34.70							
279	BMP3		0.107	9	0	0	1.125	100	0
	11:47	34.71							
280	BMP4		0.175	16	0	0	1.125	100	0
	11:42	12.66							
281	BMP5		7.373	25	0	37	26.816	89	0
	12:17	15.91							

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.89	32.10	165.66	23.491
System	99.89	32.10	165.66	23.491

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.47	0 11:07	8.74	5.35	1.00
12inRCP	CONDUIT	9.98	0 12:09	12.71	1.98	1.00
24inRcp (2)	CONDUIT	15.12	0 12:18	4.81	2.14	1.00
PipeRecessed	CONDUIT	16.17	0 12:16	5.19	4.24	1.00
15inCMP	CONDUIT	2.52	0 11:49	2.10	1.03	1.00
21inCMP	CONDUIT	11.52	0 12:39	4.79	1.61	1.00
27inCMP	CONDUIT	19.95	0 12:19	5.10	1.69	1.00
30inRCP	CONDUIT	47.89	0 12:08	9.76	1.30	1.00
36inRCP (2)	CONDUIT	60.17	0 12:04	8.51	2.75	1.00
36inRCP	CONDUIT	69.45	0 12:00	9.97	1.29	0.99
36inCMP (2)	CONDUIT	43.03	0 12:12	6.66	4.53	1.00
24inRCP	CONDUIT	37.04	0 12:03	11.79	1.53	1.00
48inRCP	CONDUIT	165.66	0 12:02	13.49	1.11	0.95
36inCMP	CONDUIT	31.09	0 13:28	4.40	4.78	1.00
26	CONDUIT	28.33	0 17:06	1.93	0.53	1.00
27	CONDUIT	32.77	0 16:02	2.49	0.18	1.00
28	CONDUIT	21.61	0 12:00	0.84	0.05	0.88
29	CONDUIT	44.75	0 12:01	1.24	0.15	1.00
31	CONDUIT	8.62	0 12:01	0.25	0.10	1.00
32	CONDUIT	5.73	0 12:00	0.20	0.02	0.96
33	CONDUIT	3.54	0 12:01	0.18	0.01	0.96
34	CONDUIT	35.15	0 11:51	11.19	1.01	1.00
35	CONDUIT	34.65	0 11:51	11.03	1.00	1.00
36	CONDUIT	34.66	0 12:06	11.03	1.00	1.00
37	CONDUIT	12.61	0 13:00	4.01	1.20	1.00
38	CONDUIT	15.44	0 11:53	5.92	0.15	1.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	----- Up Dry		Fraction of Down Sub Dry Crit		Time in Flow Class Sup Up Crit Crit		----- Down Norm Crit Ltd		Inlet Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
12inRCP	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.01	0.18	0.00
24inRcp(2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.78	0.00	0.00	0.22	0.56	0.00
21inCMP	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.91	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.90	0.00
30inRCP	1.00	0.00	0.00	0.00	0.03	0.08	0.00	0.89	0.02	0.00
36inRCP(2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.14	0.01	0.00	0.85	0.14	0.00
36inCMP(2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.01	0.99	0.00	0.00	0.33	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.28	0.00
31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
34	1.00	0.00	0.00	0.00	0.06	0.93	0.00	0.00	0.39	0.00
35	1.00	0.00	0.00	0.00	0.08	0.92	0.00	0.00	0.67	0.00
36	1.00	0.00	0.00	0.00	0.30	0.70	0.00	0.00	0.33	0.00
37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.85	0.00
38	1.00	0.00	0.28	0.00	0.72	0.00	0.00	0.00	0.10	0.00

Conduit Surcharge Summary

Conduit	----- Both Ends	Hours Full Upstream	----- Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
24inCMP	19.11	20.67	19.11	24.89	19.11
12inRCP	4.63	4.63	9.98	0.51	0.51
24inRcp(2)	2.16	2.18	2.16	2.36	1.76
PipeRecessed	0.41	2.16	0.41	6.44	0.41
15inCMP	1.32	1.32	1.36	0.09	0.09
21inCMP	1.18	1.34	1.18	1.36	1.18
27inCMP	0.45	0.83	0.45	1.34	0.45
30inRCP	0.32	0.36	0.32	0.67	0.32
36inRCP(2)	0.18	0.30	0.18	1.50	0.18
36inRCP	0.01	0.20	0.01	0.31	0.01
36inCMP(2)	0.22	14.62	0.22	21.99	0.22
24inRCP	0.18	0.23	0.18	0.26	0.18
48inRCP	0.01	0.01	0.01	0.21	0.01
36inCMP	14.62	14.62	20.06	23.69	0.01
26	1.59	1.59	1.72	0.01	0.01
27	1.72	1.72	3.15	0.01	0.01
28	0.01	0.01	3.15	0.01	0.01
29	3.15	3.15	19.21	0.01	0.01
31	1.56	1.56	1.72	0.01	0.01
32	0.01	0.01	1.56	0.01	0.01
33	0.01	0.01	1.56	0.01	0.01

402	34	0.79	0.79	1.42	0.38	0.38
403	35	1.42	1.42	1.70	0.01	0.01
404	36	1.70	1.70	1.97	0.01	0.01
405	37	1.97	1.97	2.18	1.25	1.26
406	38	1.54	1.54	21.65	0.01	0.01
407						
408						
409	Analysis begun on: Mon Nov 28 14:56:18 2022					
410	Analysis ended on: Mon Nov 28 14:56:18 2022					
411	Total elapsed time: < 1 sec					

Location 10: Old Washington Rd. and Shoppers World (100-Year (2100) -PROPOSED)

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 10/01/2022 00:00:00

Ending Date 10/02/2022 06:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	91.495	10.548
Evaporation Loss	0.000	0.000
Infiltration Loss	7.310	0.843
Surface Runoff	83.493	9.625
Final Storage	0.852	0.098
Continuity Error (%)	-0.175	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	83.536	27.221
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	74.037	24.126
Flooding Loss	4.506	1.468
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.986	0.321
Initial Stored Volume	0.000	0.000
Final Stored Volume	3.995	1.302
Continuity Error (%)	0.015	

Highest Continuity Errors

Node Jun-1 (6.31%)

Time-Step Critical Elements

```

70 *****
71 Link 34 (63.11%)
72 Link 38 (17.40%)
73 Link 12inRCP (9.93%)
74 Link 24inRcp(2) (2.67%)
75 Link 36 (2.47%)
76
77
78 *****
79 Highest Flow Instability Indexes
80 *****
81 Link 12inRCP (6)
82 Link 24inRcp(2) (5)
83 Link PipeRecessed (3)
84
85
86 *****
87 Most Frequent Nonconverging Nodes
88 *****
89 Node Out-5 (0.01%)
90 Node MH-1 (0.00%)
91 Node IN-2 (0.00%)
92 Node IN-3 (0.00%)
93 Node IN-12 (0.00%)
94
95
96 *****
97 Routing Time Step Summary
98 *****
99 Minimum Time Step      :      0.50 sec
100 Average Time Step      :      2.27 sec
101 Maximum Time Step      :     20.00 sec
102 % of Time in Steady State :      0.00
103 Average Iterations per Step :      2.01
104 % of Steps Not Converging :      0.01
105 Time Step Frequencies :
106 20.000 - 9.564 sec      :      0.08 %
107 9.564 - 4.573 sec      :      1.23 %
108 4.573 - 2.187 sec      :     58.65 %
109 2.187 - 1.046 sec      :     35.06 %
110 1.046 - 0.500 sec      :      4.97 %
111
112
113 *****
114 Subcatchment Runoff Summary
115 *****
116
117

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Subcatchment		Total Perv Precip Runoff in	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
118	10^6 gal	CFS				
122	DA-1	10.55	0.00	0.00	1.00	5.36
	4.07	9.43	16.55	448.55	0.894	
123	DA-2	10.55	0.00	0.00	0.16	9.59
	0.78	10.37	0.31	15.72	0.983	
124	DA-3	10.55	0.00	0.00	1.38	2.63
	6.49	9.13	1.19	45.07	0.865	
125	DA-4	10.55	0.00	0.00	0.57	7.27
	2.68	9.95	2.38	100.15	0.944	
126	DA-5	10.55	0.00	0.00	0.02	10.42
	0.09	10.51	0.16	8.26	0.996	

127	DA-6		10.55	0.00	0.00	0.13	9.80
	0.61	10.41	0.60	29.92	0.987		
128	DA-7		10.55	0.00	0.00	0.20	9.38
	0.96	10.34	0.47	23.87	0.980		
129	DA-8		10.55	0.00	0.00	0.18	9.49
	0.87	10.36	0.68	34.60	0.982		
130	DA-9		10.55	0.00	0.00	0.13	9.80
	0.61	10.41	0.41	21.15	0.987		
131	DA-10		10.55	0.00	0.00	0.31	8.75
	1.48	10.23	0.22	11.24	0.970		
132	DA-11		10.55	0.00	0.00	0.20	9.38
	0.96	10.34	1.16	58.77	0.980		
133	DA-12		10.55	0.00	0.00	0.64	6.85
	3.04	9.89	0.95	47.02	0.938		
134	DA-13		10.55	0.00	0.00	0.47	8.85
	1.21	10.06	0.46	23.71	0.954		
135	DA-14		10.55	0.00	0.00	1.42	3.58
	5.52	9.10	0.71	30.91	0.863		
136	DA-15		10.55	0.00	0.00	0.35	8.52
	1.65	10.17	0.08	4.07	0.964		
137	DA-16		10.55	0.00	0.00	0.50	7.69
	2.35	10.04	0.13	6.42	0.952		
138	DA-BASIN		10.55	0.00	0.00	0.49	7.69
	2.35	10.04	0.74	37.70	0.952		

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141 *****
142 Node Depth Summary
143 *****
144

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
MH-1	JUNCTION	1.12	3.87	206.61	0 12:04	3.84
Out-4	JUNCTION	4.50	7.26	205.77	0 12:18	7.26
IN-1	JUNCTION	4.36	6.09	207.19	0 15:24	6.09
Out-1	JUNCTION	2.54	4.81	205.81	0 12:20	4.79
Out-3	JUNCTION	1.07	3.17	205.78	0 12:19	3.17
Out-6	JUNCTION	1.49	3.79	205.79	0 12:18	3.78
Out-2	JUNCTION	1.49	3.79	205.79	0 12:18	3.78
Jun-1	JUNCTION	2.35	4.79	205.79	0 12:18	4.78
Jun-2	JUNCTION	2.45	4.90	205.80	0 12:21	4.88
Jun-3	JUNCTION	2.75	5.38	205.78	0 12:19	5.38
Out-5	OUTFALL	1.23	3.70	200.34	0 12:00	3.70
IN-2	STORAGE	0.78	4.30	207.40	0 12:07	4.22
IN-3	STORAGE	1.11	3.84	206.60	0 12:04	3.82
ExistingBasin	STORAGE	1.23	4.01	202.21	0 12:02	3.90
IN-12	STORAGE	0.27	4.22	207.12	0 12:04	4.15
IN-11	STORAGE	2.79	4.90	203.53	0 12:10	4.89
IN-10	STORAGE	0.65	3.53	203.70	0 12:01	3.45
IN-9	STORAGE	0.88	4.14	204.52	0 12:03	4.08
IN-8	STORAGE	0.65	4.25	206.52	0 12:04	4.19
IN-5	STORAGE	0.37	4.28	211.57	0 12:08	4.27
IN-6	STORAGE	0.56	4.62	210.39	0 12:13	4.62
IN-7	STORAGE	0.55	4.51	208.36	0 12:09	4.48
BMP1	STORAGE	0.41	3.00	208.00	0 11:50	3.00
BMP2	STORAGE	0.45	3.00	207.50	0 11:50	3.00
BMP3	STORAGE	0.58	3.00	207.00	0 11:46	3.00
BMP4	STORAGE	0.84	3.00	206.50	0 11:41	3.00
BMP5	STORAGE	0.79	2.80	205.80	0 12:14	2.80

177
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179 *****
180 Node Inflow Summary
181 *****
182
183

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
MH-1	JUNCTION	2.28	1.871	0.129
Out-4	JUNCTION	19.33	3.265	0.000
IN-1	JUNCTION	20.88	4.088	0.000
Out-1	JUNCTION	1.80	0.809	0.191
Jun-1	JUNCTION	1.78	0.788	0.212
Jun-2	JUNCTION	1.94	0.895	0.105
Jun-3	JUNCTION	3.61	1.384	0.000

Node Flooding Summary

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
Out-4	19.33	29.08	0 12:00	0.281	3.265
IN-1	18.97	432.86	0 12:05	8.139	1.088
Jun-3	1.16	16.11	0 12:04	0.033	0.384
BMP1	0.40	65.41	0 12:00	0.363	0.000
BMP2	0.01	0.39	0 11:50	0.000	0.000
BMP3	0.62	45.00	0 12:00	0.396	0.000
BMP4	1.37	38.53	0 12:06	0.709	0.000

Storage Volume Summary

Storage Unit hr:min	Average Max Volume Occurrence 1000 ft3	Avg Maximum Pcnt Full Loss	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
------------------------	--	--	----------------------	-----------------------	-------------------------------	---------------------	-----------------

IN-2 12:07	10.37	0.034	0	0	0	4.450	9	0
IN-3 12:04	14.92	0.010	0	0	0	0.035	0	0
ExistingBasin 12:02	165.65	1.475	9	0	0	10.378	66	0
IN-12 12:04	37.27	0.010	0	0	0	2.382	5	0
IN-11 12:10	43.43	1.311	3	0	0	40.657	81	0
IN-10 12:01	69.54	0.006	0	0	0	0.032	0	0
IN-9 12:03	61.78	0.010	0	0	0	1.031	2	0

273	IN-8		0.018	0	0	0	3.080	6	0
	12:04	48.81							
274	IN-5		0.063	0	0	0	3.937	8	0
	12:08	2.52							
275	IN-6		0.543	1	0	0	19.206	38	0
	12:13	11.55							
276	IN-7		0.121	0	0	0	13.254	26	0
	12:09	20.00							
277	BMP1		0.059	5	0	0	1.125	100	0
	11:50	35.10							
278	BMP2		0.076	7	0	0	1.125	100	0
	11:50	34.70							
279	BMP3		0.112	10	0	0	1.125	100	0
	11:46	34.71							
280	BMP4		0.181	16	0	0	1.125	100	0
	11:41	12.65							
281	BMP5		7.879	26	0	40	28.037	93	0
	12:14	15.47							

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out-5	99.89	32.87	165.65	24.124
System	99.89	32.87	165.65	24.124

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
24inCMP	CONDUIT	27.47	0 18:16	8.74	5.35	1.00
12inRCP	CONDUIT	10.37	0 12:10	13.21	2.06	1.00
24inRcp (2)	CONDUIT	14.92	0 12:20	4.75	2.11	1.00
PipeRecessed	CONDUIT	16.16	0 12:17	5.19	4.24	1.00
15inCMP	CONDUIT	2.52	0 11:49	2.10	1.03	1.00
21inCMP	CONDUIT	11.55	0 12:41	4.80	1.62	1.00
27inCMP	CONDUIT	20.00	0 12:21	5.11	1.70	1.00
30inRCP	CONDUIT	48.81	0 12:09	9.94	1.33	1.00
36inRCP (2)	CONDUIT	61.78	0 12:07	8.74	2.83	1.00
36inRCP	CONDUIT	69.54	0 11:59	9.99	1.29	1.00
36inCMP (2)	CONDUIT	43.43	0 12:13	6.71	4.57	1.00
24inRCP	CONDUIT	37.27	0 12:04	11.86	1.54	1.00
48inRCP	CONDUIT	165.65	0 12:00	13.48	1.11	0.96
36inCMP	CONDUIT	31.24	0 13:37	4.42	4.80	1.00
26	CONDUIT	27.66	0 17:32	1.93	0.52	1.00
27	CONDUIT	28.57	0 17:26	2.49	0.15	1.00
28	CONDUIT	23.13	0 11:59	0.89	0.06	0.90
29	CONDUIT	48.53	0 12:00	1.35	0.16	1.00
31	CONDUIT	10.41	0 12:00	0.29	0.12	1.00
32	CONDUIT	6.34	0 12:00	0.21	0.02	0.97
33	CONDUIT	4.01	0 12:00	0.19	0.01	0.97
34	CONDUIT	35.06	0 11:50	11.16	1.01	1.00
35	CONDUIT	34.65	0 11:51	11.03	1.00	1.00
36	CONDUIT	34.66	0 11:52	11.03	1.00	1.00
37	CONDUIT	12.60	0 13:03	4.01	1.20	1.00
38	CONDUIT	15.01	0 11:53	5.57	0.14	1.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	----- Up Dry		Fraction of Down Sub Dry Crit		Time in Flow Class Sup Up Crit Crit		Down Norm Crit Ltd		Inlet Ctrl
24inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
12inRCP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.18	0.00
24inRcp (2)	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
PipeRecessed	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.96	0.00	0.00
15inCMP	1.00	0.00	0.00	0.00	0.78	0.00	0.00	0.21	0.62	0.00
21inCMP	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.90	0.00	0.00
27inCMP	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	0.00
30inRCP	1.00	0.00	0.00	0.00	0.03	0.08	0.00	0.88	0.03	0.00
36inRCP (2)	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.98	0.00	0.00
36inRCP	1.00	0.00	0.00	0.00	0.14	0.01	0.00	0.85	0.14	0.00
36inCMP (2)	1.00	0.00	0.00	0.00	0.02	0.00	0.00	0.98	0.00	0.00
24inRCP	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48inRCP	1.00	0.00	0.00	0.00	0.01	0.99	0.00	0.00	0.33	0.00
36inCMP	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
26	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
27	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.02	0.00
28	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
29	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.28	0.00
31	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
32	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
33	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
34	1.00	0.00	0.00	0.00	0.07	0.93	0.00	0.00	0.39	0.00
35	1.00	0.00	0.00	0.00	0.08	0.91	0.00	0.00	0.65	0.00
36	1.00	0.00	0.00	0.00	0.31	0.69	0.00	0.00	0.31	0.00
37	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.84	0.00
38	1.00	0.00	0.27	0.00	0.73	0.00	0.00	0.00	0.10	0.00

Conduit Surcharge Summary

Conduit	----- Both Ends	Hours Full Upstream	----- Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
24inCMP	19.21	20.88	19.21	25.15	19.21
12inRCP	4.91	4.91	10.65	0.55	0.55
24inRcp (2)	2.28	2.30	2.28	2.50	1.84
PipeRecessed	0.41	2.28	0.41	6.91	0.35
15inCMP	1.42	1.42	1.46	0.09	0.09
21inCMP	1.27	1.43	1.27	1.45	1.27
27inCMP	0.47	0.89	0.47	1.43	0.47
30inRCP	0.35	0.37	0.35	0.71	0.35
36inRCP (2)	0.21	0.32	0.21	1.60	0.21
36inRCP	0.04	0.22	0.04	0.33	0.04
36inCMP (2)	0.25	15.64	0.25	22.46	0.25
24inRCP	0.21	0.26	0.21	0.28	0.21
48inRCP	0.01	0.03	0.01	0.24	0.01
36inCMP	15.64	15.64	20.24	24.12	0.01
26	1.80	1.80	1.94	0.01	0.01
27	1.94	1.94	3.61	0.01	0.01
28	0.01	0.01	3.61	0.01	0.01
29	3.61	3.61	19.33	0.01	0.01
31	1.78	1.78	1.94	0.01	0.01
32	0.01	0.01	1.78	0.01	0.01
33	0.01	0.01	1.78	0.01	0.01

402	34	0.82	0.82	1.49	0.40	0.39
403	35	1.49	1.49	1.79	0.01	0.01
404	36	1.79	1.79	2.10	0.01	0.01
405	37	2.10	2.10	2.30	1.32	1.33
406	38	1.74	1.74	21.82	0.01	0.01
407						
408						
409	Analysis begun on: Mon Nov 28 14:55:35 2022					
410	Analysis ended on: Mon Nov 28 14:55:36 2022					
411	Total elapsed time: 00:00:01					

Location 12: Existing Industrial Drive and Post Office Road SWMM Schematic



Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	130.610	6.297
Evaporation Loss	0.000	0.000
Infiltration Loss	20.220	0.975
Surface Runoff	102.606	4.947
Final Storage	7.976	0.385
Continuity Error (%)	-0.147	

Flow Routing Continuity

	Volume acre-feet	Volume 10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	102.533	33.412
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	83.923	27.348
Flooding Loss	18.579	6.054
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.032	0.010
Continuity Error (%)	-0.001	

Time-Step Critical Elements

Link C3 (89.68%)

70 Link C6 (5.46%)
 71 Link C7 (4.24%)
 72
 73
 74 *****
 75 Highest Flow Instability Indexes
 76 *****
 77 All links are stable.
 78
 79
 80 *****
 81 Most Frequent Nonconverging Nodes
 82 *****
 83 Node Out1 (0.02%)
 84 Node J2 (0.01%)
 85 Node J1 (0.01%)
 86 Node J3 (0.00%)
 87 Node J8 (0.00%)
 88
 89

90 *****
 91 Routing Time Step Summary
 92 *****
 93 Minimum Time Step : 0.50 sec
 94 Average Time Step : 1.97 sec
 95 Maximum Time Step : 20.00 sec
 96 % of Time in Steady State : 0.00
 97 Average Iterations per Step : 2.00
 98 % of Steps Not Converging : 0.02
 99 Time Step Frequencies :
 100 20.000 - 9.564 sec : 0.12 %
 101 9.564 - 4.573 sec : 1.16 %
 102 4.573 - 2.187 sec : 32.17 %
 103 2.187 - 1.046 sec : 57.44 %
 104 1.046 - 0.500 sec : 9.11 %
 105
 106

107 *****
 108 Subcatchment Runoff Summary
 109 *****
 110
 111

Subcatchment in	in	10 ⁶ gal	Total Perv Precip Runoff in CFS	Total Total Runon Runoff in	Total Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
S1	3.77	4.04	6.30	0.00	0.00	2.10	0.27
S5	2.11	5.15	6.30	0.00	0.00	1.04	3.04
S3	2.05	4.86	6.30	0.00	0.00	1.02	2.81
S6	0.34	6.21	6.30	0.00	0.00	0.02	5.87
S4	1.70	5.54	6.30	0.00	0.00	0.60	3.83
S7	0.89	6.13	6.30	0.00	0.00	0.12	5.24

124 *****
 125 Node Depth Summary

126	*****								
127									
128	-----								
129			Average	Maximum	Maximum	Time of Max		Reported	
130			Depth	Depth	HGL	Occurrence		Max	Depth
131	Node	Type	Feet	Feet	Feet	days	hr:min		Feet
132	-----								
133	J1	JUNCTION	0.34	2.67	197.18	0	12:06		2.64
134	J2	JUNCTION	0.99	3.50	197.14	0	12:03		3.50
135	J3	JUNCTION	4.03	10.70	200.89	0	12:12		10.61
136	J4	JUNCTION	2.74	5.15	196.22	0	11:46		5.15
137	J5	JUNCTION	1.96	4.31	195.81	0	12:11		4.29
138	J6	JUNCTION	2.02	4.26	195.50	0	12:11		4.26
139	J7	JUNCTION	2.49	5.02	196.37	0	11:46		5.02
140	J8	JUNCTION	0.36	2.94	197.33	0	12:05		2.72
141	Out1	OUTFALL	1.95	4.08	195.25	0	12:03		4.08
142									
143									
144	*****								
145	Node Inflow Summary								
146	*****								
147									
148	-----								
149			Maximum	Maximum			Lateral		
150			Total	Flow					
151			Lateral	Total	Time of Max			Inflow	
151			Inflow	Balance	Occurrence			Volume	
152	Node	Type	Inflow	Inflow	Error	days	hr:min	10^6	10^6
152	gal	Percent	CFS	CFS				gal	
153	-----								
154	J1	JUNCTION	6.24	6.24	0	12:05		0.197	
154	0.197	0.011							
155	J2	JUNCTION	0.00	6.21	0	12:07		0	
155	0.197	0.109							
156	J3	JUNCTION	616.53	616.53	0	12:05		27.8	
156	27.8	0.004							
157	J4	JUNCTION	144.08	305.20	0	12:00		4.33	
157	27.4	0.012							
158	J5	JUNCTION	0.00	200.39	0	12:07		0	
158	27.1	0.007							
159	J6	JUNCTION	3.20	205.51	0	12:03		0.0674	
159	27.3	0.005							
160	J7	JUNCTION	1.70	436.09	0	12:12		0.0332	
160	27.9	0.007							
161	J8	JUNCTION	37.99	37.99	0	12:00		0.937	
161	0.937	-0.002							
162	Out1	OUTFALL	0.00	205.51	0	12:03		0	
162	27.3	0.000							
163									
164									
165	*****								
166	Node Surge Summary								
167	*****								
168									
169	Surcharging occurs when water rises above the top of the highest conduit.								
170	-----								
171			Hours	Max. Height	Min. Depth				
172			Surcharged	Above Crown	Below Rim				
173	Node	Type		Feet	Feet				
174	-----								
175	J1	JUNCTION	1.01	0.671	0.000				
176	J2	JUNCTION	1.27	1.460	0.000				
177	J3	JUNCTION	2.57	5.695	0.000				

178	J4	JUNCTION	0.98	0.000	0.000
179	J7	JUNCTION	1.27	0.000	0.000
180	J8	JUNCTION	0.31	0.940	0.000

181

182

183 *****

184 Node Flooding Summary

185 *****

186

187 Flooding refers to all water that overflows a node, whether it ponds or not.

188 -----

		Maximum	Time of Max	Total	Maximum
	Hours	Rate	Occurrence	Flood	Ponded
	Flooded	CFS	days hr:min	Volume	Depth
Node				10^6 gal	Feet
193					
194	J1	0.99	0 12:03	0.012	0.171
195	J2	0.37	0 12:07	0.014	0.000
196	J3	1.30	0 12:00	1.512	3.885
197	J4	0.98	0 12:00	1.266	0.000
198	J7	1.27	0 12:12	4.773	0.000
199	J8	0.27	0 12:00	0.020	0.440

200

201

202 *****

203 Outfall Loading Summary

204 *****

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
	Pcnt	CFS	CFS	10^6 gal
Outfall Node				
210				
211	Out1	99.91	60.97	205.51
212				
213	System	99.91	60.97	205.51
214				

215

216

217 *****

218 Link Flow Summary

219 *****

		Maximum	Time of Max	Maximum	Max/	Max/
		Flow	Occurrence	Veloc	Full	Full
	Type	CFS	days hr:min	ft/sec	Flow	Depth
225						
226	C1	CONDUIT	6.21	0 12:07	1.98	0.22
227	C3	CONDUIT	435.73	0 12:12	22.19	0.77
228	C4	CONDUIT	190.85	0 13:03	10.19	0.77
229	C5	CONDUIT	200.40	0 12:07	11.32	1.21
230	C6	CONDUIT	205.51	0 12:03	11.74	1.87
231	C2	CONDUIT	2.87	0 12:11	4.14	0.88
232	C7	CONDUIT	171.43	0 13:02	8.73	1.14
233	C8	CONDUIT	31.34	0 12:05	9.98	0.74

234

235

236 *****

237 Flow Classification Summary

238 *****

	Adjusted	-----		Fraction of		Time in		Flow Class		-----	
	/Actual	Up		Down	Sub	Sup	Up	Down	Norm	Inlet	
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl	
244											
245	C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.91	
246	C3	1.00	0.00	0.01	0.00	0.98	0.00	0.00	0.00	0.00	

247	C4	1.00	0.00	0.02	0.00	0.93	0.00	0.05	0.00	0.00	0.00
248	C5	1.00	0.00	0.00	0.00	0.15	0.78	0.00	0.07	0.00	0.00
249	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
250	C2	1.00	0.08	0.00	0.00	0.91	0.00	0.00	0.02	0.81	0.00
251	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.01	0.00
252	C8	1.00	0.00	0.00	0.00	0.97	0.01	0.00	0.02	0.90	0.00

253
254

255 *****
256 Conduit Surcharge Summary
257 *****

258

259	-----					
260					Hours	Hours
261		-----	Hours Full	-----	Above Full	Capacity
262	Conduit	Both Ends	Upstream	Dnstream	Normal Flow	Limited
263	-----					
264	C1	1.01	1.01	1.27	0.01	0.01
265	C3	1.27	1.27	2.57	0.01	0.01
266	C4	0.01	0.01	1.33	0.01	0.01
267	C5	0.01	0.01	0.01	1.36	0.01
268	C6	0.01	0.01	0.01	2.28	0.01
269	C2	1.63	1.63	14.10	0.01	0.01
270	C7	0.98	1.29	0.98	1.31	0.98
271	C8	0.31	0.31	4.95	0.01	0.01

272
273

274 Analysis begun on: Wed Nov 30 11:13:20 2022
275 Analysis ended on: Wed Nov 30 11:13:20 2022
276 Total elapsed time: < 1 sec

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year (2050) - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	146.436	7.060
Evaporation Loss	0.000	0.000
Infiltration Loss	20.887	1.007
Surface Runoff	117.361	5.658
Final Storage	8.408	0.405
Continuity Error (%)	-0.150	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	117.281	38.218
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	92.699	30.207
Flooding Loss	24.550	8.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.033	0.011
Continuity Error (%)	-0.001	

Time-Step Critical Elements

Link C3 (88.31%)

Link C6 (6.03%)
Link C7 (5.16%)

Highest Flow Instability Indexes

Link C7 (1)
Link C4 (1)

Most Frequent Nonconverging Nodes

Node Out1 (0.02%)
Node J2 (0.02%)
Node J1 (0.02%)
Node J8 (0.00%)
Node J3 (0.00%)

Routing Time Step Summary

Minimum Time Step : 0.50 sec
Average Time Step : 1.88 sec
Maximum Time Step : 20.00 sec
% of Time in Steady State : 0.00
Average Iterations per Step : 2.01
% of Steps Not Converging : 0.02
Time Step Frequencies :
20.000 - 9.564 sec : 0.07 %
9.564 - 4.573 sec : 1.01 %
4.573 - 2.187 sec : 24.99 %
2.187 - 1.046 sec : 62.94 %
1.046 - 0.500 sec : 10.99 %

Subcatchment Runoff Summary

		Total		Total	Total	Total	Imperv
		Perv		Total	Total	Peak	Runoff
		Precip		Runon	Evap	Infil	Runoff
		Runoff		Runoff	Runoff	Runoff	Coeff
Subcatchment		in		in	in	in	in
in	in	10^6 gal	CFS				
S1		7.06		0.00	0.00	2.19	0.30
4.41	4.71	0.23	7.54	0.667			
S5		7.06		0.00	0.00	1.07	3.42
2.46	5.87	1.07	43.86	0.832			
S3		7.06		0.00	0.00	1.05	3.16
2.41	5.57	31.92	716.83	0.789			
S6		7.06		0.00	0.00	0.02	6.59
0.39	6.97	0.08	3.63	0.988			
S4		7.06		0.00	0.00	0.62	4.30
1.97	6.28	4.91	166.78	0.889			
S7		7.06		0.00	0.00	0.13	5.88
1.01	6.89	0.04	1.91	0.976			

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.37	2.69	197.20	0 12:05	2.65
J2	JUNCTION	1.03	3.50	197.14	0 12:01	3.50
J3	JUNCTION	4.23	11.86	202.05	0 12:12	11.79
J4	JUNCTION	2.86	5.15	196.22	0 11:45	5.15
J5	JUNCTION	2.07	4.32	195.82	0 12:14	4.30
J6	JUNCTION	2.13	4.27	195.51	0 12:04	4.27
J7	JUNCTION	2.61	5.02	196.37	0 11:45	5.02
J8	JUNCTION	0.39	3.28	197.67	0 12:05	2.92
Out1	OUTFALL	2.06	4.09	195.26	0 12:04	4.09

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.23	JUNCTION	7.54	7.54	0 12:05	0.23	
J2	0.23	JUNCTION	0.00	7.52	0 12:06	0	
J3	31.9	JUNCTION	716.83	716.83	0 12:05	31.9	
J4	30.4	JUNCTION	166.78	327.90	0 12:00	4.91	
J5	29.9	JUNCTION	0.00	201.22	0 12:07	0	
J6	30.2	JUNCTION	3.63	206.46	0 12:04	0.0757	
J7	31.9	JUNCTION	1.91	489.02	0 12:12	0.0374	
J8	1.07	JUNCTION	43.86	43.86	0 12:00	1.07	
Out1	30.2	OUTFALL	0.00	206.46	0 12:04	0	

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	1.11	0.687	0.000
J2	JUNCTION	1.41	1.460	0.000

178	J3	JUNCTION	3.02	6.858	0.000
179	J4	JUNCTION	1.10	0.000	0.000
180	J7	JUNCTION	1.49	0.000	0.000
181	J8	JUNCTION	0.38	1.284	0.000

182

183

184 *****

185 Node Flooding Summary

186 *****

187

188 Flooding refers to all water that overflows a node, whether it ponds or not.

	Hours	Maximum	Time of Max		Total	Maximum
	Flooded	Rate	Occurrence		Flood	Ponded
Node		CFS	days	hr:min	Volume	Depth

J1	1.09	4.42	0	12:01	0.013	0.187
J2	0.49	4.82	0	12:06	0.027	0.000
J3	1.53	331.09	0	12:00	1.965	5.048
J4	1.10	159.26	0	12:00	1.577	0.000
J7	1.49	327.90	0	12:12	6.396	0.000
J8	0.34	12.79	0	12:00	0.035	0.784

201

202

203 *****

204 Outfall Loading Summary

205 *****

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CFS	CFS	10^6 gal

Out1	99.94	66.60	206.46	30.205

System	99.94	66.60	206.46	30.205

215

216

217

218 *****

219 Link Flow Summary

220 *****

Link	Type	Maximum	Time of Max		Maximum	Max/	Max/
		Flow	Occurrence		Veloc	Full	Full
		CFS	days	hr:min	ft/sec	Flow	Depth

C1	CONDUIT	7.52	0	12:06	2.39	0.26	1.00
C3	CONDUIT	488.64	0	12:12	24.89	0.86	1.00
C4	CONDUIT	190.93	0	13:14	10.20	0.77	0.92
C5	CONDUIT	201.23	0	12:07	11.32	1.21	0.85
C6	CONDUIT	206.46	0	12:04	11.77	1.88	0.84
C2	CONDUIT	2.86	0	12:14	4.13	0.87	1.00
C7	CONDUIT	172.50	0	13:14	8.79	1.15	1.00
C8	CONDUIT	34.56	0	12:05	11.00	0.82	1.00

235

236

237 *****

238 Flow Classification Summary

239 *****

Conduit	Adjusted	Fraction of Time in Flow Class					-----			
	/Actual	Up		Down	Sub	Sup	Up	Down	Norm	Inlet
	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl

C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.90	0.00

247	C3	1.00	0.00	0.01	0.00	0.98	0.00	0.00	0.00	0.00	0.00
248	C4	1.00	0.00	0.02	0.00	0.94	0.00	0.04	0.00	0.00	0.00
249	C5	1.00	0.00	0.00	0.00	0.17	0.76	0.00	0.06	0.00	0.00
250	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
251	C2	1.00	0.07	0.00	0.00	0.92	0.00	0.00	0.01	0.81	0.00
252	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
253	C8	1.00	0.01	0.00	0.00	0.97	0.01	0.00	0.02	0.88	0.00

254

255

256 *****

257 Conduit Surcharge Summary

258 *****

259

260

261

		-----	Hours Full	-----	Hours	Hours
		Both Ends	Upstream	Dnstream	Above Full	Capacity
Conduit					Normal Flow	Limited

263

C1	1.11	1.11	1.41	0.01	0.01
----	------	------	------	------	------

C3	1.49	1.49	3.02	0.01	0.01
----	------	------	------	------	------

C4	0.01	0.01	1.56	0.01	0.01
----	------	------	------	------	------

C5	0.01	0.01	0.01	1.63	0.01
----	------	------	------	------	------

C6	0.01	0.01	0.01	2.66	0.01
----	------	------	------	------	------

C2	1.91	1.91	15.40	0.01	0.01
----	------	------	-------	------	------

C7	1.11	1.50	1.11	1.55	1.11
----	------	------	------	------	------

C8	0.38	0.38	5.66	0.01	0.01
----	------	------	------	------	------

273

274

275 Analysis begun on: Wed Nov 30 11:13:47 2022

276 Analysis ended on: Wed Nov 30 11:13:47 2022

277 Total elapsed time: < 1 sec

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year (2100) - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	156.205	7.531
Evaporation Loss	0.000	0.000
Infiltration Loss	21.248	1.024
Surface Runoff	126.355	6.092
Final Storage	8.843	0.426
Continuity Error (%)	-0.154	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	126.266	41.146
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	97.887	31.898
Flooding Loss	28.346	9.237
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.036	0.012
Continuity Error (%)	-0.002	

Time-Step Critical Elements

Link C3 (87.51%)

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.38	2.70	197.21	0 12:05	2.66
J2	JUNCTION	1.05	3.50	197.14	0 12:00	3.50
J3	JUNCTION	4.35	12.59	202.78	0 12:13	12.53
J4	JUNCTION	2.93	5.15	196.22	0 11:44	5.15
J5	JUNCTION	2.13	4.32	195.82	0 12:16	4.30
J6	JUNCTION	2.20	4.28	195.52	0 12:04	4.27
J7	JUNCTION	2.68	5.02	196.37	0 11:44	5.02
J8	JUNCTION	0.42	3.50	197.89	0 12:05	3.06
Out1	OUTFALL	2.12	4.10	195.27	0 12:04	4.09

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.25	JUNCTION	8.32	8.32	0 12:05	0.25	
J2	0.25	JUNCTION	0.00	8.19	0 12:05	0	
J3	34.4	JUNCTION	776.48	776.48	0 12:05	34.4	
J4	32.2	JUNCTION	180.25	341.37	0 12:00	5.26	
J5	31.6	JUNCTION	0.00	201.70	0 12:08	0	
J6	31.9	JUNCTION	3.87	207.02	0 12:04	0.0808	
J7	34.4	JUNCTION	2.04	519.52	0 12:13	0.0399	
J8	1.15	JUNCTION	47.35	47.35	0 12:00	1.15	
Out1	31.9	OUTFALL	0.00	207.02	0 12:04	0	

Node Surge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	1.17	0.698	0.000

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*****
Node Flooding Summary
*****
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Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J1	1.15	5.09	0 12:00	0.014	0.198
J2	0.54	5.50	0 12:05	0.036	0.000
J3	1.67	370.31	0 12:00	2.249	5.779
J4	1.18	173.80	0 12:00	1.766	0.000
J7	1.61	358.41	0 12:13	7.435	0.000
J8	0.37	14.97	0 12:00	0.045	1.002

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	69.85	207.02	31.896
System	99.94	69.85	207.02	31.896

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	8.19	0	12:05	2.61	0.28	1.00
C3	CONDUIT	519.14	0	12:13	26.44	0.91	1.00
C4	CONDUIT	190.96	0	13:20	10.20	0.77	0.92
C5	CONDUIT	201.72	0	12:08	11.34	1.22	0.85
C6	CONDUIT	207.02	0	12:04	11.79	1.88	0.84
C2	CONDUIT	2.86	0	12:15	4.13	0.87	1.00
C7	CONDUIT	173.09	0	13:20	8.82	1.15	1.00
C8	CONDUIT	36.47	0	12:05	11.61	0.86	1.00

	Adjusted	----- Fraction of Time in Flow Class -----								
	/Actual	Up		Down	Sub	Sup	Up	Down	Norm	Inlet
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl

247	C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.89	0.00
248	C3	1.00	0.00	0.01	0.00	0.98	0.00	0.00	0.00	0.00	0.00
249	C4	1.00	0.00	0.02	0.00	0.94	0.00	0.04	0.00	0.00	0.00
250	C5	1.00	0.00	0.00	0.00	0.19	0.75	0.00	0.06	0.00	0.00
251	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
252	C2	1.00	0.07	0.00	0.00	0.92	0.00	0.00	0.01	0.81	0.00
253	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
254	C8	1.00	0.01	0.00	0.00	0.97	0.01	0.00	0.02	0.88	0.00

257 *****
258 Conduit Surcharge Summary
259 *****

Conduit	----- Hours Full -----			Hours	Hours	
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited	

C1	1.17	1.17	1.49	0.01	0.01	
C3	1.61	1.61	3.26	0.01	0.01	
C4	0.01	0.01	1.70	0.01	0.01	
C5	0.01	0.01	0.01	1.80	0.01	
C6	0.01	0.01	0.01	2.88	0.01	
C2	2.08	2.08	15.70	0.01	0.01	
C7	1.19	1.64	1.19	1.71	1.19	
C8	0.41	0.41	6.14	0.01	0.01	

276 Analysis begun on: Wed Nov 30 11:14:17 2022
277 Analysis ended on: Wed Nov 30 11:14:17 2022
278 Total elapsed time: < 1 sec

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

Volume

Depth

acre-feet

inches

Total Precipitation

180.660

8.710

Evaporation Loss

0.000

0.000

Infiltration Loss

22.022

1.062

Surface Runoff

149.464

7.206

Final Storage

9.462

0.456

Continuity Error (%)

-0.160

Flow Routing Continuity

Volume

Volume

acre-feet

10^6 gal

Dry Weather Inflow

0.000

0.000

Wet Weather Inflow

149.362

48.672

Groundwater Inflow

0.000

0.000

RDII Inflow

0.000

0.000

External Inflow

0.000

0.000

External Outflow

109.977

35.838

Flooding Loss

39.349

12.822

Evaporation Loss

0.000

0.000

Exfiltration Loss

0.000

0.000

Initial Stored Volume

0.000

0.000

Final Stored Volume

0.038

0.012

Continuity Error (%)

-0.002

Time-Step Critical Elements

Link C3 (85.29%)

70 Link C7 (7.21%)
71 Link C6 (6.90%)
72
73
74 *****
75 Highest Flow Instability Indexes
76 *****
77 Link C7 (1)
78 Link C4 (1)
79 Link C5 (1)

80
81
82 *****
83 Most Frequent Nonconverging Nodes
84 *****
85 Node Out1 (0.01%)
86 Node J2 (0.01%)
87 Node J3 (0.00%)
88 Node J1 (0.00%)
89

90
91 *****
92 Routing Time Step Summary
93 *****
94 Minimum Time Step : 0.50 sec
95 Average Time Step : 1.74 sec
96 Maximum Time Step : 20.00 sec
97 % of Time in Steady State : 0.00
98 Average Iterations per Step : 2.00
99 % of Steps Not Converging : 0.01
100 Time Step Frequencies :
101 20.000 - 9.564 sec : 0.08 %
102 9.564 - 4.573 sec : 0.75 %
103 4.573 - 2.187 sec : 20.27 %
104 2.187 - 1.046 sec : 64.77 %
105 1.046 - 0.500 sec : 14.12 %

106
107
108 *****
109 Subcatchment Runoff Summary
110 *****
111
112

		Total	Total	Total	Total	Imperv	
		Perv	Total	Total	Peak	Runoff	
		Precip	Runon	Evap	Infil	Runoff	
		Runoff	Runoff	Runoff	Runoff	Coeff	
Subcatchment		in	in	in	in		in
in	in	10^6 gal	CFS				

117	S1	8.71	0.00	0.00	2.33	0.37	
	5.82	6.20	0.30	10.47	0.712		
118	S5	8.71	0.00	0.00	1.14	4.22	
	3.23	7.45	1.36	56.90	0.855		
119	S3	8.71	0.00	0.00	1.11	3.90	
	3.21	7.11	40.74	941.46	0.816		
120	S6	8.71	0.00	0.00	0.02	8.14	
	0.49	8.62	0.09	4.53	0.990		
121	S4	8.71	0.00	0.00	0.64	5.32	
	2.56	7.88	6.16	217.11	0.905		
122	S7	8.71	0.00	0.00	0.13	7.26	
	1.28	8.53	0.05	2.38	0.980		

123
124
125 *****

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.42	2.73	197.24	0 12:05	2.70
J2	JUNCTION	1.09	3.50	197.14	0 11:57	3.50
J3	JUNCTION	4.63	14.72	204.91	0 12:13	14.69
J4	JUNCTION	3.08	5.15	196.22	0 11:41	5.15
J5	JUNCTION	2.27	4.33	195.83	0 12:05	4.32
J6	JUNCTION	2.33	4.29	195.53	0 12:04	4.29
J7	JUNCTION	2.84	5.02	196.37	0 11:41	5.02
J8	JUNCTION	0.47	4.15	198.54	0 12:06	3.46
Out1	OUTFALL	2.25	4.11	195.28	0 12:05	4.10

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.303	JUNCTION	10.47	10.47	0 12:05	0.303	
J2	0.303	JUNCTION	0.00	10.13	0 12:06	0	
J3	40.7	JUNCTION	941.46	941.46	0 12:05	40.7	
J4	36.4	JUNCTION	217.11	378.23	0 12:00	6.16	
J5	35.5	JUNCTION	0.00	203.00	0 12:08	0	
J6	35.8	JUNCTION	4.53	208.54	0 12:05	0.0936	
J7	40.8	JUNCTION	2.38	599.62	0 12:13	0.0463	
J8	1.35	JUNCTION	56.90	56.90	0 12:00	1.35	
Out1	35.8	OUTFALL	0.00	208.54	0 12:05	0	

Node Surge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	1.31	0.733	0.000
J2	JUNCTION	1.70	1.460	0.000

178	J3	JUNCTION	3.96	9.719	0.000
179	J4	JUNCTION	1.37	0.000	0.000
180	J7	JUNCTION	1.96	0.000	0.000
181	J8	JUNCTION	0.50	2.147	0.000

182
183

184 *****
185 Node Flooding Summary
186 *****

187

188 Flooding refers to all water that overflows a node, whether it ponds or not.

189

		Maximum	Time of Max	Total	Maximum
	Hours	Rate	Occurrence	Flood	Ponded
Node	Flooded	CFS	days hr:min	Volume 10^6 gal	Depth Feet
J1	1.29	5.56	0 11:58	0.016	0.233
J2	0.66	7.45	0 12:06	0.059	0.000
J3	2.03	482.10	0 12:00	3.078	7.909
J4	1.37	213.67	0 12:00	2.287	0.000
J7	1.96	438.51	0 12:13	10.476	0.000
J8	0.47	20.87	0 12:00	0.073	1.647

201

202

203 *****
204 Outfall Loading Summary
205 *****

206

	Flow	Avg	Max	Total
Outfall Node	Freq Pcnt	Flow CFS	Flow CFS	Volume 10^6 gal
Out1	99.92	76.99	208.54	35.835
System	99.92	76.99	208.54	35.835

215

216

217

218 *****
219 Link Flow Summary
220 *****

221

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	10.13	0 12:06	3.23	0.35	1.00
C3	CONDUIT	599.23	0 12:13	30.52	1.05	1.00
C4	CONDUIT	191.03	0 13:38	10.21	0.77	0.92
C5	CONDUIT	203.01	0 12:08	11.38	1.23	0.86
C6	CONDUIT	208.54	0 12:05	11.84	1.89	0.84
C2	CONDUIT	2.86	0 12:19	4.13	0.87	1.00
C7	CONDUIT	174.39	0 13:38	8.89	1.16	1.00
C8	CONDUIT	41.59	0 12:06	13.24	0.98	1.00

235

236

237 *****
238 Flow Classification Summary
239 *****

240

Conduit	Adjusted /Actual Length	----- Up Dry	Down Dry	Fraction of Time in Flow Class	Time Up Crit	Sub Sup Crit	Time Down Crit	Flow Class	Norm Ltd	Inlet Ctrl
C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.88	0.00

246

247	C3	1.00	0.00	0.01	0.00	0.98	0.00	0.00	0.00	0.00	0.00
248	C4	1.00	0.00	0.01	0.00	0.95	0.00	0.03	0.00	0.00	0.00
249	C5	1.00	0.00	0.00	0.00	0.22	0.72	0.00	0.05	0.00	0.00
250	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
251	C2	1.00	0.06	0.00	0.00	0.93	0.00	0.00	0.00	0.80	0.00
252	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
253	C8	1.00	0.00	0.00	0.00	0.97	0.01	0.00	0.02	0.86	0.00

254

255

256 *****

257 Conduit Surcharge Summary

258 *****

259

260

261

		-----	Hours Full	-----	Hours	Hours
		Both Ends	Upstream	Dnstream	Above Full	Capacity
Conduit					Normal Flow	Limited

264

C1	1.31	1.31	1.70	0.01	0.01
----	------	------	------	------	------

C3	1.96	1.96	3.96	0.26	0.01
----	------	------	------	------	------

C4	0.01	0.01	2.05	0.01	0.01
----	------	------	------	------	------

C5	0.01	0.01	0.01	2.17	0.01
----	------	------	------	------	------

C6	0.01	0.01	0.01	3.48	0.01
----	------	------	------	------	------

C2	2.48	2.48	16.85	0.01	0.01
----	------	------	-------	------	------

C7	1.38	1.98	1.38	2.12	1.38
----	------	------	------	------	------

C8	0.50	0.50	7.20	0.01	0.01
----	------	------	------	------	------

273

274

275 Analysis begun on: Wed Nov 30 11:14:43 2022

276 Analysis ended on: Wed Nov 30 11:14:43 2022

277 Total elapsed time: < 1 sec

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year (2050) - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	207.271	9.993
Evaporation Loss	0.000	0.000
Infiltration Loss	22.701	1.094
Surface Runoff	174.879	8.431
Final Storage	10.032	0.484
Continuity Error (%)	-0.164	

Flow Routing Continuity

	Volume acre-feet	Volume 10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	174.766	56.950
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	122.122	39.795
Flooding Loss	52.605	17.142
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.041	0.013
Continuity Error (%)	-0.001	

Time-Step Critical Elements

Link C3 (83.38%)

70 Link C7 (8.53%)
 71 Link C6 (7.59%)
 72
 73
 74 *****
 75 Highest Flow Instability Indexes
 76 *****
 77 Link C4 (2)
 78 Link C7 (2)
 79 Link C5 (1)
 80 Link C8 (1)
 81
 82
 83 *****
 84 Most Frequent Nonconverging Nodes
 85 *****
 86 Node Out1 (0.01%)
 87 Node J2 (0.01%)
 88 Node J3 (0.00%)
 89 Node J1 (0.00%)
 90 Node J8 (0.00%)
 91
 92

93 *****
 94 Routing Time Step Summary
 95 *****
 96 Minimum Time Step : 0.50 sec
 97 Average Time Step : 1.66 sec
 98 Maximum Time Step : 20.00 sec
 99 % of Time in Steady State : 0.00
 100 Average Iterations per Step : 2.00
 101 % of Steps Not Converging : 0.01
 102 Time Step Frequencies :
 103 20.000 - 9.564 sec : 0.07 %
 104 9.564 - 4.573 sec : 0.63 %
 105 4.573 - 2.187 sec : 16.99 %
 106 2.187 - 1.046 sec : 65.85 %
 107 1.046 - 0.500 sec : 16.46 %
 108
 109

110 *****
 111 Subcatchment Runoff Summary
 112 *****
 113
 114

Subcatchment		Total Perv Precip Runoff in	Total Runon Runoff in	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
in	in	10^6 gal	CFS			
S1		9.99	0.00	0.00	2.42	0.43
6.96	7.39	0.36	12.89	0.739		
S5		9.99	0.00	0.00	1.17	4.85
3.84	8.69	1.58	67.61	0.870		
S3		9.99	0.00	0.00	1.14	4.49
3.84	8.33	47.73	1128.20	0.834		
S6		9.99	0.00	0.00	0.02	9.34
0.56	9.91	0.11	5.26	0.991		
S4		9.99	0.00	0.00	0.66	6.11
3.03	9.14	7.15	258.55	0.915		
S7		9.99	0.00	0.00	0.13	8.33
1.48	9.82	0.05	2.74	0.982		

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.45	2.78	197.29	0 12:05	2.74
J2	JUNCTION	1.13	3.50	197.14	0 11:55	3.50
J3	JUNCTION	4.93	17.32	207.51	0 12:14	17.31
J4	JUNCTION	3.21	5.15	196.22	0 11:40	5.15
J5	JUNCTION	2.40	4.35	195.85	0 12:05	4.33
J6	JUNCTION	2.46	4.31	195.55	0 12:04	4.30
J7	JUNCTION	2.98	5.02	196.37	0 11:40	5.02
J8	JUNCTION	0.52	4.93	199.32	0 12:06	3.96
Out1	OUTFALL	2.38	4.12	195.29	0 12:05	4.11

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.361	JUNCTION	12.89	12.89	0 12:05	0.361	
J2	0.361	JUNCTION	0.00	12.32	0 12:06	0	
J3	47.7	JUNCTION	1128.20	1128.20	0 12:05	47.7	
J4	40.7	JUNCTION	258.55	419.67	0 12:00	7.14	
J5	39.4	JUNCTION	0.00	204.41	0 12:09	0	
J6	39.8	JUNCTION	5.26	210.17	0 12:05	0.108	
J7	47.8	JUNCTION	2.74	684.71	0 12:14	0.0533	
J8	1.58	JUNCTION	67.61	67.61	0 12:00	1.58	
Out1	39.8	OUTFALL	0.00	210.17	0 12:05	0	

Node Surge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
------	------	---------------------	------------------------------------	---------------------------------

178	J1	JUNCTION	1.45	0.782	0.000
179	J2	JUNCTION	1.91	1.460	0.000
180	J3	JUNCTION	4.64	12.316	0.000
181	J4	JUNCTION	1.56	0.000	0.000
182	J7	JUNCTION	2.29	0.000	0.000
183	J8	JUNCTION	0.60	2.930	0.000

184

185

186 *****

187 Node Flooding Summary

188 *****

189

190 Flooding refers to all water that overflows a node, whether it ponds or not.

191 -----

	Hours	Maximum	Time of Max	Total	Maximum
	Flooded	Rate	Occurrence	Flood	Ponded
Node		CFS	days hr:min	Volume	Depth
				10^6 gal	Feet
196	-----				
197	J1	1.42	5.69	0 11:56	0.020
198	J2	0.76	9.65	0 12:06	0.087
199	J3	2.38	614.28	0 12:00	4.088
200	J4	1.55	258.44	0 12:00	2.878
201	J7	2.29	523.59	0 12:14	14.177
202	J8	0.55	27.51	0 12:00	0.108
203					2.430

204

205 *****

206 Outfall Loading Summary

207 *****

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CFS	CFS	10^6 gal
213	-----			
214	Out1	99.93	83.84	210.17
215				39.792
216	System	99.93	83.84	210.17
217				39.792

218

219

220 *****

221 Link Flow Summary

222 *****

		Maximum	Time of Max	Maximum	Max/	Max/
		Flow	Occurrence	Veloc	Full	Full
Link	Type	CFS	days hr:min	ft/sec	Flow	Depth
228	-----					
229	C1	CONDUIT	12.32	0 12:06	3.92	0.43
230	C3	CONDUIT	684.30	0 12:14	34.85	1.20
231	C4	CONDUIT	191.04	0 13:56	10.21	0.77
232	C5	CONDUIT	204.43	0 12:09	11.41	1.23
233	C6	CONDUIT	210.17	0 12:05	11.90	1.91
234	C2	CONDUIT	2.86	0 12:23	4.13	0.87
235	C7	CONDUIT	175.31	0 13:57	8.93	1.17
236	C8	CONDUIT	47.08	0 12:06	14.99	1.11
237						1.00

238

239 *****

240 Flow Classification Summary

241 *****

	Adjusted	Fraction of Time in Flow Class							
	/Actual	Up	Down	Sub	Sup	Up	Down	Norm	Inlet
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd Ctrl
246	-----								

247											
248	C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.85	0.00
249	C3	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.00	0.00
250	C4	1.00	0.00	0.01	0.00	0.95	0.00	0.03	0.00	0.00	0.00
251	C5	1.00	0.00	0.00	0.00	0.26	0.69	0.00	0.04	0.00	0.00
252	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
253	C2	1.00	0.05	0.00	0.00	0.94	0.00	0.00	0.00	0.78	0.00
254	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
255	C8	1.00	0.00	0.00	0.00	0.97	0.01	0.00	0.02	0.84	0.00

256

257

258 *****

259 Conduit Surcharge Summary

260 *****

261

262						
263						
264		-----	Hours Full	-----	Hours	Hours
265	Conduit	Both Ends	Upstream	Dnstream	Above Full	Capacity
266					Normal Flow	Limited
267	C1	1.45	1.45	1.91	0.01	0.01
268	C3	2.29	2.29	4.64	0.55	0.01
269	C4	0.01	0.01	2.41	0.01	0.01
270	C5	0.01	0.01	0.01	2.56	0.01
271	C6	0.01	0.01	0.01	4.15	0.01
272	C2	2.91	2.91	17.76	0.01	0.01
273	C7	1.57	2.32	1.57	2.49	1.57
274	C8	0.60	0.60	8.32	0.19	0.19

275

276

277 Analysis begun on: Wed Nov 30 11:15:09 2022

278 Analysis ended on: Wed Nov 30 11:15:10 2022

279 Total elapsed time: 00:00:01

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year (2100) - EXISTING)

WARNING 02: maximum depth increased for Node J4
 WARNING 02: maximum depth increased for Node J5
 WARNING 02: maximum depth increased for Node J6
 WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	207.271	9.993
Evaporation Loss	0.000	0.000
Infiltration Loss	22.701	1.094
Surface Runoff	174.879	8.431
Final Storage	10.032	0.484
Continuity Error (%)	-0.164	

Flow Routing Continuity

	Volume acre-feet	Volume 10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	174.766	56.950
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	122.122	39.795
Flooding Loss	52.605	17.142
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.041	0.013
Continuity Error (%)	-0.001	

Time-Step Critical Elements

Link C3 (83.38%)

70 Link C7 (8.53%)
 71 Link C6 (7.59%)
 72
 73
 74 *****
 75 Highest Flow Instability Indexes
 76 *****
 77 Link C4 (2)
 78 Link C7 (2)
 79 Link C5 (1)
 80 Link C8 (1)
 81
 82
 83 *****
 84 Most Frequent Nonconverging Nodes
 85 *****
 86 Node Out1 (0.01%)
 87 Node J2 (0.01%)
 88 Node J3 (0.00%)
 89 Node J1 (0.00%)
 90 Node J8 (0.00%)
 91
 92

93 *****
 94 Routing Time Step Summary
 95 *****
 96 Minimum Time Step : 0.50 sec
 97 Average Time Step : 1.66 sec
 98 Maximum Time Step : 20.00 sec
 99 % of Time in Steady State : 0.00
 100 Average Iterations per Step : 2.00
 101 % of Steps Not Converging : 0.01
 102 Time Step Frequencies :
 103 20.000 - 9.564 sec : 0.07 %
 104 9.564 - 4.573 sec : 0.63 %
 105 4.573 - 2.187 sec : 16.99 %
 106 2.187 - 1.046 sec : 65.85 %
 107 1.046 - 0.500 sec : 16.46 %
 108
 109

110 *****
 111 Subcatchment Runoff Summary
 112 *****
 113
 114

			Total Perv Precip Runoff	Total Total Runon Runoff	Total Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
Subcatchment in	in	10^6 gal	in CFS	in	in	in	in

119	S1		9.99	0.00	0.00	2.42	0.43
	6.96	7.39	0.36 12.89	0.739			
120	S5		9.99	0.00	0.00	1.17	4.85
	3.84	8.69	1.58 67.61	0.870			
121	S3		9.99	0.00	0.00	1.14	4.49
	3.84	8.33	47.73 1128.20	0.834			
122	S6		9.99	0.00	0.00	0.02	9.34
	0.56	9.91	0.11 5.26	0.991			
123	S4		9.99	0.00	0.00	0.66	6.11
	3.03	9.14	7.15 258.55	0.915			
124	S7		9.99	0.00	0.00	0.13	8.33
	1.48	9.82	0.05 2.74	0.982			

125

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.45	2.78	197.29	0 12:05	2.74
J2	JUNCTION	1.13	3.50	197.14	0 11:55	3.50
J3	JUNCTION	4.93	17.32	207.51	0 12:14	17.31
J4	JUNCTION	3.21	5.15	196.22	0 11:40	5.15
J5	JUNCTION	2.40	4.35	195.85	0 12:05	4.33
J6	JUNCTION	2.46	4.31	195.55	0 12:04	4.30
J7	JUNCTION	2.98	5.02	196.37	0 11:40	5.02
J8	JUNCTION	0.52	4.93	199.32	0 12:06	3.96
Out1	OUTFALL	2.38	4.12	195.29	0 12:05	4.11

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.361	JUNCTION	12.89	12.89	0 12:05	0.361	
J2	0.361	JUNCTION	0.00	12.32	0 12:06	0	
J3	47.7	JUNCTION	1128.20	1128.20	0 12:05	47.7	
J4	40.7	JUNCTION	258.55	419.67	0 12:00	7.14	
J5	39.4	JUNCTION	0.00	204.41	0 12:09	0	
J6	39.8	JUNCTION	5.26	210.17	0 12:05	0.108	
J7	47.8	JUNCTION	2.74	684.71	0 12:14	0.0533	
J8	1.58	JUNCTION	67.61	67.61	0 12:00	1.58	
Out1	39.8	OUTFALL	0.00	210.17	0 12:05	0	

Node Surge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
------	------	---------------------	------------------------------------	---------------------------------

178	J1	JUNCTION	1.45	0.782	0.000
179	J2	JUNCTION	1.91	1.460	0.000
180	J3	JUNCTION	4.64	12.316	0.000
181	J4	JUNCTION	1.56	0.000	0.000
182	J7	JUNCTION	2.29	0.000	0.000
183	J8	JUNCTION	0.60	2.930	0.000

184

185

186 *****

187 Node Flooding Summary

188 *****

189

190 Flooding refers to all water that overflows a node, whether it ponds or not.

191 -----

	Hours	Maximum	Time of Max	Total	Maximum
	Flooded	Rate	Occurrence	Flood	Ponded
Node		CFS	days hr:min	Volume	Depth
				10^6 gal	Feet
196	-----				
197	J1	1.42	5.69	0 11:56	0.020 0.282
198	J2	0.76	9.65	0 12:06	0.087 0.000
199	J3	2.38	614.28	0 12:00	4.088 10.506
200	J4	1.55	258.44	0 12:00	2.878 0.000
201	J7	2.29	523.59	0 12:14	14.177 0.000
202	J8	0.55	27.51	0 12:00	0.108 2.430

203

204

205 *****

206 Outfall Loading Summary

207 *****

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CFS	CFS	10^6 gal
213	-----			
214	Out1	99.93	83.84	210.17 39.792
215	-----			
216	System	99.93	83.84	210.17 39.792

217

218

219

220 *****

221 Link Flow Summary

222 *****

		Maximum	Time of Max	Maximum	Max/	Max/
		Flow	Occurrence	Veloc	Full	Full
Link	Type	CFS	days hr:min	ft/sec	Flow	Depth
228	-----					
229	C1	CONDUIT	12.32	0 12:06	3.92	0.43 1.00
230	C3	CONDUIT	684.30	0 12:14	34.85	1.20 1.00
231	C4	CONDUIT	191.04	0 13:56	10.21	0.77 0.92
232	C5	CONDUIT	204.43	0 12:09	11.41	1.23 0.86
233	C6	CONDUIT	210.17	0 12:05	11.90	1.91 0.84
234	C2	CONDUIT	2.86	0 12:23	4.13	0.87 1.00
235	C7	CONDUIT	175.31	0 13:57	8.93	1.17 1.00
236	C8	CONDUIT	47.08	0 12:06	14.99	1.11 1.00

237

238

239 *****

240 Flow Classification Summary

241 *****

	Adjusted	Fraction of Time in Flow Class							
	/Actual	Up	Down	Sub	Sup	Up	Down	Norm	Inlet
Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd Ctrl
246	-----								

247											
248	C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.85	0.00
249	C3	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.00	0.00
250	C4	1.00	0.00	0.01	0.00	0.95	0.00	0.03	0.00	0.00	0.00
251	C5	1.00	0.00	0.00	0.00	0.26	0.69	0.00	0.04	0.00	0.00
252	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
253	C2	1.00	0.05	0.00	0.00	0.94	0.00	0.00	0.00	0.78	0.00
254	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
255	C8	1.00	0.00	0.00	0.00	0.97	0.01	0.00	0.02	0.84	0.00

256
257
258 *****
259 Conduit Surcharge Summary
260 *****
261

262						
263					Hours	Hours
264		-----	Hours Full	-----	Above Full	Capacity
265	Conduit	Both Ends	Upstream	Dnstream	Normal Flow	Limited
266						
267	C1	1.45	1.45	1.91	0.01	0.01
268	C3	2.29	2.29	4.64	0.55	0.01
269	C4	0.01	0.01	2.41	0.01	0.01
270	C5	0.01	0.01	0.01	2.56	0.01
271	C6	0.01	0.01	0.01	4.15	0.01
272	C2	2.91	2.91	17.76	0.01	0.01
273	C7	1.57	2.32	1.57	2.49	1.57
274	C8	0.60	0.60	8.32	0.19	0.19

275
276
277 Analysis begun on: Wed Nov 30 11:15:09 2022
278 Analysis ended on: Wed Nov 30 11:15:10 2022
279 Total elapsed time: 00:00:01

WARNING 02: maximum depth increased for Node J4
WARNING 02: maximum depth increased for Node J5
WARNING 02: maximum depth increased for Node J6
WARNING 02: maximum depth increased for Node J7

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	218.596	10.539
Evaporation Loss	0.000	0.000
Infiltration Loss	22.949	1.106
Surface Runoff	185.655	8.951
Final Storage	10.356	0.499
Continuity Error (%)	-0.166	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	185.535	60.459
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	127.238	41.462
Flooding Loss	58.258	18.984
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.042	0.014
Continuity Error (%)	-0.002	

Time-Step Critical Elements

Link C3 (82.75%)

70 Link C7 (8.96%)
 71 Link C6 (7.81%)
 72
 73
 74 *****
 75 Highest Flow Instability Indexes
 76 *****
 77 Link C4 (2)
 78 Link C7 (2)
 79 Link C5 (1)
 80 Link C8 (1)
 81 Link C6 (1)
 82
 83

84 *****
 85 Most Frequent Nonconverging Nodes
 86 *****
 87 Node Out1 (0.05%)
 88 Node J2 (0.04%)
 89 Node J1 (0.00%)
 90 Node J8 (0.00%)
 91 Node J3 (0.00%)
 92
 93

94 *****
 95 Routing Time Step Summary
 96 *****
 97 Minimum Time Step : 0.50 sec
 98 Average Time Step : 1.63 sec
 99 Maximum Time Step : 20.00 sec
 100 % of Time in Steady State : 0.00
 101 Average Iterations per Step : 2.01
 102 % of Steps Not Converging : 0.05
 103 Time Step Frequencies :
 104 20.000 - 9.564 sec : 0.06 %
 105 9.564 - 4.573 sec : 0.56 %
 106 4.573 - 2.187 sec : 15.78 %
 107 2.187 - 1.046 sec : 66.11 %
 108 1.046 - 0.500 sec : 17.49 %
 109
 110

111 *****
 112 Subcatchment Runoff Summary
 113 *****
 114
 115

Subcatchment	in	in	10^6 gal	CFS	Total Perv Precip Runoff	Total Runon Runoff	Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
S1	7.44	7.90	0.39	13.88	0.00	0.00	0.00	2.45	0.45
S5	4.11	9.22	1.68	72.01	0.00	0.00	0.00	1.19	5.11
S3	4.11	8.85	50.69	1205.48	0.00	0.00	0.00	1.16	4.74
S6	0.59	10.45	0.11	5.56	0.00	0.00	0.00	0.02	9.86
S4	3.23	9.68	7.57	275.58	0.00	0.00	0.00	0.67	6.45
S7	1.57	10.36	0.06	2.89	0.00	0.00	0.00	0.13	8.79

120 S1 10.54 0.00 0.00 2.45 0.45
 7.44 7.90 0.39 13.88 0.749
 121 S5 10.54 0.00 0.00 1.19 5.11
 4.11 9.22 1.68 72.01 0.875
 122 S3 10.54 0.00 0.00 1.16 4.74
 4.11 8.85 50.69 1205.48 0.840
 123 S6 10.54 0.00 0.00 0.02 9.86
 0.59 10.45 0.11 5.56 0.992
 124 S4 10.54 0.00 0.00 0.67 6.45
 3.23 9.68 7.57 275.58 0.918
 125 S7 10.54 0.00 0.00 0.13 8.79
 1.57 10.36 0.06 2.89 0.983

Node Depth Summary

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	0.46	2.80	197.31	0 12:05	2.75
J2	JUNCTION	1.14	3.50	197.14	0 11:38	3.50
J3	JUNCTION	5.05	18.44	208.63	0 12:14	18.44
J4	JUNCTION	3.27	5.15	196.22	0 11:39	5.15
J5	JUNCTION	2.45	4.36	195.86	0 12:05	4.34
J6	JUNCTION	2.51	4.32	195.56	0 12:05	4.31
J7	JUNCTION	3.03	5.02	196.37	0 11:39	5.02
J8	JUNCTION	0.54	5.27	199.66	0 12:06	4.18
Out1	OUTFALL	2.43	4.13	195.30	0 12:05	4.12

Node Inflow Summary

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1	0.386	JUNCTION	13.88	13.88	0 12:05	0.386	
J2	0.386	JUNCTION	0.00	13.21	0 12:06	0	
J3	50.7	JUNCTION	1205.48	1205.48	0 12:05	50.7	
J4	42.5	JUNCTION	275.58	436.69	0 12:00	7.56	
J5	41.1	JUNCTION	0.00	204.98	0 12:09	0	
J6	41.5	JUNCTION	5.56	210.82	0 12:05	0.113	
J7	50.7	JUNCTION	2.89	718.39	0 12:14	0.0563	
J8	1.68	JUNCTION	72.01	72.01	0 12:00	1.68	
Out1	41.5	OUTFALL	0.00	210.82	0 12:05	0	

Node Surge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
------	------	---------------------	------------------------------------	---------------------------------

178					
179	J1	JUNCTION	1.50	0.805	0.000
180	J2	JUNCTION	2.00	1.460	0.000
181	J3	JUNCTION	4.88	13.439	0.000
182	J4	JUNCTION	1.64	0.000	0.000
183	J7	JUNCTION	2.42	0.000	0.000
184	J8	JUNCTION	0.63	3.266	0.000

185
186
187 *****
188 Node Flooding Summary
189 *****

190
191 Flooding refers to all water that overflows a node, whether it ponds or not.

192						
193					Total	Maximum
194			Maximum	Time of Max	Flood	Ponded
195		Hours	Rate	Occurrence	Volume	Depth
196	Node	Flooded	CFS	days hr:min	10^6 gal	Feet
197						
198	J1	1.47	5.64	0 11:55	0.021	0.305
199	J2	0.81	10.54	0 12:06	0.098	0.000
200	J3	2.51	670.66	0 12:00	4.526	11.629
201	J4	1.63	276.80	0 12:00	3.123	0.000
202	J7	2.42	557.27	0 12:14	15.762	0.000
203	J8	0.58	30.30	0 12:00	0.123	2.766

204
205
206 *****
207 Outfall Loading Summary
208 *****

209					
210					
211		Flow	Avg	Max	Total
212		Freq	Flow	Flow	Volume
213	Outfall Node	Pcnt	CFS	CFS	10^6 gal
214					
215	Out1	99.94	86.53	210.82	41.459
216					
217	System	99.94	86.53	210.82	41.459

218
219
220
221 *****
222 Link Flow Summary
223 *****

224							
225							
226			Maximum	Time of Max	Maximum	Max/	Max/
227			Flow	Occurrence	Veloc	Full	Full
228	Link	Type	CFS	days hr:min	ft/sec	Flow	Depth
229							
230	C1	CONDUIT	13.21	0 12:06	4.20	0.46	1.00
231	C3	CONDUIT	717.98	0 12:14	36.57	1.26	1.00
232	C4	CONDUIT	191.04	0 14:03	10.21	0.77	0.93
233	C5	CONDUIT	205.00	0 12:09	11.43	1.24	0.86
234	C6	CONDUIT	210.82	0 12:05	11.92	1.92	0.84
235	C2	CONDUIT	2.86	0 12:25	4.13	0.87	1.00
236	C7	CONDUIT	175.53	0 14:04	8.95	1.17	1.00
237	C8	CONDUIT	49.26	0 12:06	15.68	1.16	1.00

238
239
240 *****
241 Flow Classification Summary
242 *****

243									
244									
245		Adjusted		Fraction of Time in Flow Class					
246		/Actual	Up	Down Sub Sup Up	Down Norm Inlet				

	Conduit	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
247											
248											
249	C1	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.85	0.00
250	C3	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.00	0.00
251	C4	1.00	0.00	0.01	0.00	0.96	0.00	0.03	0.00	0.00	0.00
252	C5	1.00	0.00	0.00	0.00	0.27	0.68	0.00	0.04	0.00	0.00
253	C6	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.00	0.00
254	C2	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.77	0.00
255	C7	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
256	C8	1.00	0.00	0.00	0.00	0.98	0.01	0.00	0.01	0.83	0.00

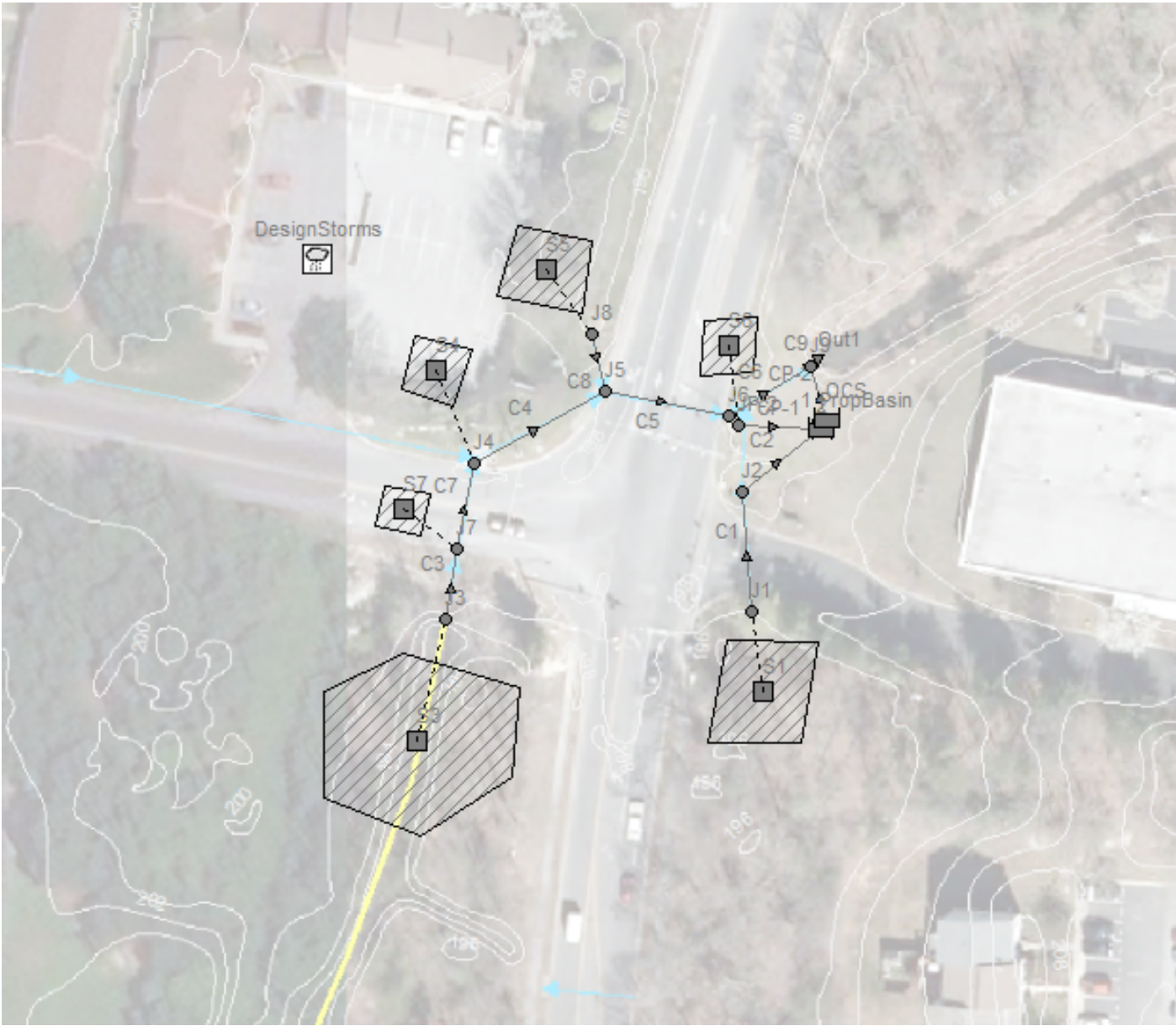
257
258
259 *****

260 Conduit Surcharge Summary
261 *****

262						
263		-----				
264					Hours	Hours
265		-----	Hours Full	-----	Above Full	Capacity
266	Conduit	Both Ends	Upstream	Dnstream	Normal Flow	Limited
267		-----				
268	C1	1.50	1.50	2.00	0.01	0.01
269	C3	2.42	2.42	4.88	0.64	0.01
270	C4	0.01	0.01	2.55	0.01	0.01
271	C5	0.01	0.01	0.01	2.72	0.01
272	C6	0.01	0.01	0.01	4.38	0.01
273	C2	3.12	3.12	18.20	0.01	0.01
274	C7	1.64	2.46	1.64	2.65	1.64
275	C8	0.63	0.63	8.81	0.23	0.23

276
277
278 Analysis begun on: Wed Nov 30 11:15:36 2022
279 Analysis ended on: Wed Nov 30 11:15:37 2022
280 Total elapsed time: 00:00:01

Location 12: Proposed Industrial Drive and Post Office Road SWMM Schematic



Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year - PROPOSED)

WARNING 03: negative offset ignored for Link C2
 WARNING 03: negative offset ignored for Link CP-1
 WARNING 04: minimum elevation drop used for Conduit C9
 WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	130.610	6.297
Evaporation Loss	0.000	0.000
Infiltration Loss	20.220	0.975
Surface Runoff	102.606	4.947
Final Storage	7.976	0.385
Continuity Error (%)	-0.147	

Flow Routing Continuity

	Volume acre-feet	Volume 10^6 gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	102.535	33.412
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	89.627	29.206
Flooding Loss	11.670	3.803
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.046	0.015
Continuity Error (%)	1.162	

Highest Continuity Errors

Node JP-2 (4.16%)

```

70 Node J9 (1.39%)
71
72
73 *****
74 Time-Step Critical Elements
75 *****
76 Link C9 (99.98%)
77
78
79 *****
80 Highest Flow Instability Indexes
81 *****
82 Link C9 (51)
83 Link C6 (45)
84 Link C3 (16)
85 Link C7 (13)
86 Link CP-2 (7)
87
88
89 *****
90 Most Frequent Nonconverging Nodes
91 *****
92 Node Out1 (8.32%)
93 Node J9 (8.16%)
94 Node J6 (0.21%)
95 Node J5 (0.14%)
96 Node J4 (0.11%)
97
98
99 *****
100 Routing Time Step Summary
101 *****
102 Minimum Time Step      :      0.17 sec
103 Average Time Step      :      0.50 sec
104 Maximum Time Step      :     20.00 sec
105 % of Time in Steady State :      0.00
106 Average Iterations per Step :      2.83
107 % of Steps Not Converging :      8.32
108 Time Step Frequencies  :
109     20.000 - 9.564 sec   :      0.01 %
110     9.564 - 4.573 sec   :      0.00 %
111     4.573 - 2.187 sec   :      0.00 %
112     2.187 - 1.046 sec   :      0.00 %
113     1.046 - 0.500 sec   :     99.98 %
114
115

```

```

116 *****
117 Subcatchment Runoff Summary
118 *****
119
120

```

Subcatchment		Total Perv Precip Runoff in 10 ⁶ gal	Total Runon Runoff in CFS	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
S1	3.77	4.04	6.30	0.00	2.10	0.27
S5	2.11	5.15	6.30	0.00	1.04	3.04
S3	2.05	4.86	6.30	0.00	1.02	2.81
S6			6.30	0.00	0.02	5.87

```

129      0.34      6.21      0.07      3.20      0.986
      S4              6.30      0.00      0.00      0.60      3.83
      1.70      5.54      4.33      144.08      0.879
130      S7              6.30      0.00      0.00      0.12      5.24
      0.89      6.13      0.03      1.70      0.973

```

```

131
132
133 *****
134 Node Depth Summary
135 *****

```

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	1.86	2.48	196.99	0 12:00	2.48
J2	JUNCTION	1.92	2.50	196.95	0 07:47	2.50
J3	JUNCTION	1.71	6.55	197.80	0 12:06	6.05
J4	JUNCTION	1.53	5.00	196.17	0 11:52	5.00
J5	JUNCTION	1.47	5.00	196.11	0 11:53	5.00
J6	JUNCTION	1.42	5.00	196.05	0 11:56	4.24
J7	JUNCTION	1.53	5.00	196.22	0 11:52	5.00
J8	JUNCTION	0.24	2.99	197.38	0 12:05	2.75
JP-2	JUNCTION	1.76	2.00	200.00	0 04:41	2.00
J9	JUNCTION	1.35	4.01	195.01	0 12:01	3.85
Out1	OUTFALL	1.31	3.75	194.75	0 11:50	3.75
PropBasin	STORAGE	0.00	0.00	200.00	0 00:00	0.00
OCS	STORAGE	0.48	3.31	195.31	0 12:36	2.96

```

155
156
157 *****
158 Node Inflow Summary
159 *****

```

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1		JUNCTION	6.24	6.24	0 12:05	0.197	
0.197	0.372						
J2		JUNCTION	0.00	6.25	0 12:05	0	
0.196	0.743						
J3		JUNCTION	616.53	616.53	0 12:05	27.8	
27.8	0.021						
J4		JUNCTION	144.08	339.66	0 12:13	4.33	
28.9	-0.008						
J5		JUNCTION	0.00	360.24	0 12:01	0	
29.7	-0.035						
J6		JUNCTION	0.00	367.68	0 12:01	0	
29.6	-0.014						
J7		JUNCTION	1.70	570.72	0 12:06	0.0332	
27.9	-0.013						
J8		JUNCTION	37.99	37.99	0 12:00	0.937	
0.937	-0.031						
JP-2		JUNCTION	3.20	3.20	0 12:00	0.0674	
0.0674	4.340						
J9		JUNCTION	0.00	389.03	0 12:02	0	
29.6	1.413						

```

177 Out1          0.00  430.05  0  12:01  0
178 29.2          0.000
178 PropBasin      STORAGE      0.00  0.00  0  00:00  0
178 0          0.000 gal
179 OCS            STORAGE      0.00  4.02  0  12:51  0
179 0.0193         0.053

```

```

182 *****
183 Node Surcharge Summary
184 *****

```

186 Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	16.24	0.482	0.018
J2	JUNCTION	16.26	0.500	0.000
J3	JUNCTION	0.91	1.716	0.000
J4	JUNCTION	0.51	0.167	0.000
J5	JUNCTION	0.15	0.167	0.000
J6	JUNCTION	0.01	0.167	0.000
J7	JUNCTION	0.64	0.167	0.000
J8	JUNCTION	0.32	0.994	0.000
JP-2	JUNCTION	19.30	0.000	0.000

```

203 *****
204 Node Flooding Summary
205 *****

```

207 Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J2	16.21	6.25	0 12:05	0.195	0.000
J3	0.47	111.15	0 12:00	0.346	0.799
J4	0.34	89.64	0 12:25	0.136	0.000
J5	0.10	110.44	0 12:12	0.073	0.000
J6	0.01	72.02	0 12:02	0.006	0.000
J7	0.62	397.94	0 12:05	3.327	0.000
J8	0.30	11.89	0 12:00	0.023	0.494
JP-2	19.30	3.20	0 12:00	0.065	0.000

```

224 *****
225 Storage Volume Summary
226 *****

```

Storage Unit hr:min	Average Max Volume	Avg Maximum Pcnt	Evap Pcnt	Exfil Pcnt	Maximum Volume	Max Pcnt	Time of days
PropBasin	0.000	0	0	0	0.000	0	0
00:00	0.00						
OCS	0.008	5	0	0	0.053	33	0

 Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.93	45.44	430.05	29.204
System	99.93	45.44	430.05	29.204

 Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	6.25	0 12:05	1.99	0.81	1.00
C3	CONDUIT	569.79	0 12:06	19.32	3.74	1.00
C4	CONDUIT	340.76	0 12:13	11.64	2.42	1.00
C5	CONDUIT	367.68	0 12:01	12.90	2.42	1.00
C6	CONDUIT	388.81	0 12:02	14.58	2.49	0.91
C2	CONDUIT	0.00	0 00:00	0.00	0.00	0.50
C7	CONDUIT	288.18	0 12:22	9.78	1.85	1.00
C8	CONDUIT	35.10	0 12:05	11.17	0.83	1.00
CP-1	CONDUIT	0.00	0 00:00	0.00	0.00	0.50
CP-2	CONDUIT	4.59	0 12:50	2.60	0.28	1.00
C9	CONDUIT	430.05	0 12:01	17.17	2.87	0.80
1	WEIR	0.00	0 00:00			0.00
2	WEIR	0.00	0 00:00			0.00

 Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.38
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.98	0.02	0.00	0.00	0.00	0.00
C2	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.03	0.00
C8	1.00	0.00	0.00	0.00	0.87	0.04	0.00	0.09	0.88	0.00
CP-1	1.00	0.00	0.19	0.00	0.80	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.35	0.00	0.64	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.34	0.65	0.00	0.00	0.40	0.00

 Conduit Surge Summary

		-----	Hours Full	-----	Hours	Hours
		Both Ends	Upstream	Dnstream	Above Full	Capacity
	Conduit				Normal Flow	Limited
307	C1	16.24	16.24	16.26	0.01	0.01
308	C3	0.63	0.91	0.64	1.25	0.63
309	C4	0.14	0.51	0.14	1.64	0.04
310	C5	0.01	0.14	0.01	1.52	0.01
311	C6	0.01	0.01	0.01	1.48	0.01
312	C7	0.51	0.64	0.51	1.20	0.17
313	C8	0.32	0.32	2.36	0.01	0.01
314	CP-1	0.01	0.01	19.30	0.01	0.01
315	CP-2	2.04	2.04	7.82	0.01	0.01
316	C9	0.01	0.01	0.01	1.54	0.01
317						
318						
319	Analysis begun on: Wed Nov 30 11:02:20 2022					
320	Analysis ended on: Wed Nov 30 11:02:22 2022					
321	Total elapsed time: 00:00:02					

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year (2050) - PROPOSED)

WARNING 03: negative offset ignored for Link C2
 WARNING 03: negative offset ignored for Link CP-1
 WARNING 04: minimum elevation drop used for Conduit C9
 WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

Total Precipitation 146.436 7.060

Evaporation Loss 0.000 0.000

Infiltration Loss 20.887 1.007

Surface Runoff 117.361 5.658

Final Storage 8.408 0.405

Continuity Error (%) -0.150

Flow Routing Continuity

Dry Weather Inflow 0.000 0.000

Wet Weather Inflow 117.283 38.218

Groundwater Inflow 0.000 0.000

RDII Inflow 0.000 0.000

External Inflow 0.000 0.000

External Outflow 99.793 32.519

Flooding Loss 16.171 5.270

Evaporation Loss 0.000 0.000

Exfiltration Loss 0.000 0.000

Initial Stored Volume 0.000 0.000

Final Stored Volume 0.048 0.016

Continuity Error (%) 1.084

Highest Continuity Errors

Node JP-2 (3.70%)

70 Node J9 (1.35%)
 71
 72
 73 *****
 74 Time-Step Critical Elements
 75 *****
 76 Link C9 (99.98%)
 77
 78
 79 *****
 80 Highest Flow Instability Indexes
 81 *****
 82 Link C9 (56)
 83 Link C6 (49)
 84 Link C3 (18)
 85 Link C7 (15)
 86 Link CP-2 (8)
 87
 88
 89 *****
 90 Most Frequent Nonconverging Nodes
 91 *****
 92 Node Out1 (9.67%)
 93 Node J9 (9.48%)
 94 Node J6 (0.24%)
 95 Node J5 (0.15%)
 96 Node J4 (0.11%)
 97
 98
 99 *****
 100 Routing Time Step Summary
 101 *****
 102 Minimum Time Step : 0.47 sec
 103 Average Time Step : 0.50 sec
 104 Maximum Time Step : 20.00 sec
 105 % of Time in Steady State : 0.00
 106 Average Iterations per Step : 2.95
 107 % of Steps Not Converging : 9.67
 108 Time Step Frequencies :
 109 20.000 - 9.564 sec : 0.01 %
 110 9.564 - 4.573 sec : 0.00 %
 111 4.573 - 2.187 sec : 0.00 %
 112 2.187 - 1.046 sec : 0.00 %
 113 1.046 - 0.500 sec : 99.98 %
 114
 115

116 *****
 117 Subcatchment Runoff Summary
 118 *****
 119
 120

Subcatchment		Total Perv Precip Runoff in 10^6 gal	Total Runon Runoff in CFS	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
125	S1	7.06	0.00	0.00	2.19	0.30
	4.41	4.71	0.23	7.54	0.667	
126	S5	7.06	0.00	0.00	1.07	3.42
	2.46	5.87	1.07	43.86	0.832	
127	S3	7.06	0.00	0.00	1.05	3.16
	2.41	5.57	31.92	716.83	0.789	
128	S6	7.06	0.00	0.00	0.02	6.59

```

129      0.39      6.97      0.08      3.63      0.988
      S4              7.06      0.00      0.00      0.62      4.30
      1.97      6.28      4.91      166.78      0.889
130      S7              7.06      0.00      0.00      0.13      5.88
      1.01      6.89      0.04      1.91      0.976
131
132
133
134
135
136
137

```

```

*****
Node Depth Summary
*****

```

```

-----
138                                     Average  Maximum  Maximum  Time of Max  Reported
139                                     Depth    Depth    HGL      Occurrence  Max Depth
140      Node                          Type      Feet      Feet      Feet      days hr:min  Feet
-----
141
142      J1                          JUNCTION  1.91      2.50      197.01      0  12:05      2.50
143      J2                          JUNCTION  1.96      2.50      196.95      0  07:12      2.50
144      J3                          JUNCTION  1.83      7.03      198.28      0  12:06      6.35
145      J4                          JUNCTION  1.62      5.00      196.17      0  11:49      5.00
146      J5                          JUNCTION  1.56      5.00      196.11      0  11:51      5.00
147      J6                          JUNCTION  1.50      5.00      196.05      0  11:52      4.41
148      J7                          JUNCTION  1.62      5.00      196.22      0  11:49      5.00
149      J8                          JUNCTION  0.26      3.34      197.73      0  12:05      2.96
150      JP-2                       JUNCTION  1.78      2.00      200.00      0  04:18      2.00
151      J9                          JUNCTION  1.44      4.02      195.02      0  12:02      3.98
152      Out1                       OUTFALL   1.39      3.75      194.75      0  11:48      3.74
153      PropBasin                  STORAGE   0.00      0.00      200.00      0  00:00      0.00
154      OCS                        STORAGE   0.55      3.32      195.32      0  12:42      2.82
155
156

```

```

*****
Node Inflow Summary
*****

```

```

-----
162                                     Maximum  Maximum  Lateral
163                                     Total    Flow
164                                     Lateral  Total  Time of Max  Inflow
165                                     Inflow   Balance  Occurrence  Volume
166                                     Volume    Error  days hr:min  10^6 gal  10^6
167      Node                          Type      CFS      CFS      CFS
168      gal      Percent
-----
169
170      J1                          JUNCTION  7.54      7.54      0  12:05      0.23
171      0.23      0.300
172      J2                          JUNCTION  0.00      7.58      0  12:05      0
173      0.229      0.635
174      J3                          JUNCTION  716.83     716.83     0  12:05      31.9
175      31.9      0.016
176      J4                          JUNCTION  166.78     340.03     0  12:15      4.91
177      32.2      -0.007
178      J5                          JUNCTION  0.00      359.49     0  12:02      0
179      33      -0.042
180      J6                          JUNCTION  0.00      364.47     0  12:05      0
181      33      -0.014
182      J7                          JUNCTION  1.91      652.52     0  12:07      0.0374
183      31.9      -0.010
184      J8                          JUNCTION  43.86      43.86     0  12:00      1.07
185      1.07      -0.031
186      JP-2                       JUNCTION  3.63      3.63      0  12:00      0.0757
187      0.0757      3.847
188      J9                          JUNCTION  0.00      382.23     0  12:05      0
189      33      1.365

```

```

177 Out1          0.000      0.00  443.30    0  12:02      0
178 PropBasin     STORAGE    0.00    0.00    0  00:00      0
179 OCS           STORAGE    0.00    3.91    0  13:04      0
180 0.0253        0.000

```

```

182 *****
183 Node Surcharge Summary
184 *****

```

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	16.82	0.500	0.000
J2	JUNCTION	16.84	0.500	0.000
J3	JUNCTION	1.11	2.201	0.000
J4	JUNCTION	0.63	0.167	0.000
J5	JUNCTION	0.19	0.167	0.000
J6	JUNCTION	0.02	0.167	0.000
J7	JUNCTION	0.79	0.167	0.000
J8	JUNCTION	0.40	1.341	0.000
JP-2	JUNCTION	19.70	0.000	0.000

```

203 *****
204 Node Flooding Summary
205 *****

```

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J1	0.01	0.03	0 12:05	0.000	0.000
J2	16.79	7.58	0 12:05	0.228	0.000
J3	0.58	155.37	0 12:00	0.539	1.284
J4	0.44	59.57	0 11:49	0.184	0.000
J5	0.14	112.21	0 12:14	0.093	0.000
J6	0.01	84.62	0 12:14	0.009	0.000
J7	0.76	487.72	0 12:05	4.682	0.000
J8	0.38	15.30	0 12:00	0.038	0.841
JP-2	19.70	3.63	0 12:00	0.073	0.000

```

225 *****
226 Storage Volume Summary
227 *****

```

Storage Unit hr:min	Average Max Volume Occurrence	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
PropBasin 00:00	0.000	0	0	0	0.000	0	0

235 OCS 0.009 5 0 0 0.053 33 0

12:42 4.74

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	50.59	443.30	32.517
System	99.94	50.59	443.30	32.517

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	7.58	0 12:05	2.41	0.98	1.00
C3	CONDUIT	651.53	0 12:07	22.09	4.28	1.00
C4	CONDUIT	342.37	0 12:24	11.67	2.43	1.00
C5	CONDUIT	364.47	0 12:05	12.82	2.39	1.00
C6	CONDUIT	381.35	0 12:05	14.26	2.44	0.91
C2	CONDUIT	0.00	0 00:00	0.00	0.00	0.50
C7	CONDUIT	292.55	0 12:28	9.93	1.87	1.00
C8	CONDUIT	37.83	0 12:05	12.04	0.89	1.00
CP-1	CONDUIT	0.00	0 00:00	0.00	0.00	0.50
CP-2	CONDUIT	4.74	0 13:04	2.68	0.29	1.00
C9	CONDUIT	443.30	0 12:02	17.41	2.96	0.80
1	WEIR	0.00	0 00:00			0.00
2	WEIR	0.00	0 00:00			0.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.43
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.98	0.02	0.00	0.00	0.00	0.00
C2	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
C8	1.00	0.00	0.00	0.00	0.89	0.03	0.00	0.08	0.88	0.00
CP-1	1.00	0.00	0.17	0.00	0.82	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.32	0.00	0.67	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.38	0.62	0.00	0.00	0.40	0.00

Conduit Surcharge Summary

```

303 -----
304
305             ----- Hours Full -----
306 Conduit      Both Ends  Upstream  Dnstream  Hours      Hours
307             ----- Above Full ----- Capacity
308             ----- Normal Flow ----- Limited
308 C1           16.82      16.82      16.84      0.01      0.02
309 C3           0.79       1.11       0.79      1.51      0.78
310 C4           0.19       0.63       0.19      1.95      0.05
311 C5           0.01       0.19       0.02      1.82      0.01
312 C6           0.01       0.02       0.01      1.77      0.01
313 C7           0.63       0.79       0.63      1.46      0.19
314 C8           0.40       0.40       2.86      0.01      0.01
315 CP-1        0.01       0.01      19.70      0.01      0.01
316 CP-2        2.43       2.43       8.86      0.01      0.01
317 C9           0.01       0.01       0.01      1.83      0.01
318
319
320 Analysis begun on:  Wed Nov 30 11:02:51 2022
321 Analysis ended on:  Wed Nov 30 11:02:52 2022
322 Total elapsed time: 00:00:01

```

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (25-Year (2100) - PROPOSED)

WARNING 03: negative offset ignored for Link C2
WARNING 03: negative offset ignored for Link CP-1
WARNING 04: minimum elevation drop used for Conduit C9
WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

*****	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	156.205	7.531
Evaporation Loss	0.000	0.000
Infiltration Loss	21.248	1.024
Surface Runoff	126.355	6.092
Final Storage	8.843	0.426
Continuity Error (%)	-0.154	

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	126.268	41.146
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	105.847	34.492
Flooding Loss	19.050	6.208
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.050	0.016
Continuity Error (%)	1.046	

Highest Continuity Errors

Node JP-2 (3.47%)

70 Node J9 (1.32%)
 71
 72
 73 *****
 74 Time-Step Critical Elements
 75 *****
 76 Link C9 (99.98%)
 77
 78
 79 *****
 80 Highest Flow Instability Indexes
 81 *****
 82 Link C9 (62)
 83 Link C6 (54)
 84 Link C3 (16)
 85 Link C7 (14)
 86 Link CP-2 (8)
 87
 88
 89 *****
 90 Most Frequent Nonconverging Nodes
 91 *****
 92 Node Out1 (10.45%)
 93 Node J9 (10.24%)
 94 Node J6 (0.29%)
 95 Node J5 (0.20%)
 96 Node J4 (0.11%)
 97
 98
 99 *****

100 Routing Time Step Summary
 101 *****
 102 Minimum Time Step : 0.47 sec
 103 Average Time Step : 0.50 sec
 104 Maximum Time Step : 20.00 sec
 105 % of Time in Steady State : 0.00
 106 Average Iterations per Step : 3.03
 107 % of Steps Not Converging : 10.45
 108 Time Step Frequencies :
 109 20.000 - 9.564 sec : 0.01 %
 110 9.564 - 4.573 sec : 0.00 %
 111 4.573 - 2.187 sec : 0.00 %
 112 2.187 - 1.046 sec : 0.00 %
 113 1.046 - 0.500 sec : 99.98 %
 114
 115
 116 *****

117 Subcatchment Runoff Summary
 118 *****
 119
 120

Subcatchment		Total Perv Precip Runoff in 10^6 gal	Total Runon Runoff in CFS	Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
S1	4.80	5.13	7.53	0.00	2.23	0.32
S5	2.67	6.32	7.53	0.00	1.09	3.65
S3	2.63	6.00	7.53	0.00	1.07	3.37
S6			7.53	0.00	0.02	7.03


```

129      0.42      7.44      0.08      3.87      0.988
      S4              7.53      0.00      0.00      0.63      4.59
      2.14      6.73      5.26      180.25      0.894
130      S7              7.53      0.00      0.00      0.13      6.27
      1.09      7.36      0.04      2.04      0.977
131
132
133
134
135
136
137

```

```

*****
Node Depth Summary
*****

```

```

-----
138                                     Average  Maximum  Maximum  Time of Max  Reported
139                                     Depth    Depth    HGL      Occurrence  Max Depth
140      Node                        Type      Feet      Feet      Feet      days hr:min  Feet
141      -----
142      J1                        JUNCTION  1.93      2.51      197.02      0 12:05      2.50
143      J2                        JUNCTION  1.99      2.50      196.95      0 06:56      2.50
144      J3                        JUNCTION  1.90      7.35      198.60      0 12:07      6.61
145      J4                        JUNCTION  1.67      5.00      196.17      0 11:47      5.00
146      J5                        JUNCTION  1.61      5.00      196.11      0 11:50      4.80
147      J6                        JUNCTION  1.55      5.00      196.05      0 11:51      4.42
148      J7                        JUNCTION  1.68      5.00      196.22      0 11:47      5.00
149      J8                        JUNCTION  0.27      3.56      197.95      0 12:05      3.10
150      JP-2                      JUNCTION  1.80      2.00      200.00      0 04:05      2.00
151      J9                        JUNCTION  1.49      4.01      195.01      0 11:58      3.89
152      Out1                      OUTFALL   1.43      3.75      194.75      0 11:47      3.75
153      PropBasin                 STORAGE    0.00      0.00      200.00      0 00:00      0.00
154      OCS                       STORAGE    0.59      3.16      195.16      0 12:36      2.91
155
156

```

```

*****
Node Inflow Summary
*****

```

```

-----
162                                     Maximum  Maximum  Lateral
163                                     Total    Flow
164                                     Lateral  Total  Time of Max  Inflow
165                                     Inflow  Balance  Occurrence  Volume
166                                     Volume  Error  days hr:min  10^6 gal  10^6
167      Node                        Type      CFS      CFS      CFS      CFS
168      gal      Percent
169      -----
170      J1                        JUNCTION  8.32      8.32      0 12:05      0.25
171      0.25      0.278
172      J2                        JUNCTION  0.00      8.13      0 12:05      0
173      0.25      0.583
174      J3                        JUNCTION  776.48      776.48      0 12:05      34.4
175      34.4      0.015
176      J4                        JUNCTION  180.25      341.44      0 12:26      5.26
177      34.1      -0.005
178      J5                        JUNCTION  0.00      365.23      0 12:00      0
179      35      -0.044
180      J6                        JUNCTION  0.00      369.45      0 12:00      0
181      35      -0.013
182      J7                        JUNCTION  2.04      700.43      0 12:07      0.0399
183      34.4      -0.008
184      J8                        JUNCTION  47.35      47.35      0 12:00      1.15
185      1.15      -0.024
186      JP-2                      JUNCTION  3.87      3.87      0 12:00      0.0808
187      0.0808      3.596
188      J9                        JUNCTION  0.00      389.64      0 12:00      0
189      35      1.337

```

```

177 Out1          0.000      0.00  428.49    0  12:00      0
178 PropBasin     0.000 gal      0.00  0.00    0  00:00      0
179 OCS           0.0251    0.088      0.00  3.89    0  13:05      0

```

```

180
181
182 *****
183 Node Surcharge Summary
184 *****
185

```

```

186 Surcharging occurs when water rises above the top of the highest conduit.
187 -----

```

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	17.09	0.506	0.000
J2	JUNCTION	17.11	0.500	0.000
J3	JUNCTION	1.24	2.516	0.000
J4	JUNCTION	0.69	0.167	0.000
J5	JUNCTION	0.23	0.167	0.000
J6	JUNCTION	0.02	0.167	0.000
J7	JUNCTION	0.84	0.167	0.000
J8	JUNCTION	0.44	1.562	0.000
JP-2	JUNCTION	19.90	0.000	0.000

```

203 *****
204 Node Flooding Summary
205 *****
206

```

```

207 Flooding refers to all water that overflows a node, whether it ponds or not.
208 -----

```

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J1	0.16	0.48	0 12:07	0.000	0.006
J2	17.06	8.13	0 12:05	0.248	0.000
J3	0.67	181.06	0 12:00	0.666	1.599
J4	0.50	76.20	0 12:01	0.235	0.000
J5	0.16	115.86	0 12:02	0.100	0.000
J6	0.01	106.35	0 11:54	0.012	0.000
J7	0.83	543.53	0 12:06	5.535	0.000
J8	0.41	16.43	0 11:59	0.048	1.062
JP-2	19.90	3.87	0 12:00	0.078	0.000

```

225 *****
226 Storage Volume Summary
227 *****
228
229

```

```

-----

```

Storage Unit hr:min	Average Max Volume Occurrence	1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
PropBasin 00:00	0.000	0.00	0	0	0	0.000	0	0

```

-----

```

235 OCS 0.009 6 0 0 0.051 32 0

12:36 4.75

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	53.66	428.49	34.489
System	99.94	53.66	428.49	34.489

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	8.13	0	12:05	2.59	1.05	1.00
C3	CONDUIT	699.40	0	12:07	23.71	4.59	1.00
C4	CONDUIT	339.87	0	12:24	11.60	2.42	1.00
C5	CONDUIT	369.45	0	12:00	12.85	2.43	1.00
C6	CONDUIT	389.51	0	12:00	14.61	2.50	0.91
C2	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
C7	CONDUIT	291.68	0	12:31	9.89	1.87	1.00
C8	CONDUIT	39.66	0	12:07	12.62	0.94	1.00
CP-1	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
CP-2	CONDUIT	4.75	0	13:05	2.69	0.29	1.00
C9	CONDUIT	428.49	0	12:00	17.11	2.86	0.80
1	WEIR	0.00	0	00:00			0.00
2	WEIR	0.00	0	00:00			0.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.44
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.97	0.02	0.00	0.00	0.00	0.00
C2	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
C8	1.00	0.00	0.00	0.00	0.90	0.03	0.00	0.07	0.88	0.00
CP-1	1.00	0.00	0.17	0.00	0.83	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.30	0.00	0.69	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.39	0.61	0.00	0.00	0.40	0.00

Conduit Surcharge Summary

```

303 -----
304
305             ----- Hours Full -----      Hours      Hours
306 Conduit      Both Ends  Upstream  Dnstream  Above Full  Capacity
307 -----
308 C1              17.09      17.09      17.11      0.12      0.17
309 C3              0.84       1.24       0.84       1.68      0.84
310 C4              0.23       0.69       0.23       2.13      0.07
311 C5              0.02       0.23       0.02       1.98      0.01
312 C6              0.01       0.02       0.01       1.92      0.01
313 C7              0.69       0.84       0.69       1.62      0.19
314 C8              0.44       0.44       3.09       0.01      0.01
315 CP-1           0.01       0.01      19.90       0.01      0.01
316 CP-2           2.62       2.62       9.47       0.01      0.01
317 C9              0.01       0.01       0.01       2.01      0.01
318
319
320 Analysis begun on:  Wed Nov 30 11:03:17 2022
321 Analysis ended on:  Wed Nov 30 11:03:19 2022
322 Total elapsed time: 00:00:02

```

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year - PROPOSED)

WARNING 03: negative offset ignored for Link C2
 WARNING 03: negative offset ignored for Link CP-1
 WARNING 04: minimum elevation drop used for Conduit C9
 WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation	180.660	8.710
Evaporation Loss	0.000	0.000
Infiltration Loss	22.022	1.062
Surface Runoff	149.464	7.206
Final Storage	9.462	0.456
Continuity Error (%)	-0.160	

	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	149.365	48.673
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	120.434	39.245
Flooding Loss	27.599	8.993
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.053	0.017
Continuity Error (%)	0.856	

Highest Continuity Errors

Node JP-2 (3.00%)

70 Node J9 (1.14%)
 71
 72
 73 *****
 74 Time-Step Critical Elements
 75 *****
 76 Link C9 (99.98%)
 77
 78
 79 *****
 80 Highest Flow Instability Indexes
 81 *****
 82 Link C9 (76)
 83 Link C6 (69)
 84 Link C3 (19)
 85 Link C7 (17)
 86 Link CP-2 (11)
 87
 88
 89 *****
 90 Most Frequent Nonconverging Nodes
 91 *****
 92 Node Out1 (12.31%)
 93 Node J9 (12.06%)
 94 Node J6 (0.34%)
 95 Node J5 (0.23%)
 96 Node J4 (0.15%)
 97
 98
 99 *****
 100 Routing Time Step Summary
 101 *****
 102 Minimum Time Step : 0.13 sec
 103 Average Time Step : 0.50 sec
 104 Maximum Time Step : 20.00 sec
 105 % of Time in Steady State : 0.00
 106 Average Iterations per Step : 3.22
 107 % of Steps Not Converging : 12.31
 108 Time Step Frequencies :
 109 20.000 - 9.564 sec : 0.01 %
 110 9.564 - 4.573 sec : 0.00 %
 111 4.573 - 2.187 sec : 0.00 %
 112 2.187 - 1.046 sec : 0.00 %
 113 1.046 - 0.500 sec : 99.98 %
 114
 115

116 *****
 117 Subcatchment Runoff Summary
 118 *****
 119
 120

		Total Perv Precip Runoff	Total Total Runon Runoff	Total Total Evap Runoff	Total Peak Infil Runoff	Imperv Runoff Coeff
Subcatchment	in	in	in	in	in	in
	in	10^6 gal	CFS			
S1		8.71	0.00	0.00	2.33	0.37
5.82	6.20	0.30	10.47	0.712		
S5		8.71	0.00	0.00	1.14	4.22
3.23	7.45	1.36	56.90	0.855		
S3		8.71	0.00	0.00	1.11	3.90
3.21	7.11	40.74	941.46	0.816		
S6		8.71	0.00	0.00	0.02	8.14

```

129      0.49      8.62      0.09      4.53      0.990
S4              8.71      0.00      0.00      0.64      5.32
2.56      7.88      6.16      217.11      0.905
130      S7              8.71      0.00      0.00      0.13      7.26
1.28      8.53      0.05      2.38      0.980

```

```

131
132
133 *****
134 Node Depth Summary
135 *****

```

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	1.98	2.54	197.05	0 12:05	2.52
J2	JUNCTION	2.04	2.50	196.95	0 06:15	2.50
J3	JUNCTION	2.06	8.30	199.55	0 12:07	7.41
J4	JUNCTION	1.79	5.00	196.17	0 11:45	5.00
J5	JUNCTION	1.73	5.00	196.11	0 11:47	4.81
J6	JUNCTION	1.66	5.00	196.05	0 11:50	4.26
J7	JUNCTION	1.80	5.00	196.22	0 11:45	5.00
J8	JUNCTION	0.31	4.20	198.59	0 12:06	3.52
JP-2	JUNCTION	1.82	2.00	200.00	0 03:39	2.00
J9	JUNCTION	1.59	4.04	195.04	0 12:00	3.94
Out1	OUTFALL	1.54	3.75	194.75	0 11:45	3.75
PropBasin	STORAGE	0.00	0.00	200.00	0 00:00	0.00
OCS	STORAGE	0.68	3.63	195.63	0 12:51	3.16

```

155
156 *****
157 Node Inflow Summary
158 *****
159
160
161

```

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1		JUNCTION	10.47	10.47	0 12:05	0.303	
0.303	0.239						
J2		JUNCTION	0.00	10.12	0 12:06	0	
0.302	0.482						
J3		JUNCTION	941.46	941.46	0 12:05	40.7	
40.7	0.017						
J4		JUNCTION	217.11	373.74	0 12:00	6.16	
38.9	-0.010						
J5		JUNCTION	0.00	360.93	0 11:56	0	
39.8	-0.043						
J6		JUNCTION	0.00	363.23	0 12:04	0	
39.7	-0.017						
J7		JUNCTION	2.38	829.14	0 12:07	0.0463	
40.8	-0.009						
J8		JUNCTION	56.90	56.90	0 12:00	1.35	
1.35	-0.041						
JP-2		JUNCTION	4.53	4.53	0 12:00	0.0936	
0.0936	3.089						
J9		JUNCTION	0.00	388.22	0 12:00	0	
39.7	1.157						

```

177 Out1          0.00  429.67  0  12:00  0
    39.2      0.000
178 PropBasin     STORAGE  0.00  0.00  0  00:00  0
    0      0.000 gal
179 OCS           STORAGE  0.00  5.64  0  12:51  0
    0.0295      0.180

```

```

182 *****
183 Node Surcharge Summary
184 *****

```

185
186 Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	17.77	0.543	0.000
J2	JUNCTION	17.78	0.500	0.000
J3	JUNCTION	1.56	3.471	0.000
J4	JUNCTION	0.85	0.167	0.000
J5	JUNCTION	0.25	0.167	0.000
J6	JUNCTION	0.02	0.167	0.000
J7	JUNCTION	1.07	0.167	0.000
J8	JUNCTION	0.53	2.204	0.000
JP-2	JUNCTION	20.33	0.000	0.000

```

203 *****
204 Node Flooding Summary
205 *****

```

206
207 Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J1	0.27	1.53	0 12:00	0.003	0.043
J2	17.74	10.12	0 12:06	0.301	0.000
J3	0.88	253.18	0 12:00	1.072	2.554
J4	0.60	106.65	0 12:01	0.451	0.000
J5	0.17	121.33	0 11:57	0.116	0.000
J6	0.01	91.35	0 12:13	0.011	0.000
J7	1.05	673.08	0 12:07	8.024	0.000
J8	0.51	22.58	0 11:59	0.077	1.704
JP-2	20.33	4.53	0 12:00	0.091	0.000

```

225 *****
226 Storage Volume Summary
227 *****

```

Storage Unit hr:min	Average Max Volume Occurrence	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
PropBasin 00:00	0.000	0	0	0	0.000	0	0

235 OCS 0.011 7 0 0 0.058 36 0

12:51 4.64

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	61.05	429.67	39.242
System	99.94	61.05	429.67	39.242

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	10.12	0	12:06	3.22	1.31	1.00
C3	CONDUIT	828.04	0	12:07	28.07	5.44	1.00
C4	CONDUIT	347.79	0	12:27	11.81	2.47	1.00
C5	CONDUIT	363.23	0	12:04	12.79	2.39	1.00
C6	CONDUIT	388.20	0	12:00	14.46	2.49	0.91
C2	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
C7	CONDUIT	298.87	0	12:38	10.15	1.92	1.00
C8	CONDUIT	44.02	0	12:08	14.01	1.04	1.00
CP-1	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
CP-2	CONDUIT	5.64	0	12:51	3.19	0.35	1.00
C9	CONDUIT	429.67	0	12:00	17.13	2.87	0.81
1	WEIR	0.00	0	00:00			0.00
2	WEIR	0.00	0	00:00			0.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								Norm Ltd	Inlet Ctrl
		Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit			
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.01	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.48
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.97	0.03	0.00	0.00	0.00	0.00	0.00
C2	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.01	0.00
C8	1.00	0.00	0.00	0.00	0.91	0.02	0.00	0.06	0.06	0.88	0.00
CP-1	1.00	0.00	0.15	0.00	0.85	0.00	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.25	0.00	0.74	0.00	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.42	0.57	0.00	0.00	0.38	0.00	0.00

Conduit Surcharge Summary

```

303 -----
304
305             ----- Hours Full -----
306 Conduit      Both Ends  Upstream  Dnstream    Hours      Hours
307             ----- Above Full ----- Capacity
308             ----- Normal Flow ----- Limited
308 C1           17.77      17.77      17.78      0.23      0.27
309 C3           1.07      1.56      1.07      2.08      1.06
310 C4           0.25      0.84      0.25      2.54      0.07
311 C5           0.02      0.25      0.02      2.38      0.01
312 C6           0.01      0.02      0.01      2.31      0.01
313 C7           0.84      1.07      0.84      2.03      0.24
314 C8           0.53      0.53      3.61      0.02      0.02
315 CP-1         0.01      0.01      20.33      0.01      0.01
316 CP-2         3.17      3.17      10.90      0.01      0.01
317 C9           0.01      0.01      0.01      2.39      0.01
318
319
320 Analysis begun on:  Wed Nov 30 11:05:06 2022
321 Analysis ended on:  Wed Nov 30 11:05:08 2022
322 Total elapsed time: 00:00:02

```

Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year (2050) - PROPOSED)

WARNING 03: negative offset ignored for Link C2
 WARNING 03: negative offset ignored for Link CP-1
 WARNING 04: minimum elevation drop used for Conduit C9
 WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	207.271	9.993
Evaporation Loss	0.000	0.000
Infiltration Loss	22.701	1.094
Surface Runoff	174.879	8.431
Final Storage	10.032	0.484
Continuity Error (%)	-0.164	

Flow Routing Continuity

	Volume acre-feet	Volume 10 ⁶ gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	174.769	56.951
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	134.800	43.927
Flooding Loss	38.579	12.572
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.057	0.018
Continuity Error (%)	0.763	

Highest Continuity Errors

Node JP-2 (2.61%)

```

70 Node J9 (1.09%)
71
72
73 *****
74 Time-Step Critical Elements
75 *****
76 Link C9 (99.98%)
77
78
79 *****
80 Highest Flow Instability Indexes
81 *****
82 Link C9 (77)
83 Link C6 (68)
84 Link C3 (22)
85 Link C7 (19)
86 Link CP-2 (12)
87
88
89 *****
90 Most Frequent Nonconverging Nodes
91 *****
92 Node Out1 (14.20%)
93 Node J9 (13.89%)
94 Node J6 (0.43%)
95 Node J5 (0.29%)
96 Node J4 (0.18%)
97
98
99 *****
100 Routing Time Step Summary
101 *****
102 Minimum Time Step      :      0.30 sec
103 Average Time Step      :      0.50 sec
104 Maximum Time Step      :     20.00 sec
105 % of Time in Steady State :      0.00
106 Average Iterations per Step :      3.37
107 % of Steps Not Converging :     14.20
108 Time Step Frequencies  :
109     20.000 - 9.564 sec   :      0.01 %
110     9.564 - 4.573 sec   :      0.00 %
111     4.573 - 2.187 sec   :      0.00 %
112     2.187 - 1.046 sec   :      0.00 %
113     1.046 - 0.500 sec   :     99.99 %
114
115

```

```

116 *****
117 Subcatchment Runoff Summary
118 *****
119
120

```

Subcatchment		Total Perv Precip Runoff in 10^6 gal	Total Runon Runoff in CFS	Total Total Evap Runoff in	Total Peak Infil Runoff in	Imperv Runoff Coeff in
125	S1	9.99	0.00	0.00	2.42	0.43
	6.96	7.39	0.36	12.89	0.739	
126	S5	9.99	0.00	0.00	1.17	4.85
	3.84	8.69	1.58	67.61	0.870	
127	S3	9.99	0.00	0.00	1.14	4.49
	3.84	8.33	47.73	1128.20	0.834	
128	S6	9.99	0.00	0.00	0.02	9.34

129 0.56 9.91 0.11 5.26 0.991
S4 9.99 0.00 0.00 0.66 6.11
3.03 9.14 7.15 258.55 0.915
130 S7 9.99 0.00 0.00 0.13 8.33
1.48 9.82 0.05 2.74 0.982

131
132
133 *****
134 Node Depth Summary
135 *****

		Average	Maximum	Maximum	Time of Max		Reported
		Depth	Depth	HGL	Occurrence		Max Depth
Node	Type	Feet	Feet	Feet	days	hr:min	Feet
J1	JUNCTION	2.03	2.59	197.10	0	12:05	2.55
J2	JUNCTION	2.09	2.50	196.95	0	05:40	2.50
J3	JUNCTION	2.23	9.53	200.78	0	12:07	8.48
J4	JUNCTION	1.91	5.00	196.17	0	11:44	5.00
J5	JUNCTION	1.84	5.00	196.11	0	11:46	5.00
J6	JUNCTION	1.77	5.00	196.05	0	11:50	4.69
J7	JUNCTION	1.92	5.00	196.22	0	11:42	5.00
J8	JUNCTION	0.35	4.98	199.37	0	12:06	4.01
JP-2	JUNCTION	1.83	2.00	200.00	0	03:17	2.00
J9	JUNCTION	1.70	4.02	195.02	0	11:59	3.90
Out1	OUTFALL	1.64	3.75	194.75	0	11:42	3.75
PropBasin	STORAGE	0.00	0.00	200.00	0	00:00	0.00
OCS	STORAGE	0.76	3.41	195.41	0	13:06	2.98

155
156
157 *****
158 Node Inflow Summary
159 *****
160
161

-----			Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
Node gal	Percent	Type					

J1 0.361	0.200	JUNCTION	12.89	12.89	0 12:05	0.361	
J2 0.36	0.404	JUNCTION	0.00	12.32	0 12:06	0	
J3 47.7	0.014	JUNCTION	1128.20	1128.20	0 12:05	47.7	
J4 43.7	-0.012	JUNCTION	258.55	414.78	0 12:00	7.14	
J5 44.5	-0.056	JUNCTION	0.00	364.96	0 11:58	0	
J6 44.4	-0.020	JUNCTION	0.00	363.98	0 11:55	0	
J7 47.7	-0.009	JUNCTION	2.74	969.14	0 12:07	0.0533	
J8 1.58	-0.041	JUNCTION	67.61	67.61	0 12:00	1.58	
JP-2 0.108	2.678	JUNCTION	5.26	5.26	0 12:00	0.108	
J9 44.4	1.102	JUNCTION	0.00	386.48	0 12:06	0	

```

177 Out1          0.000      0.000      0.00      443.36      0      11:59      0
178 PropBasin      0.000 gal      0.00      0.00      0      00:00      0
179 OCS            0.0314      0.265      0.00      4.06      0      13:32      0

```

```

180
181
182 *****
183 Node Surcharge Summary
184 *****
185

```

```

186 Surcharging occurs when water rises above the top of the highest conduit.
187 -----

```

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
J1	JUNCTION	18.35	0.592	0.000
J2	JUNCTION	18.36	0.500	0.000
J3	JUNCTION	1.91	4.693	0.000
J4	JUNCTION	1.04	0.167	0.000
J5	JUNCTION	0.34	0.167	0.000
J6	JUNCTION	0.03	0.167	0.000
J7	JUNCTION	1.33	0.167	0.000
J8	JUNCTION	0.64	2.983	0.000
JP-2	JUNCTION	20.71	0.000	0.000

```

201
202
203 *****
204 Node Flooding Summary
205 *****
206

```

```

207 Flooding refers to all water that overflows a node, whether it ponds or not.
208 -----

```

Node	Hours Flooded	Maximum Rate CFS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 gal	Maximum Ponded Depth Feet
J1	0.35	2.49	0 12:00	0.007	0.092
J2	18.32	12.32	0 12:06	0.359	0.000
J3	1.08	340.57	0 12:00	1.564	3.776
J4	0.77	156.82	0 12:01	0.746	0.000
J5	0.23	111.47	0 12:27	0.151	0.000
J6	0.02	90.43	0 12:03	0.020	0.000
J7	1.31	813.07	0 12:07	11.191	0.000
J8	0.61	29.01	0 12:00	0.112	2.483
JP-2	20.71	5.26	0 12:00	0.105	0.000

```

223
224
225 *****
226 Storage Volume Summary
227 *****
228
229

```

```

-----

```

Storage Unit hr:min	CFS	Average Max Volume Occurrence	1000 ft3	Avg Maximum Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of days
PropBasin 00:00	0.00	0.000	0	0	0	0	0.000	0	0

```

-----

```

235 OCS 0.012 8 0 0 0.055 34 0

13:06 4.33

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	68.32	443.36	43.923
System	99.94	68.32	443.36	43.923

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	12.32	0	12:06	3.92	1.59	1.00
C3	CONDUIT	967.96	0	12:07	32.81	6.36	1.00
C4	CONDUIT	340.05	0	12:50	11.65	2.42	1.00
C5	CONDUIT	363.98	0	11:55	12.83	2.39	1.00
C6	CONDUIT	386.48	0	12:06	14.55	2.48	0.91
C2	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
C7	CONDUIT	302.71	0	12:49	10.26	1.94	1.00
C8	CONDUIT	48.71	0	12:07	15.51	1.15	1.00
CP-1	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
CP-2	CONDUIT	4.33	0	13:33	2.45	0.27	1.00
C9	CONDUIT	443.36	0	11:59	17.42	2.96	0.80
1	WEIR	0.00	0	00:00			0.00
2	WEIR	0.00	0	00:00			0.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								Norm Ltd	Inlet Ctrl
		Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit			
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.01	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.47
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.96	0.03	0.00	0.00	0.00	0.00	0.00
C2	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.02	0.00
C8	1.00	0.00	0.00	0.00	0.92	0.02	0.00	0.00	0.05	0.87	0.00
CP-1	1.00	0.00	0.13	0.00	0.86	0.00	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.21	0.00	0.78	0.00	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.41	0.58	0.00	0.00	0.40	0.00	0.00

Conduit Surcharge Summary

```

303 -----
304
305             ----- Hours Full -----
306 Conduit      Both Ends  Upstream  Dnstream      Hours      Hours
307                                     Above Full  Capacity
308                                     Normal Flow  Limited
309 -----
310 C1              18.35      18.35      18.36          0.32          0.36
311 C3              1.33      1.91      1.33          2.45          1.32
312 C4              0.33      1.04      0.33          2.98          0.10
313 C5              0.03      0.33      0.03          2.80          0.01
314 C6              0.01      0.03      0.01          2.72          0.01
315 C7              1.04      1.33      1.04          2.37          0.27
316 C8              0.64      0.64      4.29          0.18          0.18
317 CP-1           0.01      0.01      20.71         0.01          0.01
318 CP-2           3.71      3.71      12.67         0.01          0.01
319 C9              0.01      0.01      0.01          2.82          0.01
320
321 Analysis begun on:  Wed Nov 30 11:05:34 2022
322 Analysis ended on:  Wed Nov 30 11:05:35 2022
323 Total elapsed time: 00:00:01

```


Location 12: Location 12: Industrial Drive and Post Office Road SWMM Schematic (100-Year (2100) - PROPOSED)

WARNING 03: negative offset ignored for Link C2
 WARNING 03: negative offset ignored for Link CP-1
 WARNING 04: minimum elevation drop used for Conduit C9
 WARNING 02: maximum depth increased for Node J9

Analysis Options

Flow Units CFS

Process Models:

Rainfall/Runoff YES

RDII NO

Snowmelt NO

Groundwater NO

Flow Routing YES

Ponding Allowed YES

Water Quality NO

Infiltration Method CURVE_NUMBER

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 01/01/2000 00:00:00

Ending Date 01/02/2000 00:00:00

Antecedent Dry Days 0.0

Report Time Step 00:15:00

Wet Time Step 00:05:00

Dry Time Step 01:00:00

Routing Time Step 20.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.005000 ft

Runoff Quantity Continuity

	Volume acre-feet	Depth inches
Total Precipitation	218.596	10.539
Evaporation Loss	0.000	0.000
Infiltration Loss	22.949	1.106
Surface Runoff	185.655	8.951
Final Storage	10.356	0.499
Continuity Error (%)	-0.166	

Flow Routing Continuity

	Volume acre-feet	Volume 10 ⁶ gal
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	185.538	60.460
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	141.057	45.965
Flooding Loss	42.988	14.008
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.058	0.019
Continuity Error (%)	0.774	

Highest Continuity Errors

Node JP-2 (2.47%)

```

70 Node J9 (1.11%)
71
72
73 *****
74 Time-Step Critical Elements
75 *****
76 Link C9 (99.98%)
77
78
79 *****
80 Highest Flow Instability Indexes
81 *****
82 Link C9 (77)
83 Link C6 (67)
84 Link C3 (20)
85 Link C7 (18)
86 Link CP-2 (13)
87
88
89 *****
90 Most Frequent Nonconverging Nodes
91 *****
92 Node Out1 (14.91%)
93 Node J9 (14.60%)
94 Node J6 (0.44%)
95 Node J5 (0.27%)
96 Node J4 (0.19%)
97
98
99 *****
100 Routing Time Step Summary
101 *****
102 Minimum Time Step      :      0.17 sec
103 Average Time Step      :      0.50 sec
104 Maximum Time Step      :     20.00 sec
105 % of Time in Steady State :      0.00
106 Average Iterations per Step :      3.44
107 % of Steps Not Converging :     14.91
108 Time Step Frequencies  :
109     20.000 - 9.564 sec   :      0.01 %
110     9.564 - 4.573 sec   :      0.00 %
111     4.573 - 2.187 sec   :      0.00 %
112     2.187 - 1.046 sec   :      0.00 %
113     1.046 - 0.500 sec   :     99.99 %
114
115

```

```

116 *****
117 Subcatchment Runoff Summary
118 *****
119
120

```

```

-----
121                                     Total      Total      Total      Total      Imperv
122                                     Perv      Total      Total      Peak      Runoff
123                                     Precip    Runon      Evap      Infil      Runoff
124 Subcatchment      in      10^6 gal      CFS      in      in      Coeff      in
125 -----
126 S1      7.44      7.90      0.39      13.88      0.749      0.00      2.45      0.45
127 S5      4.11      9.22      1.68      72.01      0.875      0.00      1.19      5.11
128 S3      4.11      8.85      50.69      1205.48      0.840      0.00      1.16      4.74
129 S6      10.54      0.00      0.00      0.02      9.86

```

```

129      0.59      10.45      0.11      5.56      0.992
S4              10.54      0.00      0.00      0.67      6.45
3.23      9.68      7.57      275.58      0.918
130      S7              10.54      0.00      0.00      0.13      8.79
1.57      10.36      0.06      2.89      0.983

```

```

131
132
133 *****
134 Node Depth Summary
135 *****

```

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
J1	JUNCTION	2.05	2.61	197.12	0 12:05	2.56
J2	JUNCTION	2.10	2.50	196.95	0 05:28	2.50
J3	JUNCTION	2.30	10.07	201.32	0 12:07	8.97
J4	JUNCTION	1.96	5.00	196.17	0 11:44	5.00
J5	JUNCTION	1.89	5.00	196.11	0 11:45	5.00
J6	JUNCTION	1.82	5.00	196.05	0 11:45	4.35
J7	JUNCTION	1.97	5.00	196.22	0 11:44	5.00
J8	JUNCTION	0.37	5.32	199.71	0 12:06	4.23
JP-2	JUNCTION	1.84	2.00	200.00	0 03:07	2.00
J9	JUNCTION	1.74	4.03	195.03	0 12:05	3.85
Out1	OUTFALL	1.68	3.75	194.75	0 11:42	3.75
PropBasin	STORAGE	0.00	0.00	200.00	0 00:00	0.00
OCS	STORAGE	0.80	3.43	195.43	0 13:13	3.18

```

155
156
157 *****
158 Node Inflow Summary
159 *****

```

Node gal	Percent	Type	Maximum Total Lateral Inflow Volume CFS	Maximum Flow Total Balance Inflow Error CFS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 gal	10^6
J1		JUNCTION	13.88	13.88	0 12:05	0.386	
0.386	0.181						
J2		JUNCTION	0.00	13.20	0 12:06	0	
0.385	0.377						
J3		JUNCTION	1205.48	1205.48	0 12:05	50.7	
50.7	0.014						
J4		JUNCTION	275.58	431.72	0 12:00	7.56	
45.8	-0.014						
J5		JUNCTION	0.00	366.96	0 12:08	0	
46.6	-0.046						
J6		JUNCTION	0.00	366.23	0 12:04	0	
46.5	-0.019						
J7		JUNCTION	2.89	1025.38	0 12:07	0.0563	
50.7	-0.007						
J8		JUNCTION	72.01	72.01	0 12:00	1.68	
1.68	-0.051						
JP-2		JUNCTION	5.56	5.56	0 12:00	0.113	
0.113	2.534						
J9		JUNCTION	0.00	391.93	0 12:04	0	
46.5	1.120						

```

177 Out1          0.000          0.00  445.74    0  12:05          0
178 PropBasin     0.000          0.00    0.00    0  00:00          0
179 OCS           0.0328      0.300          0.00    4.21    0  12:59          0

```

```

180
181
182 *****
183 Node Surcharge Summary
184 *****
185

```

186 Surcharging occurs when water rises above the top of the highest conduit.

187 -----

188			Hours	Max. Height	Min. Depth
189			Surcharged	Above Crown	Below Rim
190	Node	Type		Feet	Feet
191	-----				
192	J1	JUNCTION	18.55	0.615	0.000
193	J2	JUNCTION	18.56	0.500	0.000
194	J3	JUNCTION	2.04	5.238	0.000
195	J4	JUNCTION	1.10	0.167	0.000
196	J5	JUNCTION	0.34	0.167	0.000
197	J6	JUNCTION	0.03	0.167	0.000
198	J7	JUNCTION	1.42	0.167	0.000
199	J8	JUNCTION	0.68	3.317	0.000
200	JP-2	JUNCTION	20.87	0.000	0.000

```

201
202
203 *****
204 Node Flooding Summary
205 *****
206

```

207 Flooding refers to all water that overflows a node, whether it ponds or not.

208 -----

209			Maximum	Time of Max	Total	Maximum
210		Hours	Rate	Occurrence	Flood	Ponded
211		Flooded	CFS	days hr:min	Volume	Depth
212	Node				10^6 gal	Feet
213	-----					
214	J1	0.41	2.86	0 12:00	0.008	0.115
215	J2	18.52	13.20	0 12:06	0.384	0.000
216	J3	1.15	378.29	0 12:00	1.793	4.321
217	J4	0.78	168.55	0 12:03	0.851	0.000
218	J5	0.24	125.98	0 12:07	0.156	0.000
219	J6	0.02	96.77	0 12:06	0.017	0.000
220	J7	1.39	869.31	0 12:07	12.489	0.000
221	J8	0.64	31.18	0 12:00	0.126	2.817
222	JP-2	20.87	5.56	0 12:00	0.111	0.000

```

223
224
225 *****
226 Storage Volume Summary
227 *****
228
229

```

230 -----

231 -----

230		Average	Avg	Evap	Exfil	Maximum	Max	Time of
231		Max	Maximum					
232	Storage Unit	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	
233	hr:min	Occurrence	Outflow	Loss	Loss			days
234		1000 ft3	Full	Loss	Loss	1000 ft3	Full	
235	CFS							
236	-----							
237	PropBasin	0.000	0	0	0	0.000	0	0
238	00:00	0.00						

235 OCS 0.013 8 0 0 0.055 34 0

13:13 3.57

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Out1	99.94	71.49	445.74	45.962
System	99.94	71.49	445.74	45.962

Link Flow Summary

Link	Type	Maximum Flow CFS	Time of Max Occurrence days hr:min		Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
C1	CONDUIT	13.20	0	12:06	4.20	1.70	1.00
C3	CONDUIT	1024.18	0	12:07	34.72	6.73	1.00
C4	CONDUIT	346.47	0	12:31	11.75	2.46	1.00
C5	CONDUIT	366.23	0	12:04	12.89	2.41	1.00
C6	CONDUIT	390.54	0	12:04	14.56	2.50	0.91
C2	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
C7	CONDUIT	302.33	0	12:53	10.26	1.94	1.00
C8	CONDUIT	51.40	0	12:09	16.36	1.22	1.00
CP-1	CONDUIT	0.00	0	00:00	0.00	0.00	0.50
CP-2	CONDUIT	4.21	0	12:59	2.38	0.26	1.00
C9	CONDUIT	445.74	0	12:05	17.52	2.98	0.80
1	WEIR	0.00	0	00:00			0.00
2	WEIR	0.00	0	00:00			0.00

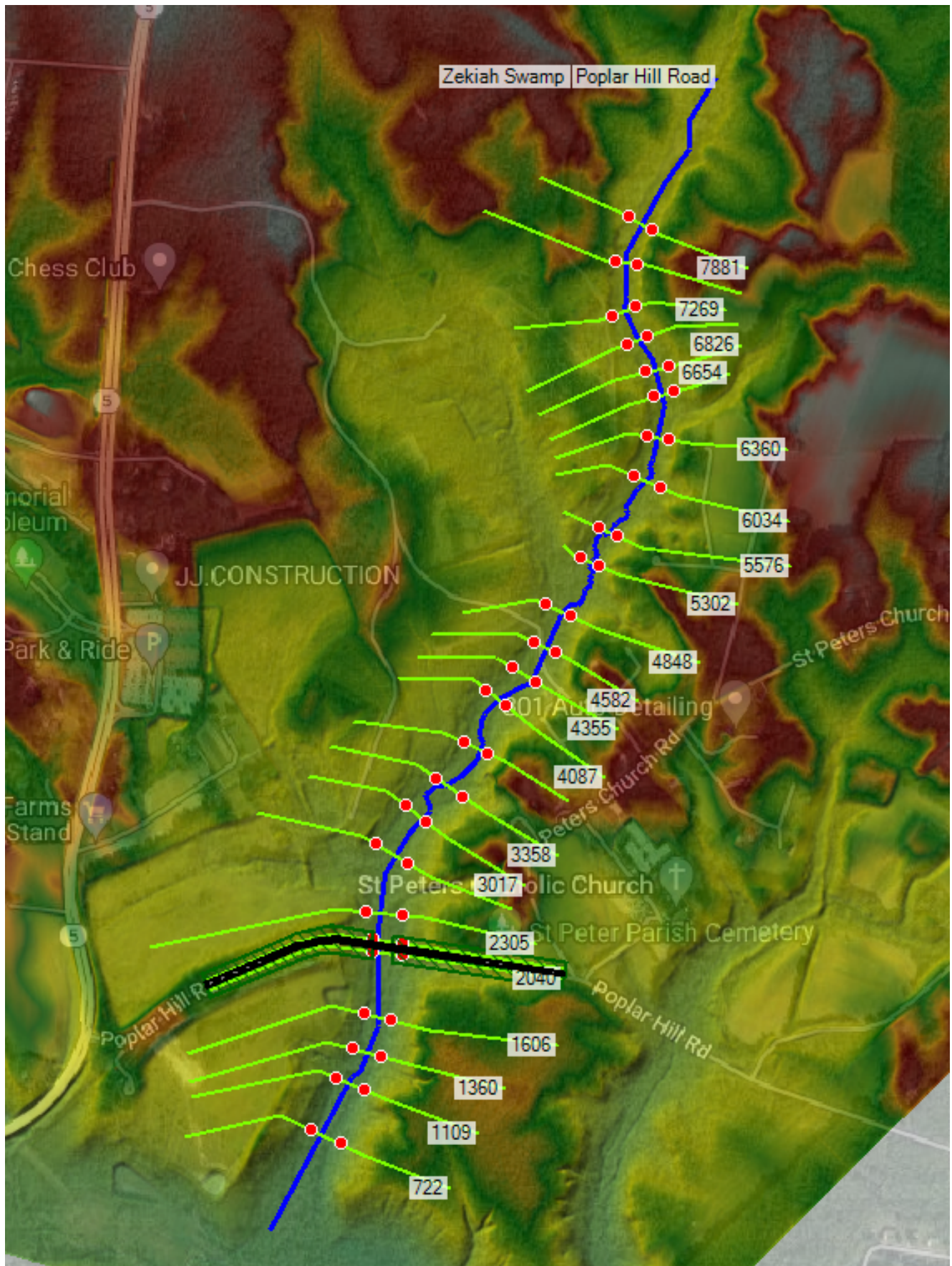
Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								Norm Ltd	Inlet Ctrl
		Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit			
C1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.01	0.00
C3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.48
C4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
C6	1.00	0.00	0.00	0.00	0.96	0.03	0.00	0.00	0.00	0.00	0.00
C2	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C7	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.02	0.00
C8	1.00	0.00	0.00	0.00	0.93	0.02	0.00	0.00	0.05	0.87	0.00
CP-1	1.00	0.00	0.13	0.00	0.87	0.00	0.00	0.00	0.00	0.00	0.00
CP-2	1.00	0.00	0.20	0.00	0.80	0.00	0.00	0.00	0.00	0.00	0.00
C9	1.00	0.00	0.00	0.00	0.41	0.58	0.00	0.00	0.41	0.00	0.00

Conduit Surcharge Summary

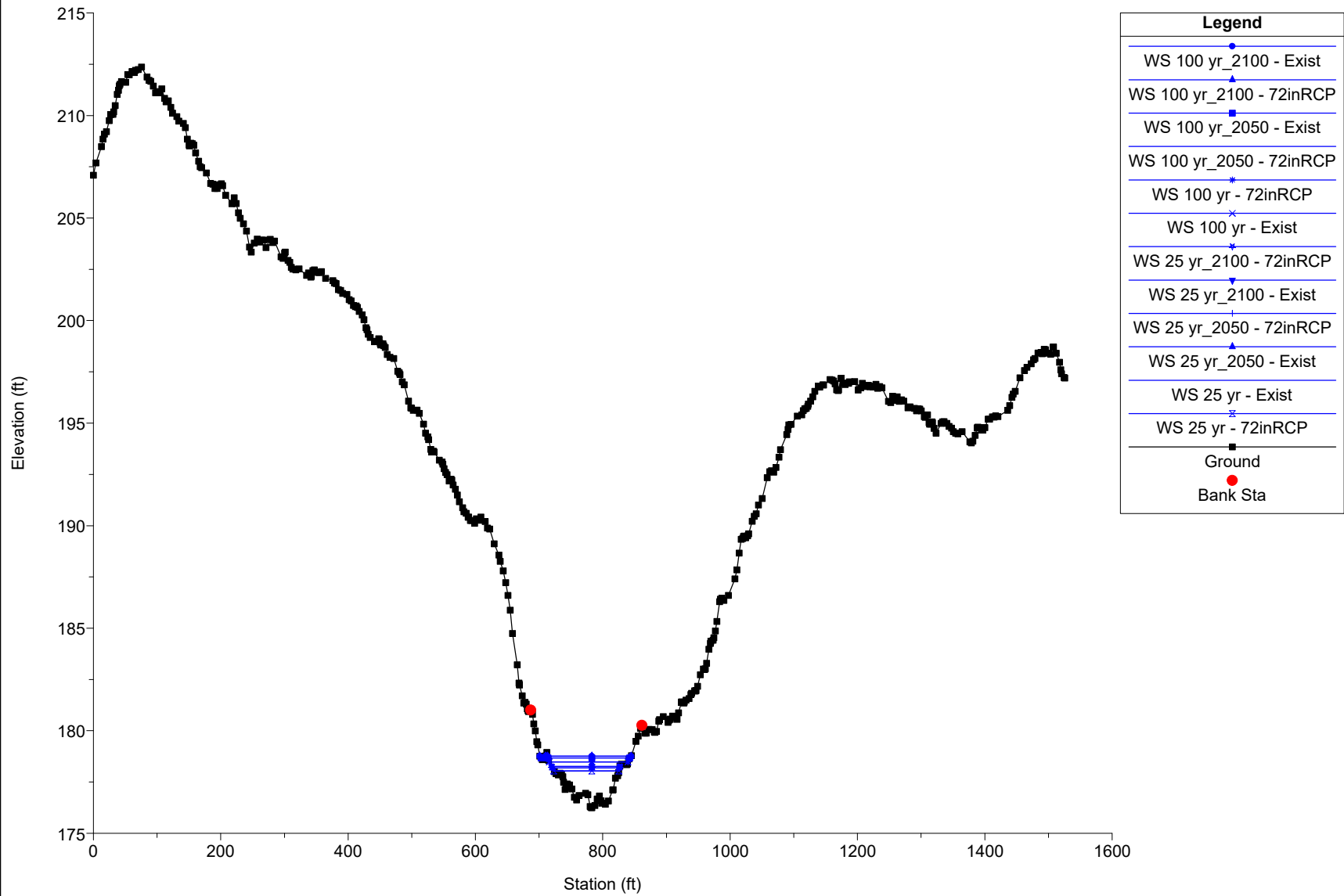
303	-----					
304						
305		Hours Full			Hours	Hours
306	Conduit	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
307	-----					
308	C1	18.55	18.55	18.56	0.35	0.42
309	C3	1.42	2.04	1.42	2.61	1.42
310	C4	0.33	1.10	0.33	3.19	0.09
311	C5	0.03	0.33	0.03	2.97	0.01
312	C6	0.01	0.03	0.01	2.88	0.01
313	C7	1.10	1.42	1.10	2.51	0.31
314	C8	0.68	0.68	4.53	0.23	0.23
315	CP-1	0.01	0.01	20.87	0.01	0.01
316	CP-2	3.93	3.93	13.77	0.01	0.01
317	C9	0.01	0.01	0.01	3.00	0.01
318						
319						
320	Analysis begun on: Wed Nov 30 11:06:07 2022					
321	Analysis ended on: Wed Nov 30 11:06:09 2022					
322	Total elapsed time: 00:00:02					

Location 24: Poplar Hill Rd. HEC-RAS Schematic

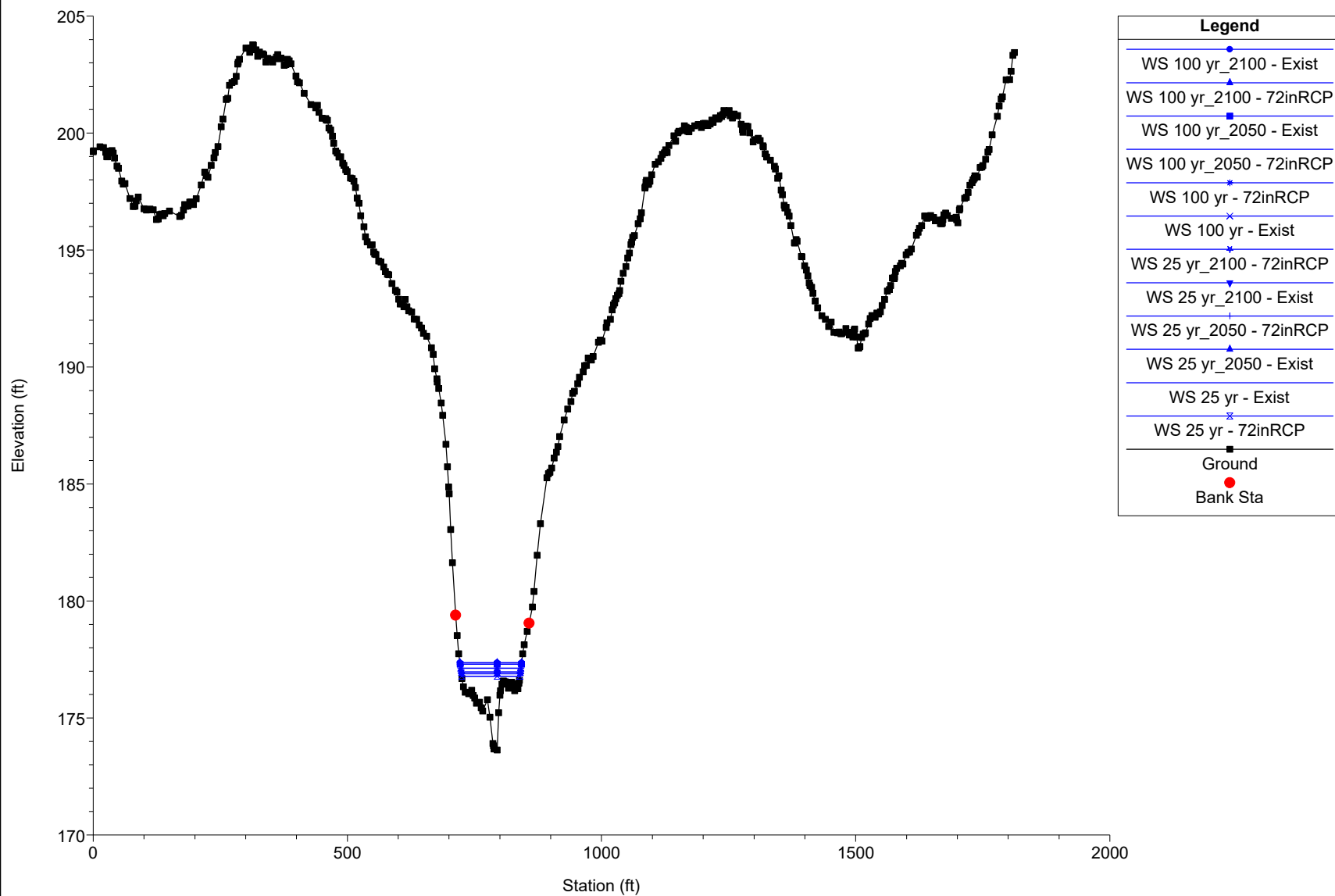


Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 7881

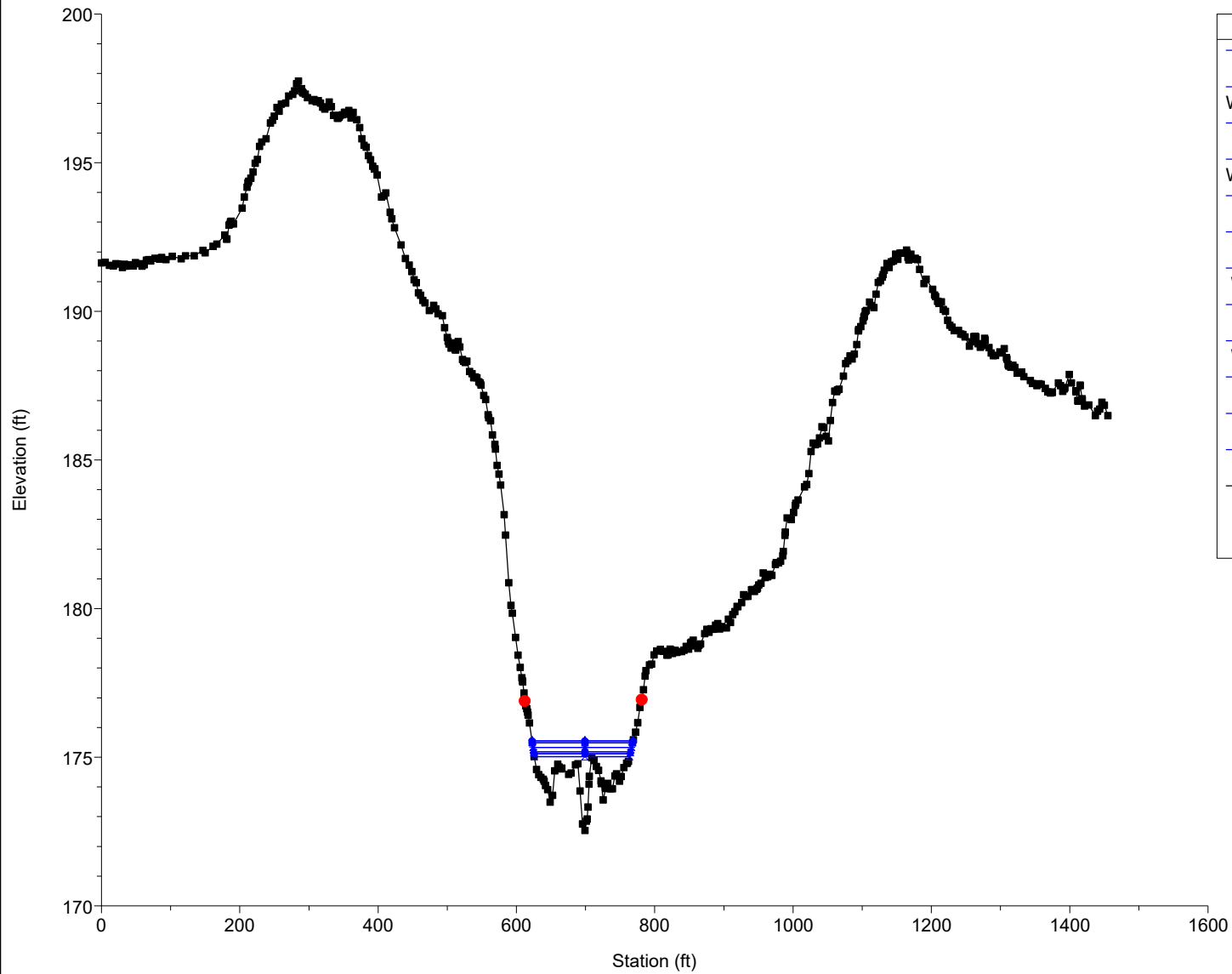


Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 7596



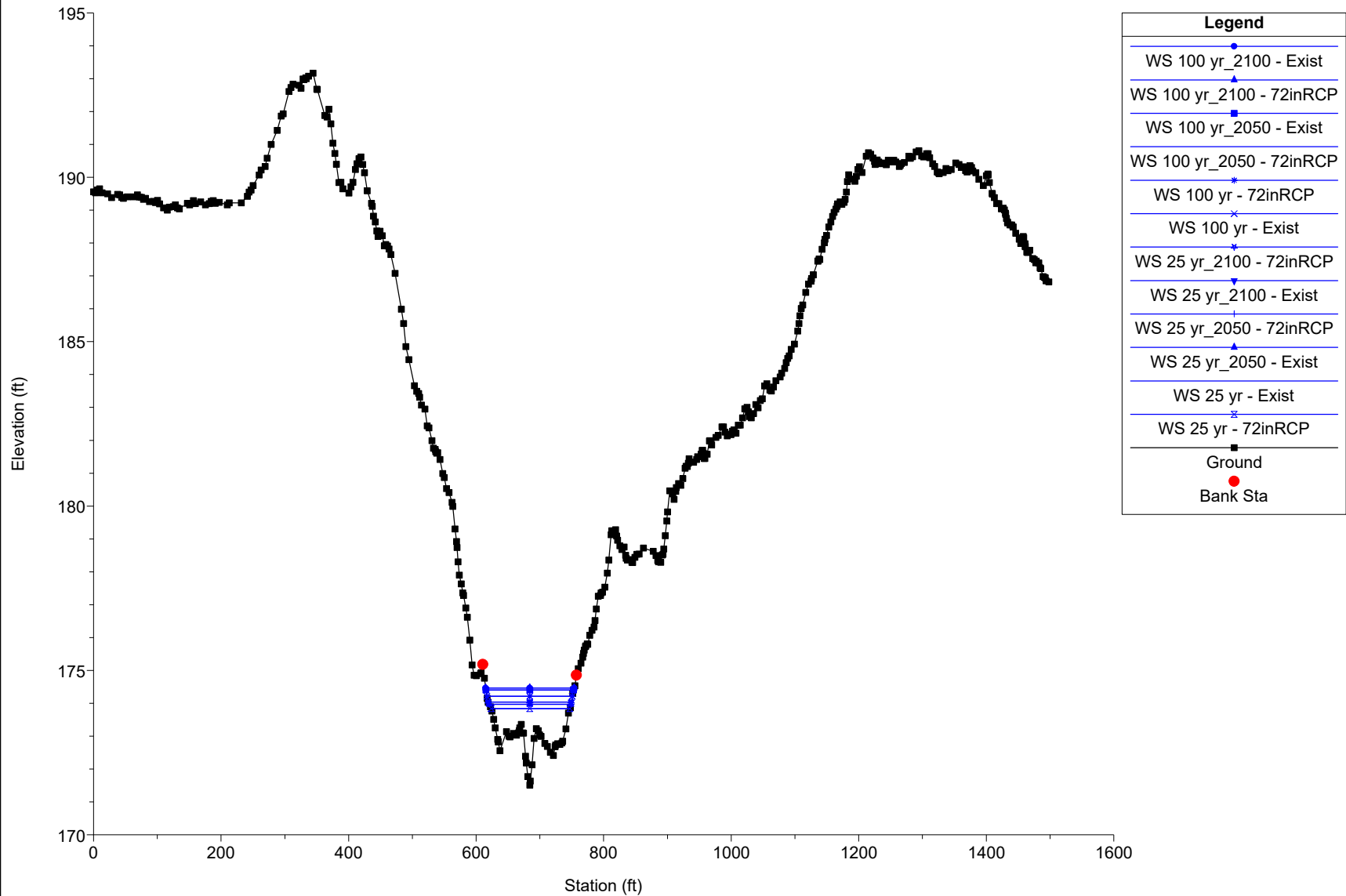
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 7269

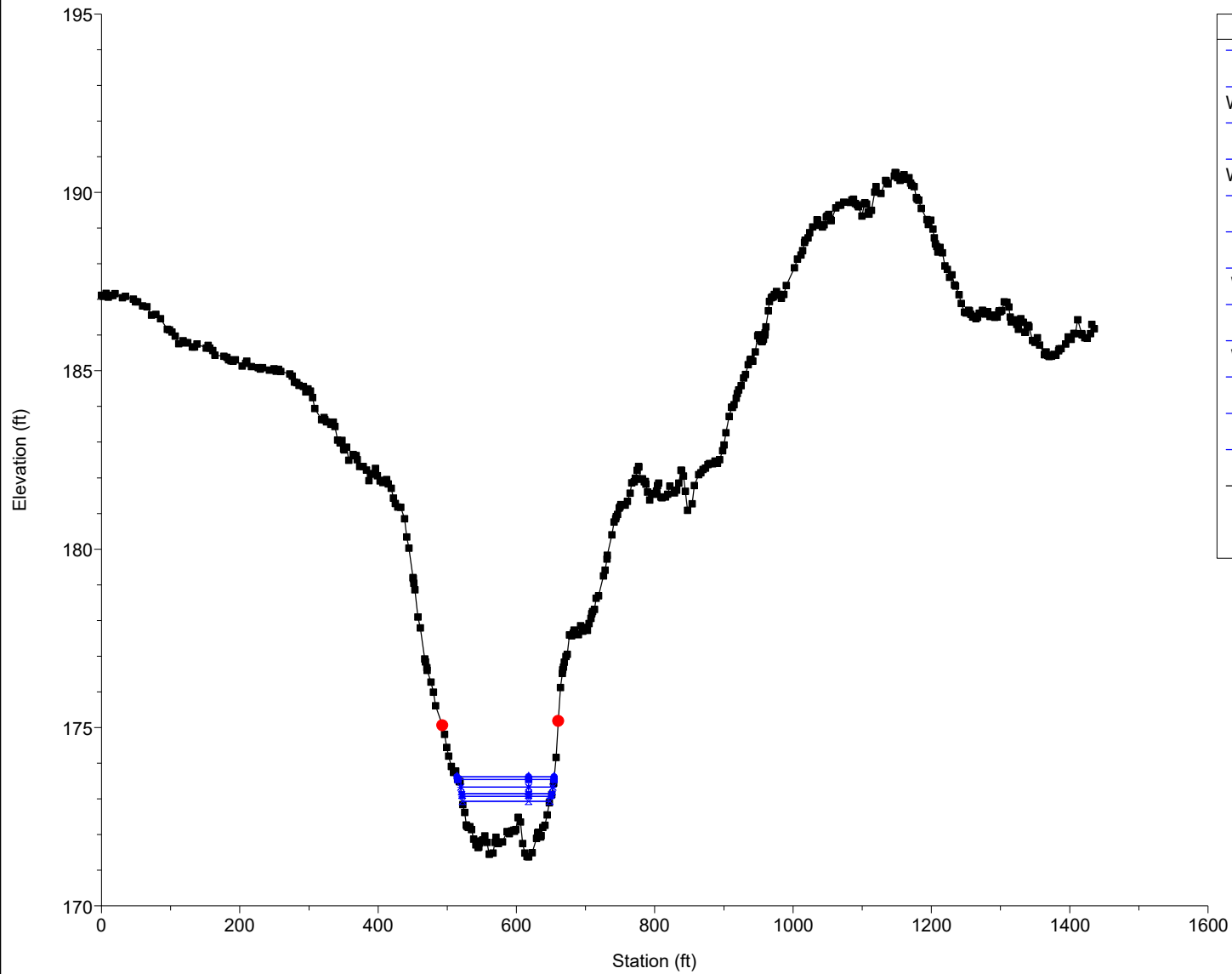


Legend	
WS 100 yr_2100 - Exist	●
WS 100 yr_2100 - 72inRCP	▲
WS 100 yr_2050 - Exist	■
WS 100 yr_2050 - 72inRCP	✱
WS 100 yr - 72inRCP	✕
WS 100 yr - Exist	✱
WS 25 yr_2100 - 72inRCP	▼
WS 25 yr_2100 - Exist	+
WS 25 yr_2050 - 72inRCP	▲
WS 25 yr_2050 - Exist	+
WS 25 yr - Exist	✕
WS 25 yr - 72inRCP	■
Ground	■
Bank Sta	●

Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 7056

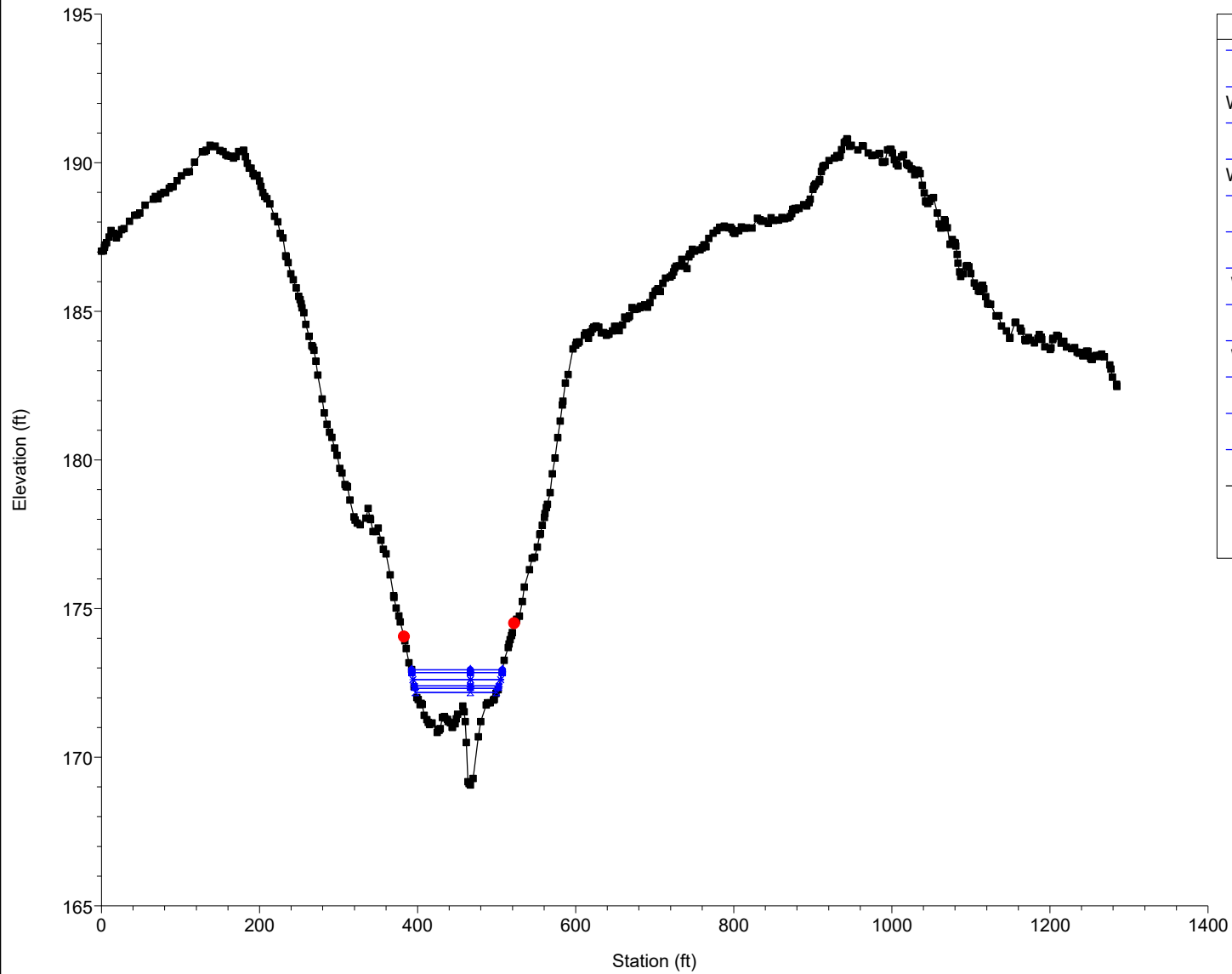


Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 6826

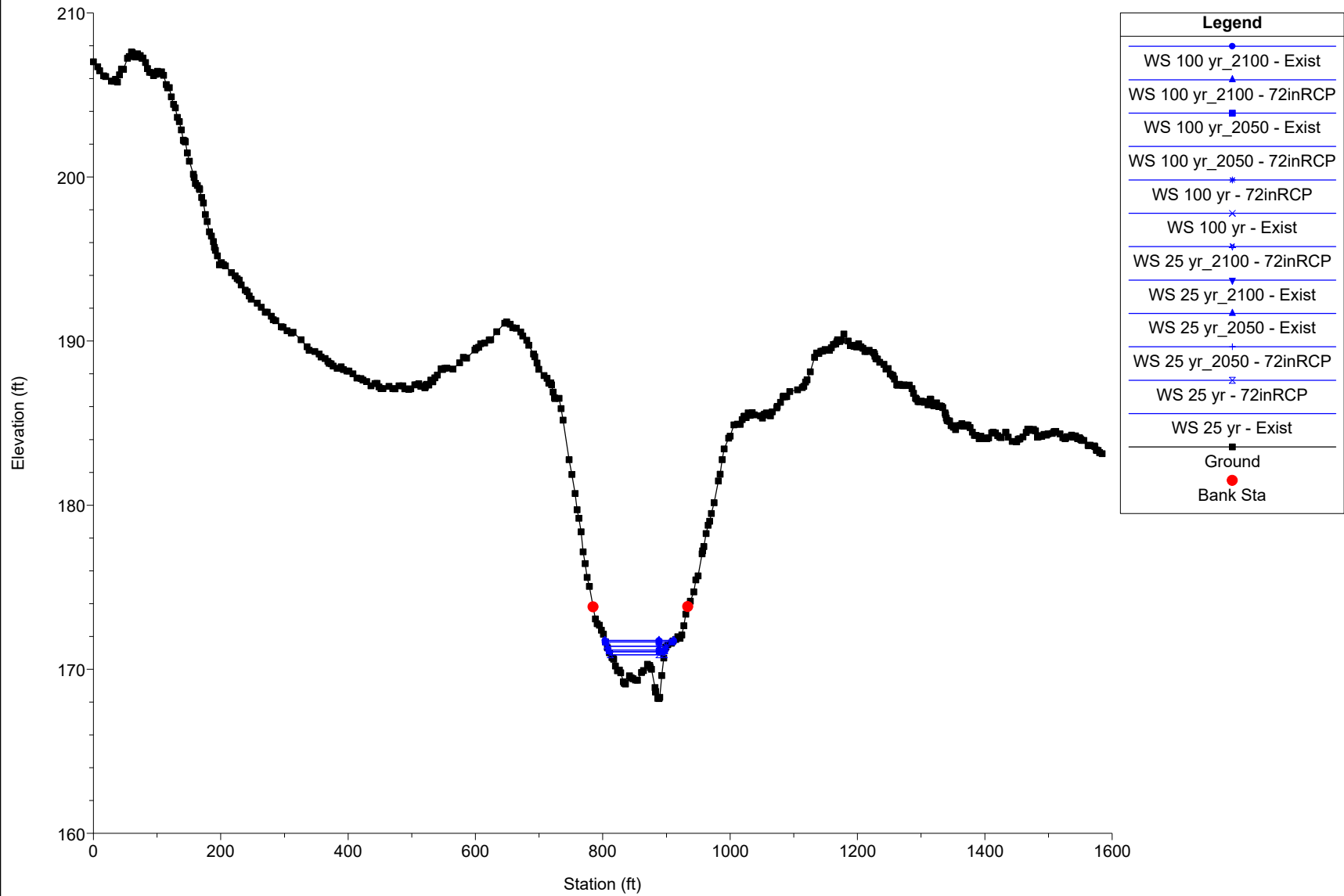


Legend	
WS 100 yr_2100 - Exist	●
WS 100 yr_2100 - 72inRCP	▲
WS 100 yr_2050 - Exist	■
WS 100 yr_2050 - 72inRCP	✱
WS 100 yr - 72inRCP	✱
WS 100 yr - Exist	✱
WS 25 yr_2100 - 72inRCP	✱
WS 25 yr_2100 - Exist	▼
WS 25 yr_2050 - 72inRCP	+
WS 25 yr_2050 - Exist	▲
WS 25 yr - Exist	✱
WS 25 yr - 72inRCP	✱
Ground	■
Bank Sta	●

Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 6654

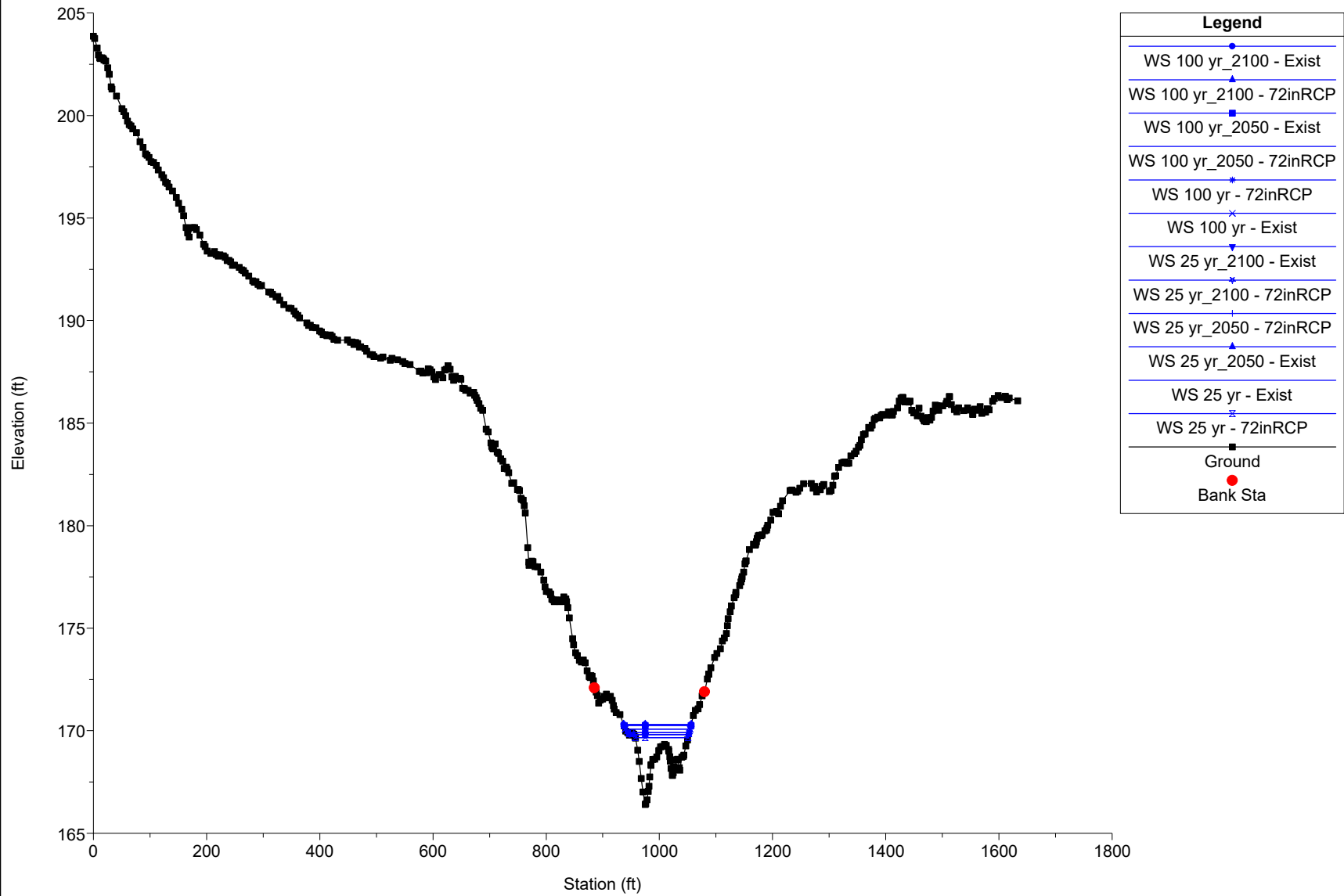


Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 6360



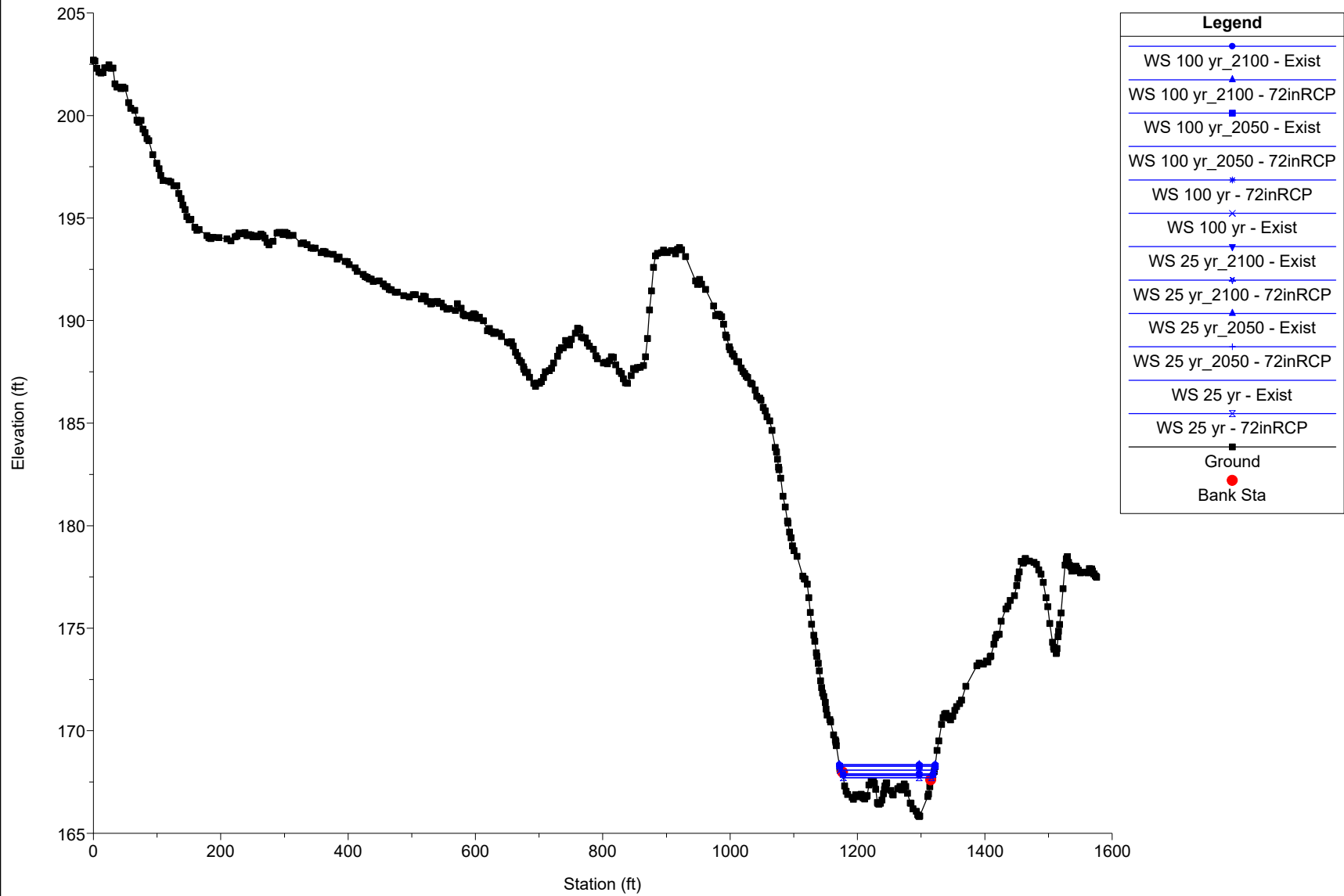
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 6034



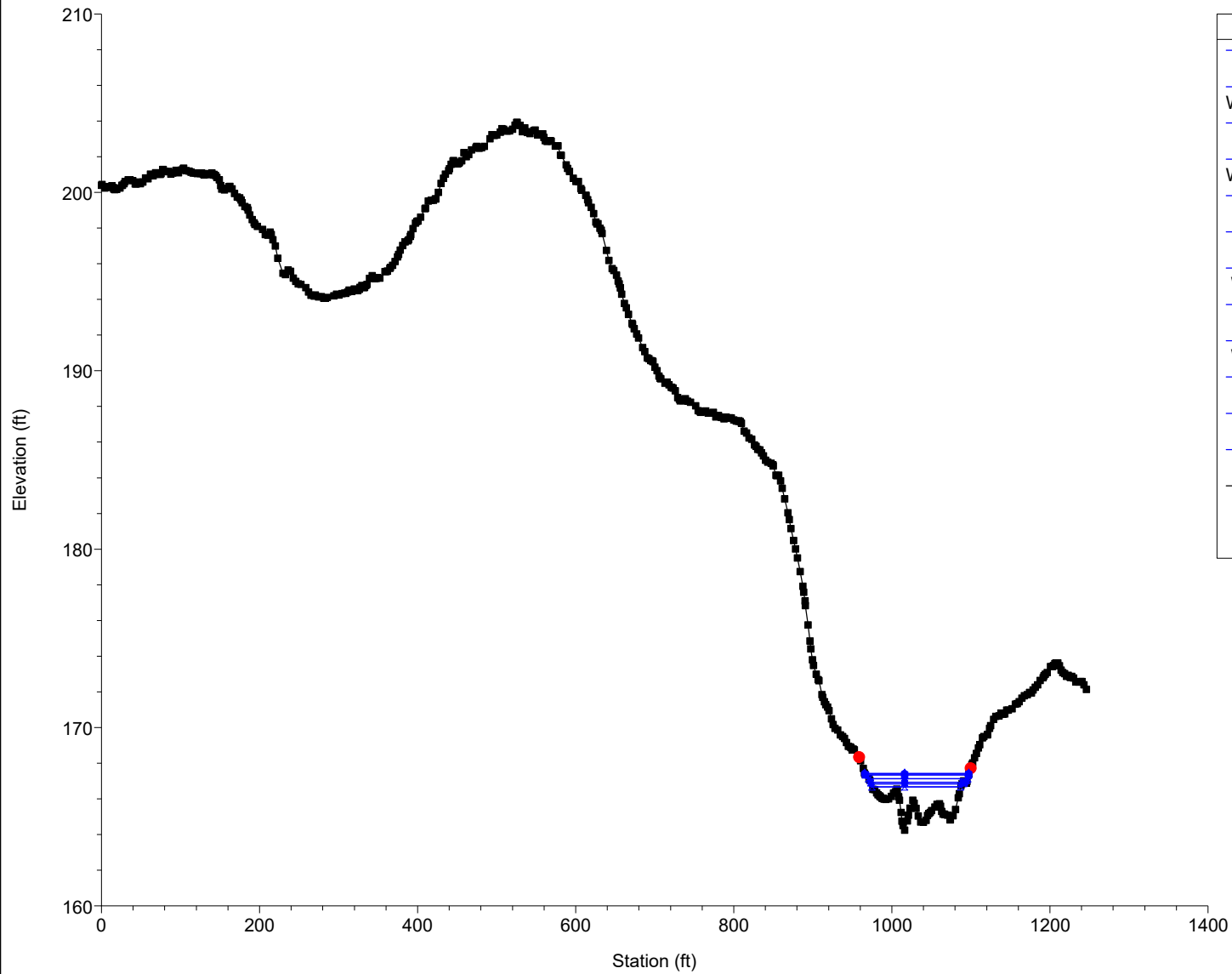
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 5576



Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 5302

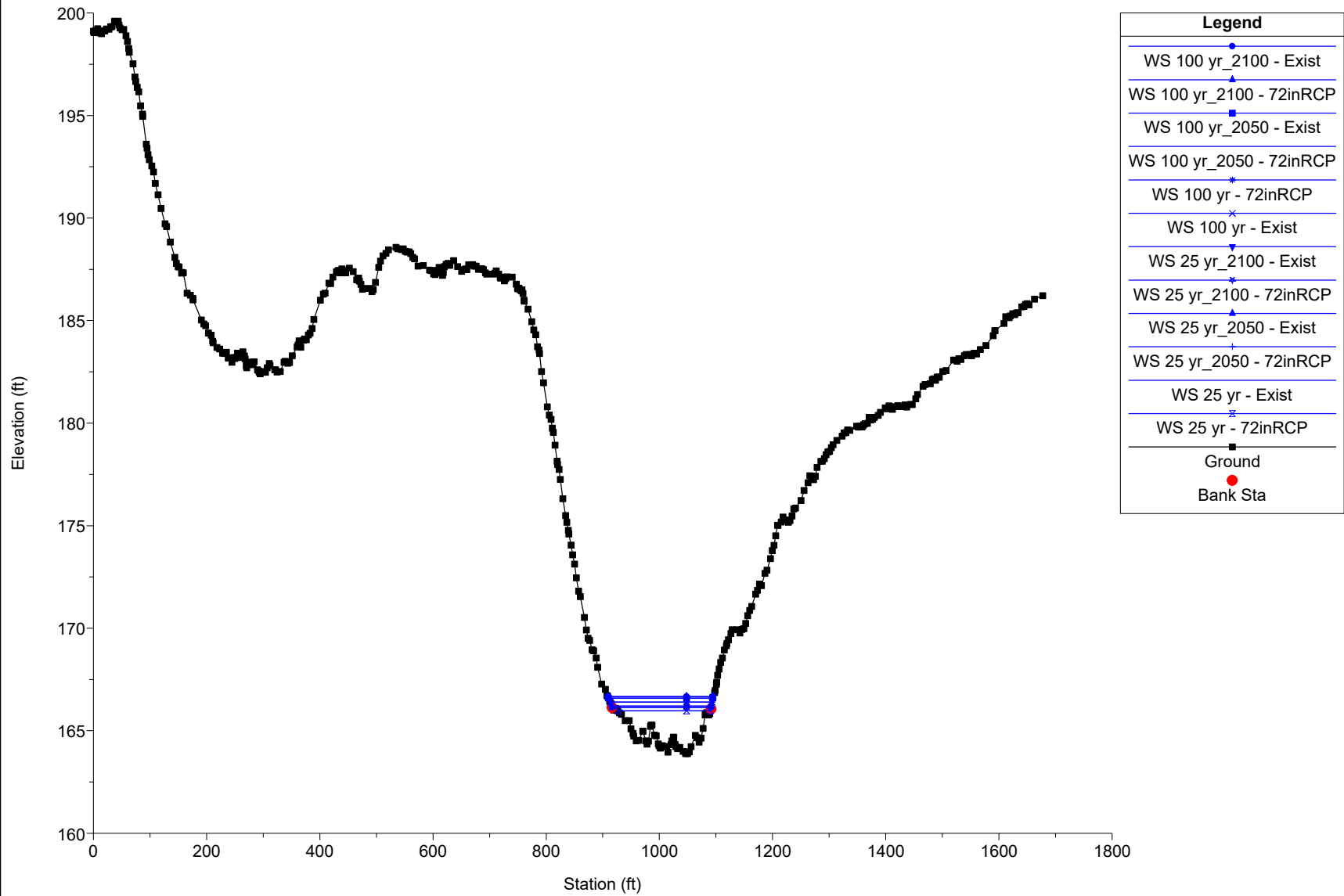


Legend

- WS 100 yr_2100 - Exist
- WS 100 yr_2100 - 72inRCP
- WS 100 yr_2050 - Exist
- WS 100 yr_2050 - 72inRCP
- WS 100 yr - 72inRCP
- WS 100 yr - Exist
- WS 25 yr_2100 - 72inRCP
- WS 25 yr_2100 - Exist
- WS 25 yr_2050 - 72inRCP
- WS 25 yr_2050 - Exist
- WS 25 yr - 72inRCP
- WS 25 yr - Exist
- Ground
- Bank Sta

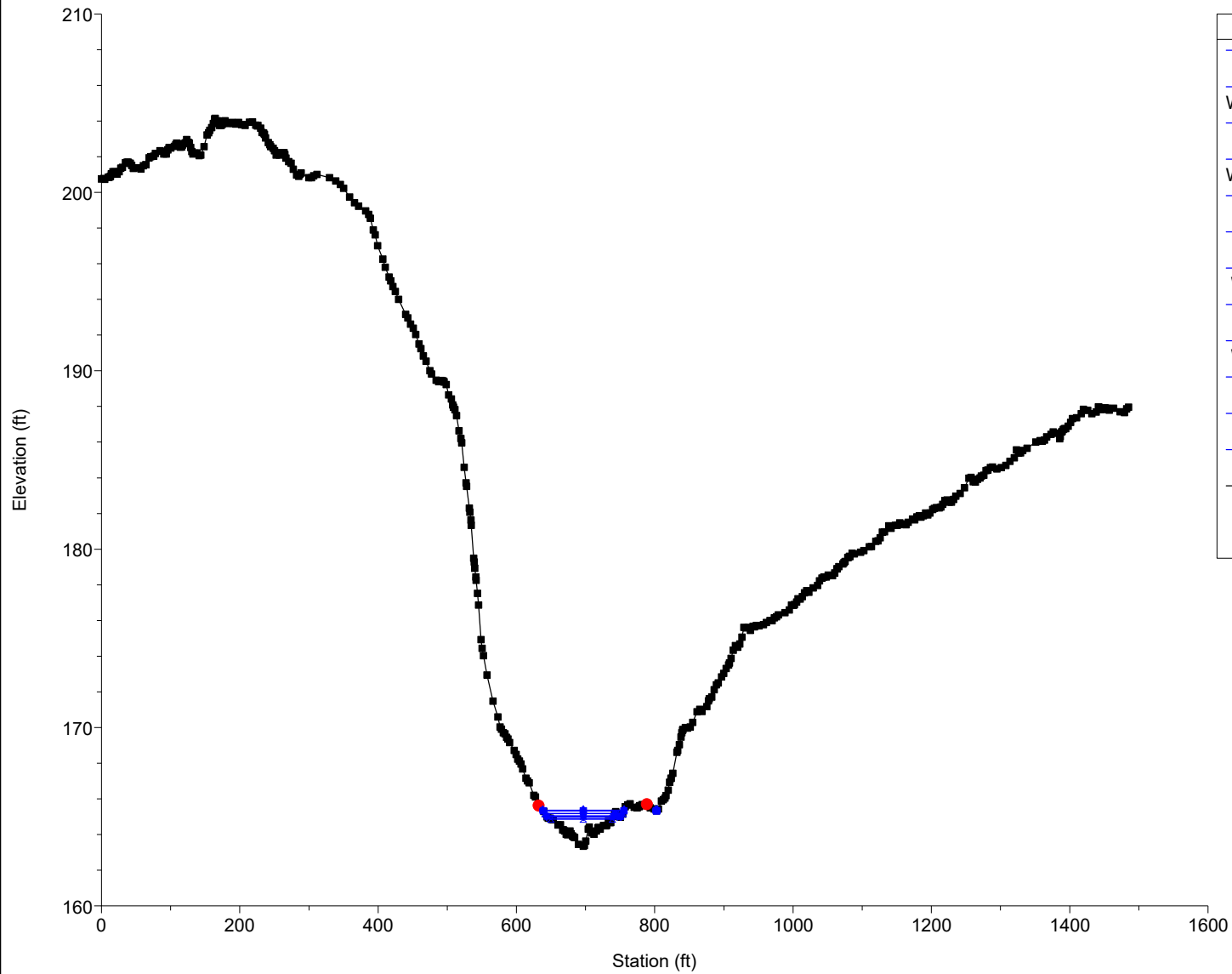
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 4848



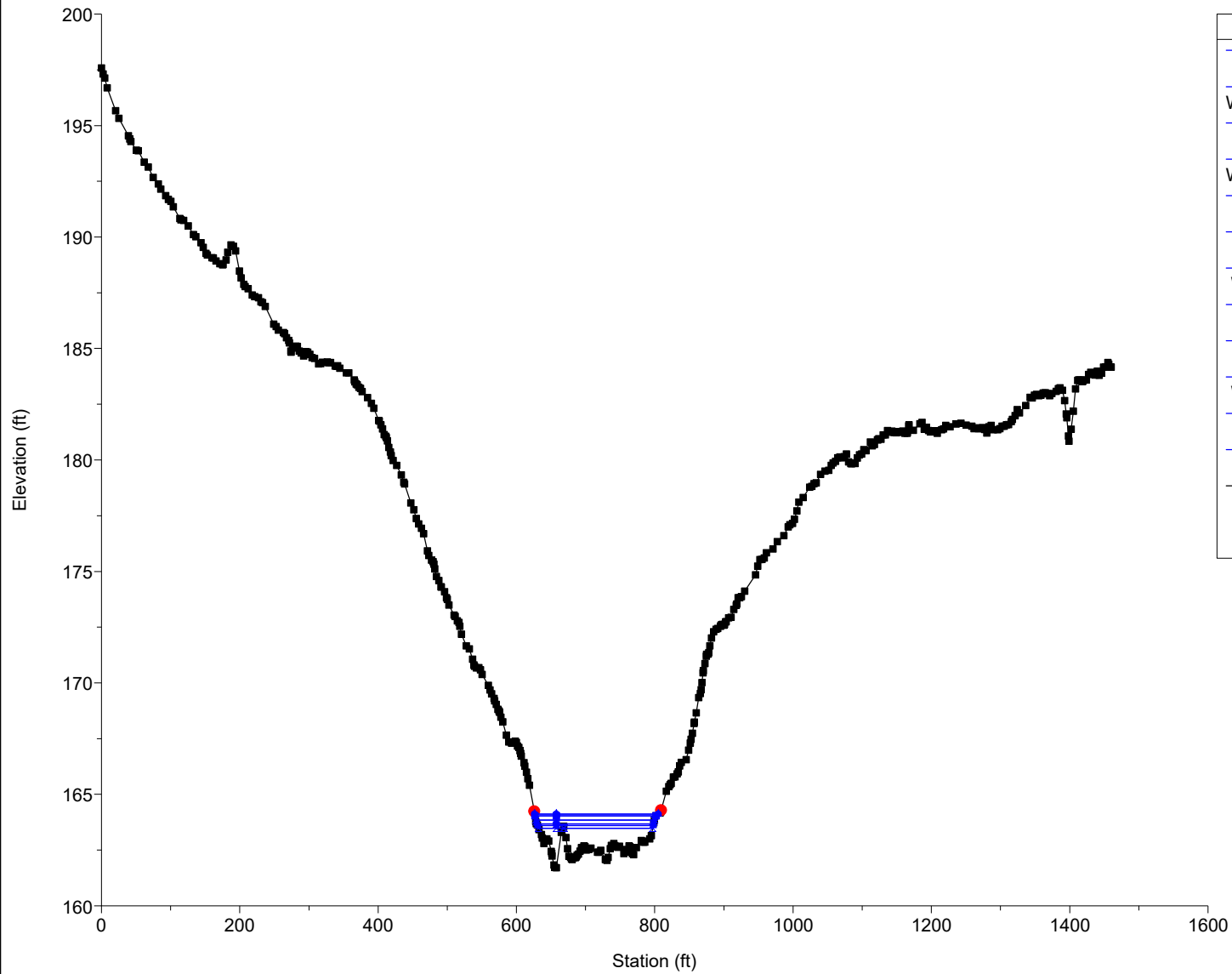
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 4582



Poplar Hill Rd

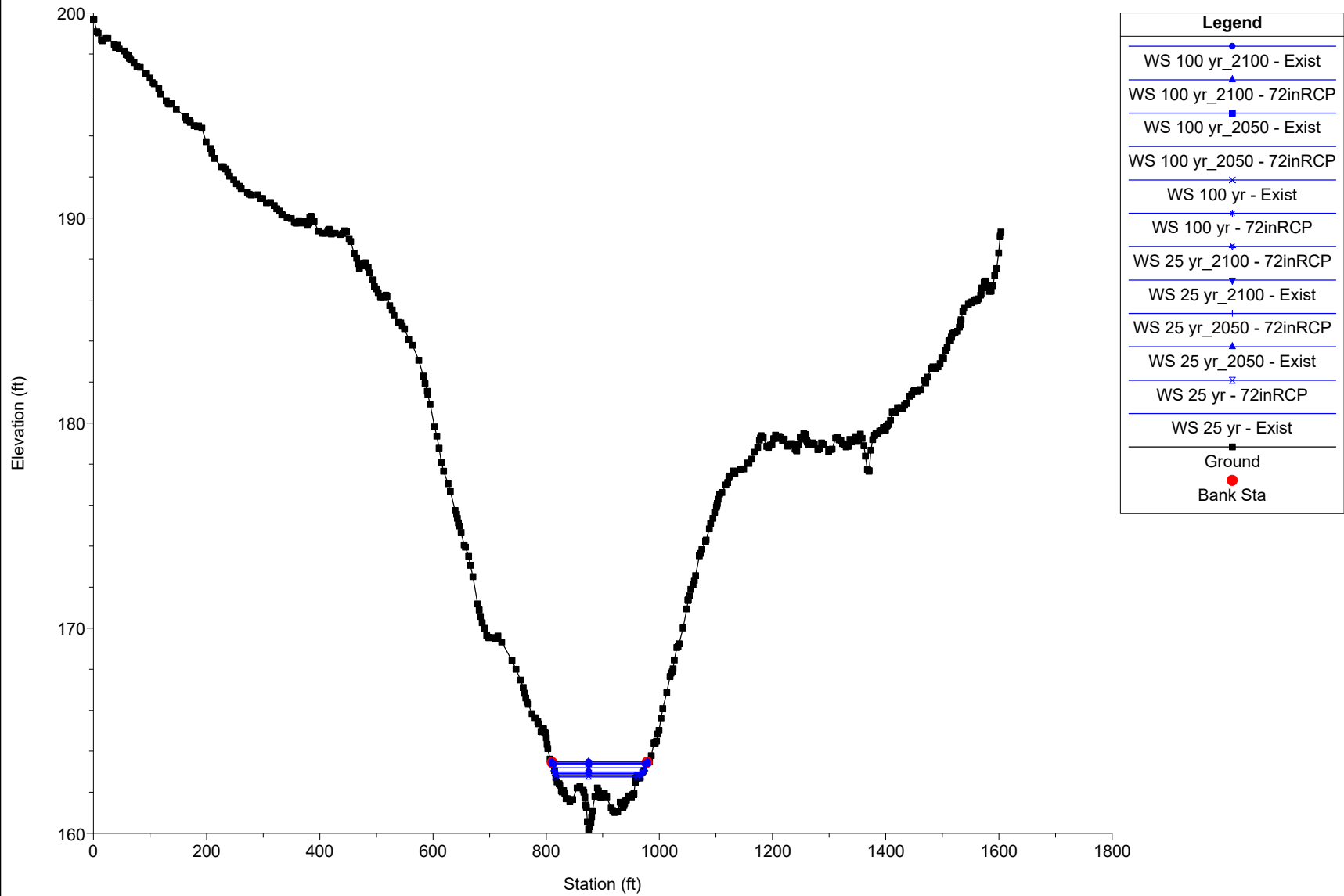
River = Zekiah Swamp Reach = Poplar Hill Road RS = 4355



Legend

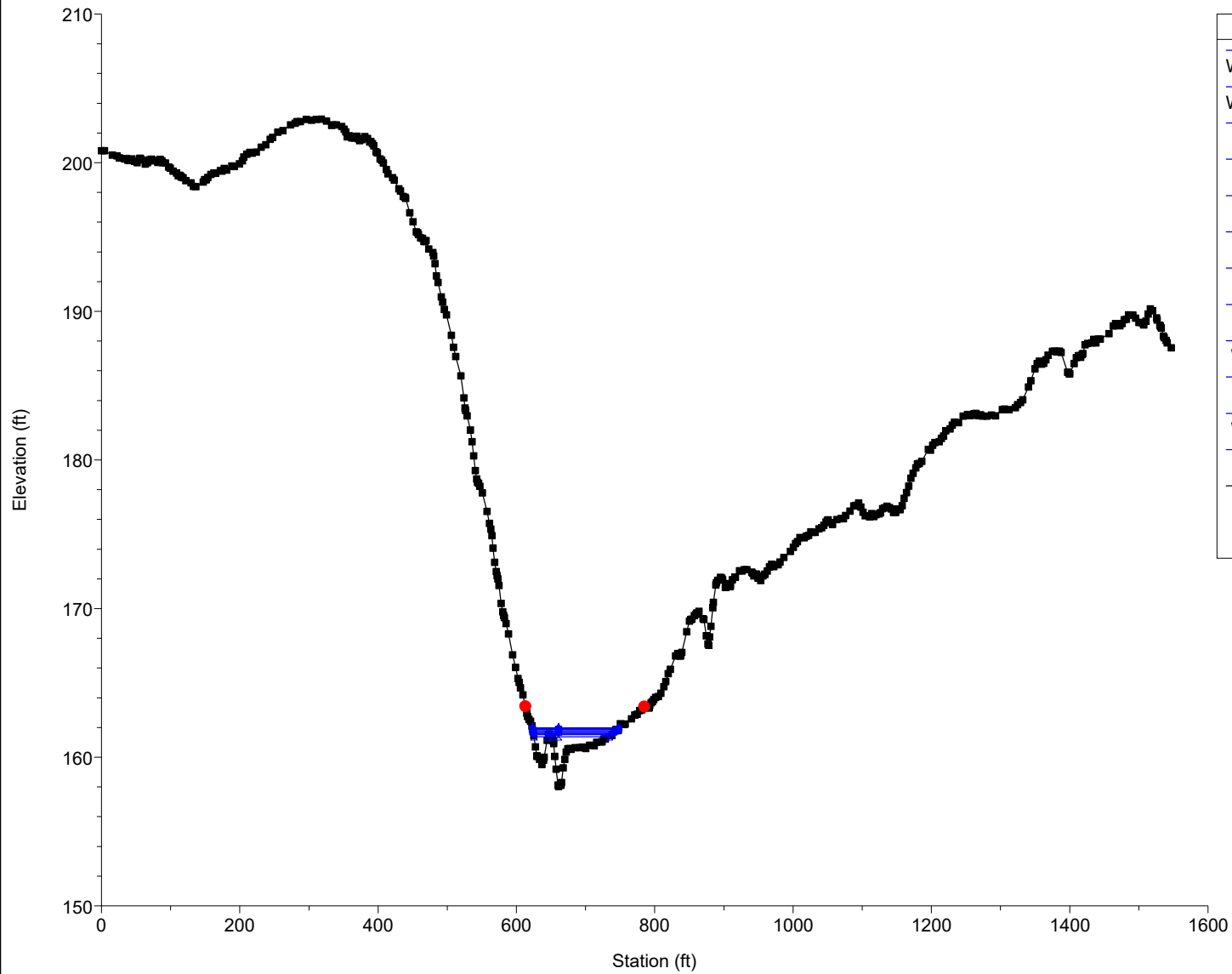
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- WS 100 yr_2100 - 72inRCP
- WS 100 yr_2050 - Exist
- WS 100 yr_2050 - 72inRCP
- WS 100 yr - Exist
- WS 100 yr - 72inRCP
- WS 25 yr_2100 - 72inRCP
- WS 25 yr_2100 - Exist
- WS 25 yr_2050 - Exist
- WS 25 yr_2050 - 72inRCP
- WS 25 yr - Exist
- WS 25 yr - 72inRCP
- Ground
- Bank Sta

Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 4087

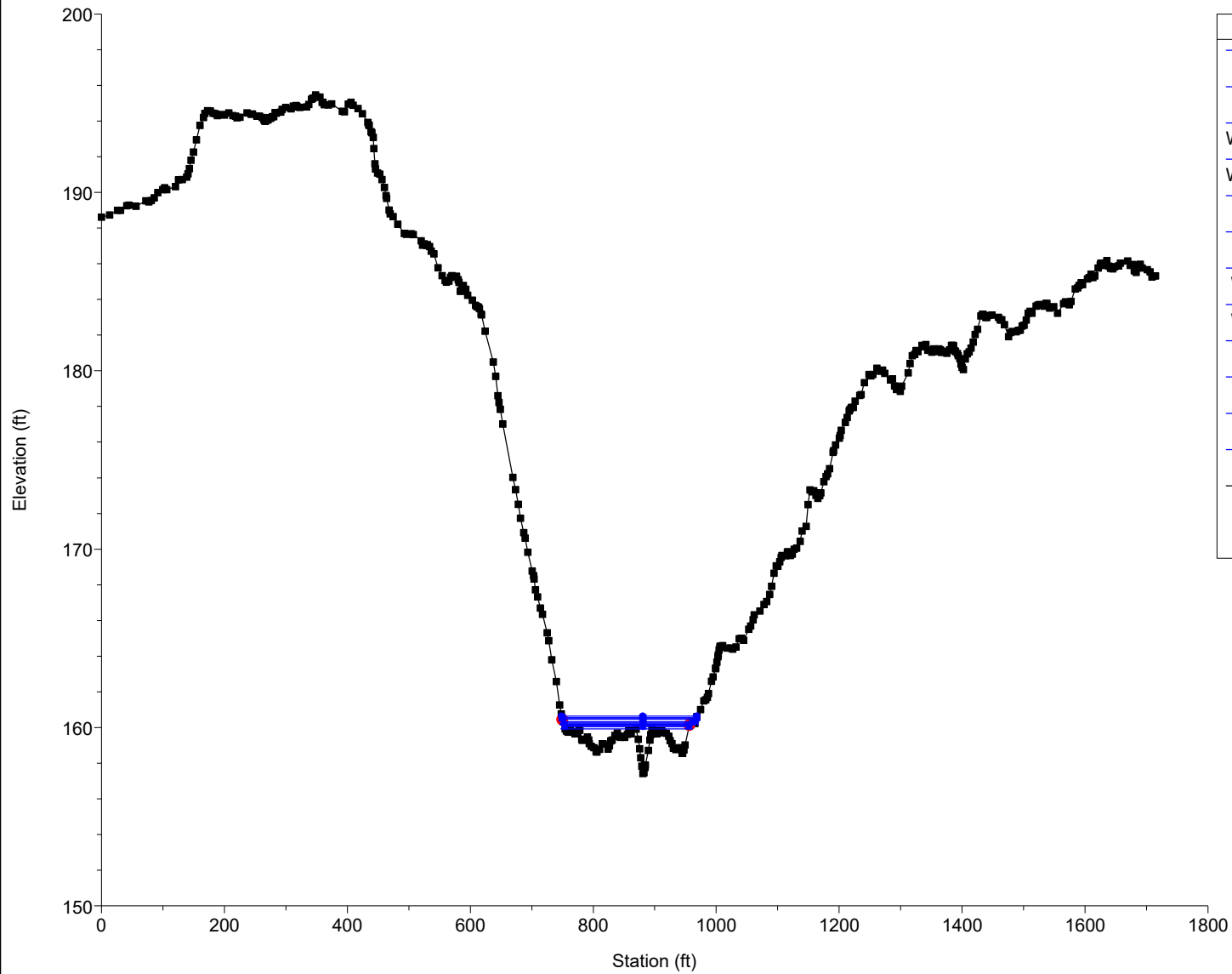


Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 3698

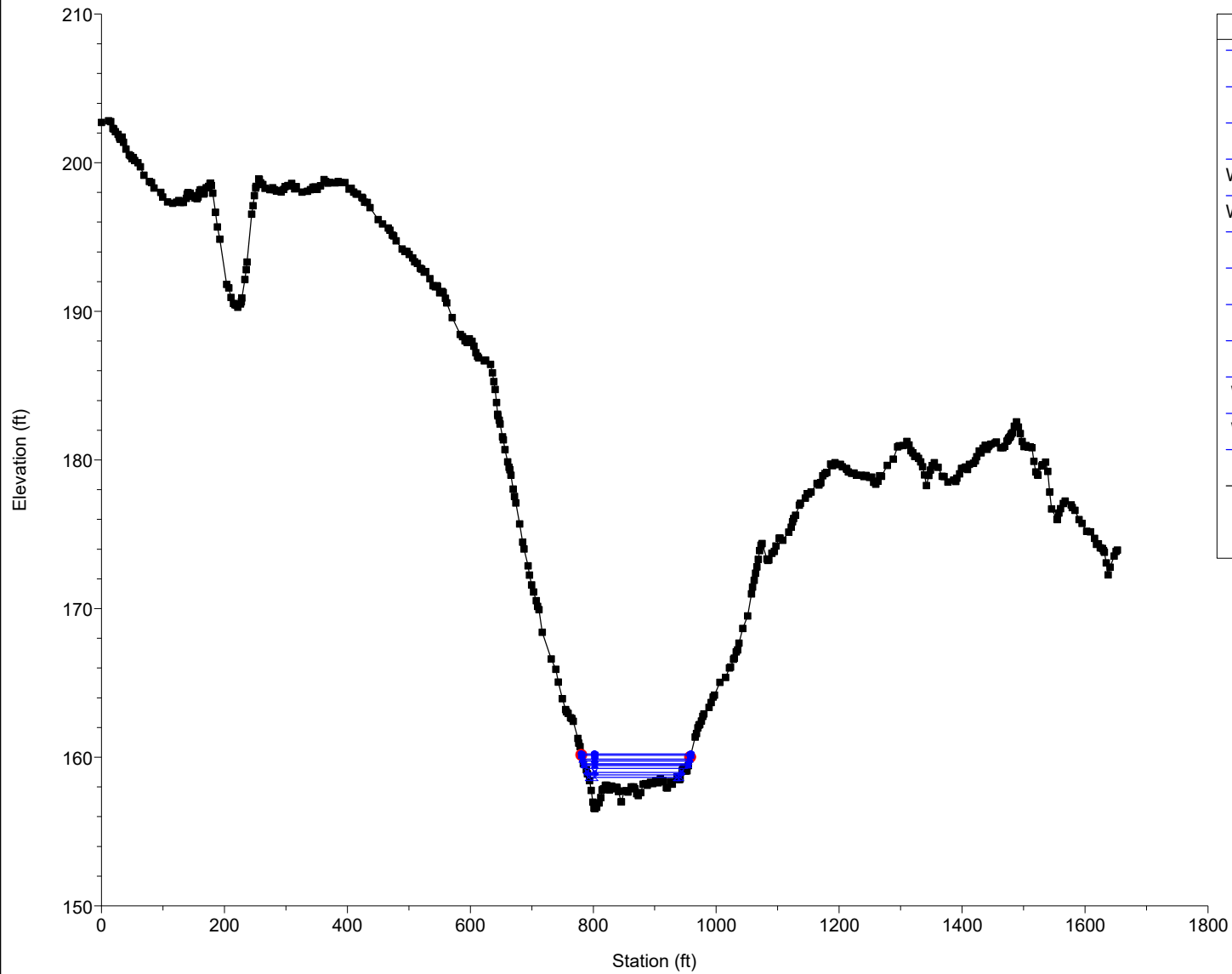


Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 3358



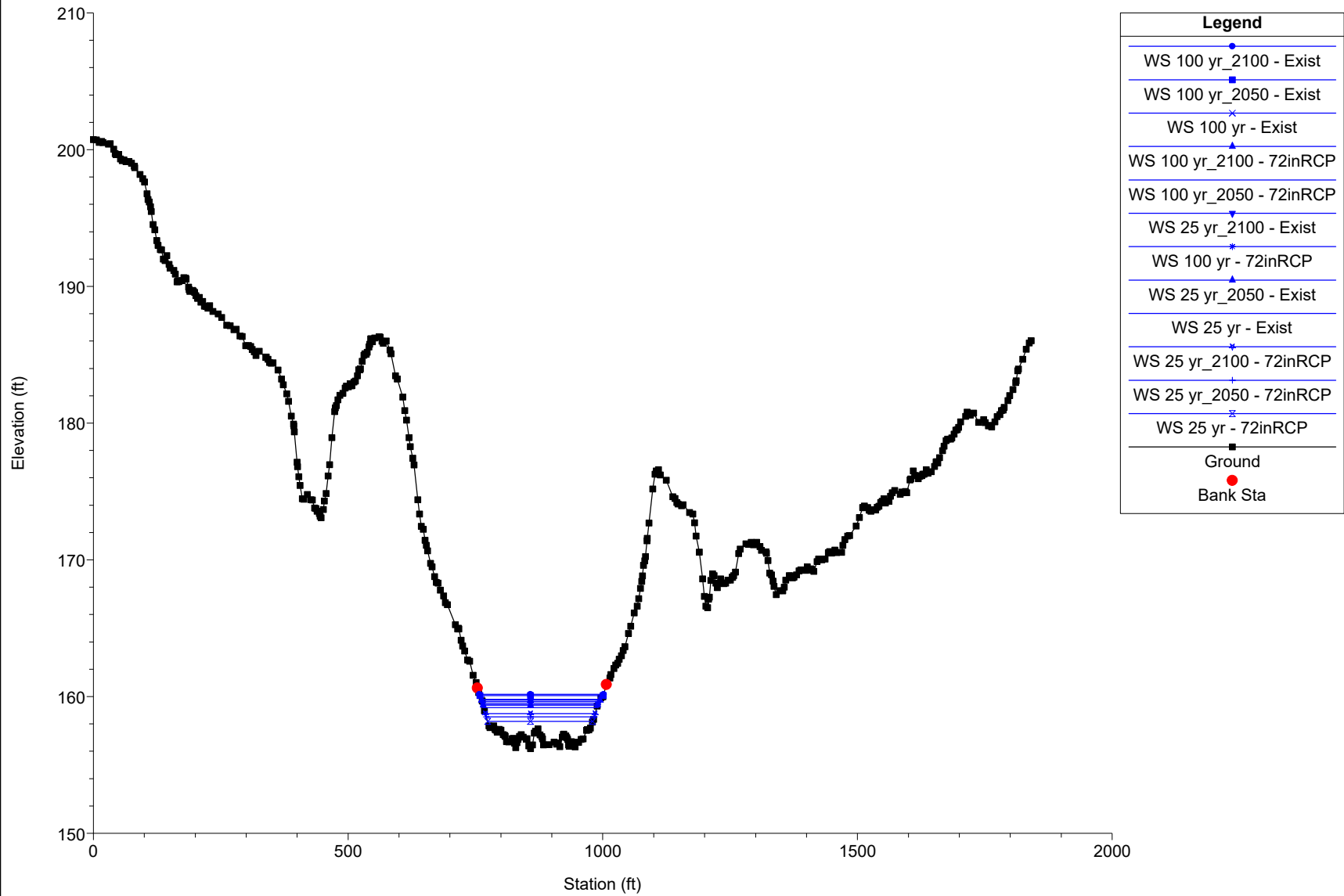
Legend	
WS 100 yr_2100 - Exist	▲
WS 100 yr_2050 - Exist	■
WS 100 yr_2100 - 72inRCP	▲
WS 100 yr_2050 - 72inRCP	▲
WS 100 yr - Exist	×
WS 100 yr - 72inRCP	×
WS 25 yr_2100 - 72inRCP	×
WS 25 yr_2050 - 72inRCP	×
WS 25 yr_2100 - Exist	▲
WS 25 yr - 72inRCP	×
WS 25 yr_2050 - Exist	▲
WS 25 yr - Exist	■
Ground	■
Bank Sta	●

Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 3017



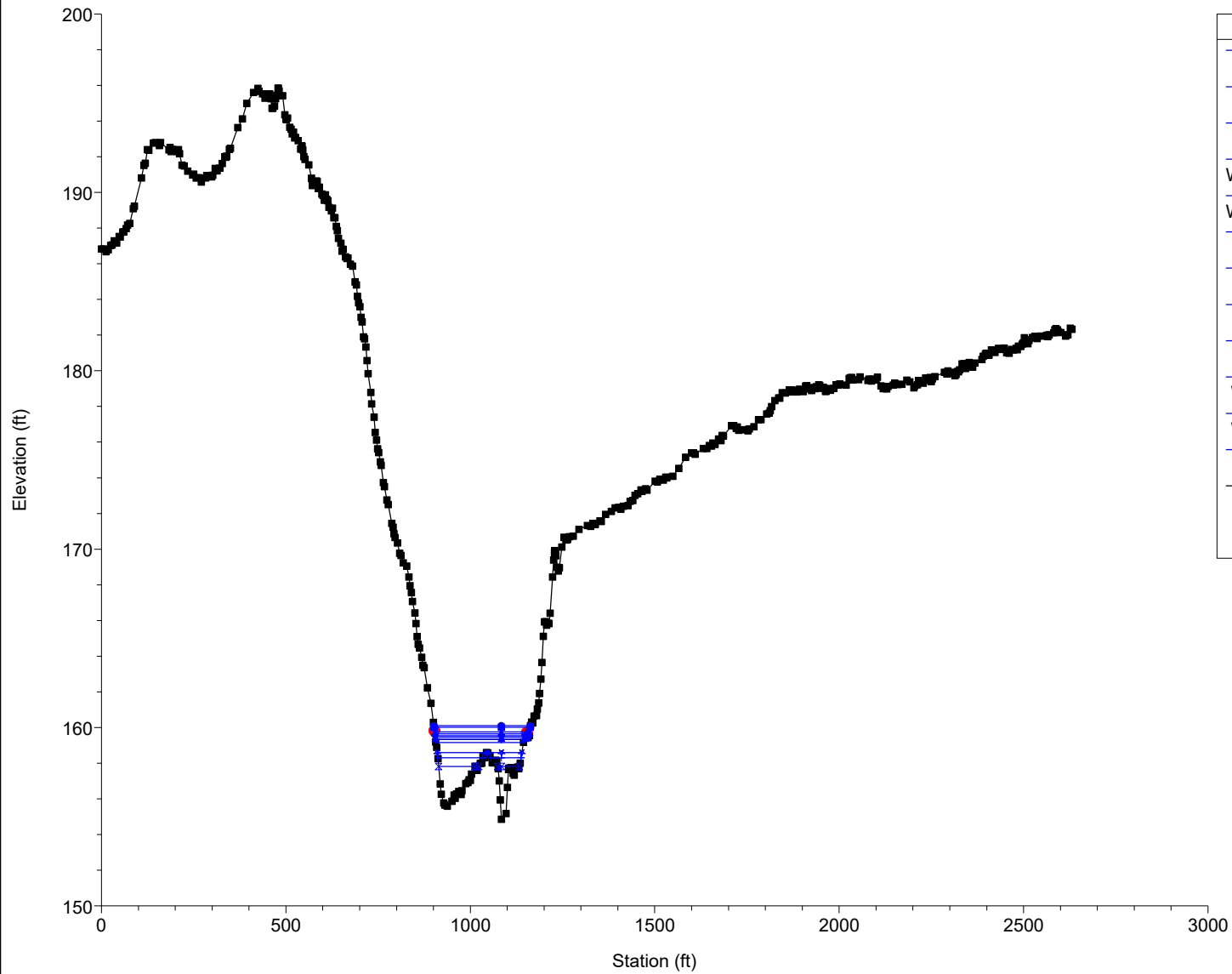
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 2708



Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 2305

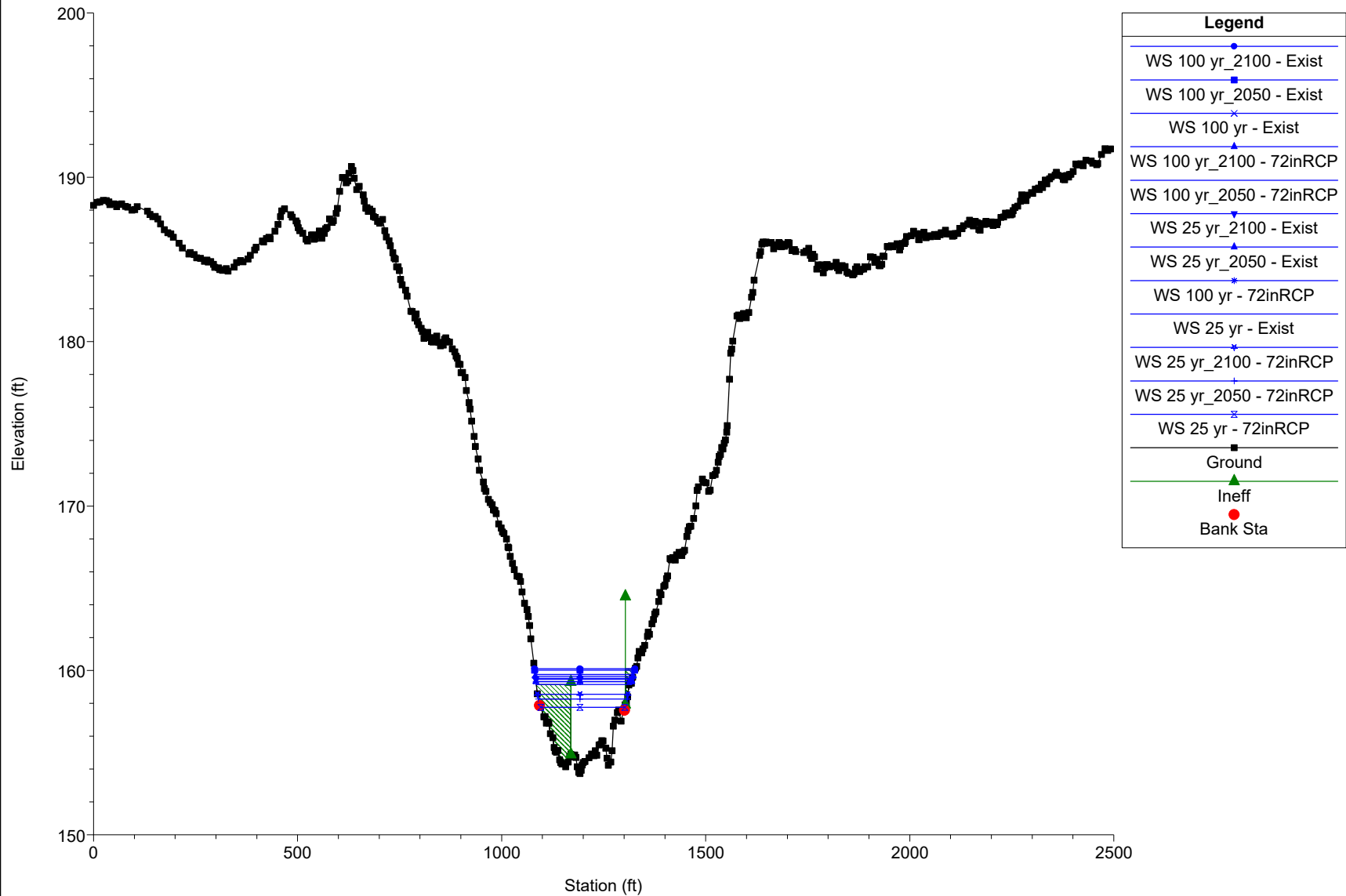


Legend

- WS 100 yr_2100 - Exist
- WS 100 yr_2050 - Exist
- WS 100 yr - Exist
- WS 100 yr_2100 - 72inRCP
- WS 100 yr_2050 - 72inRCP
- WS 25 yr_2100 - Exist
- WS 25 yr_2050 - Exist
- WS 100 yr - 72inRCP
- WS 25 yr - Exist
- WS 25 yr_2100 - 72inRCP
- WS 25 yr_2050 - 72inRCP
- WS 25 yr - 72inRCP
- Ground
- Bank Sta

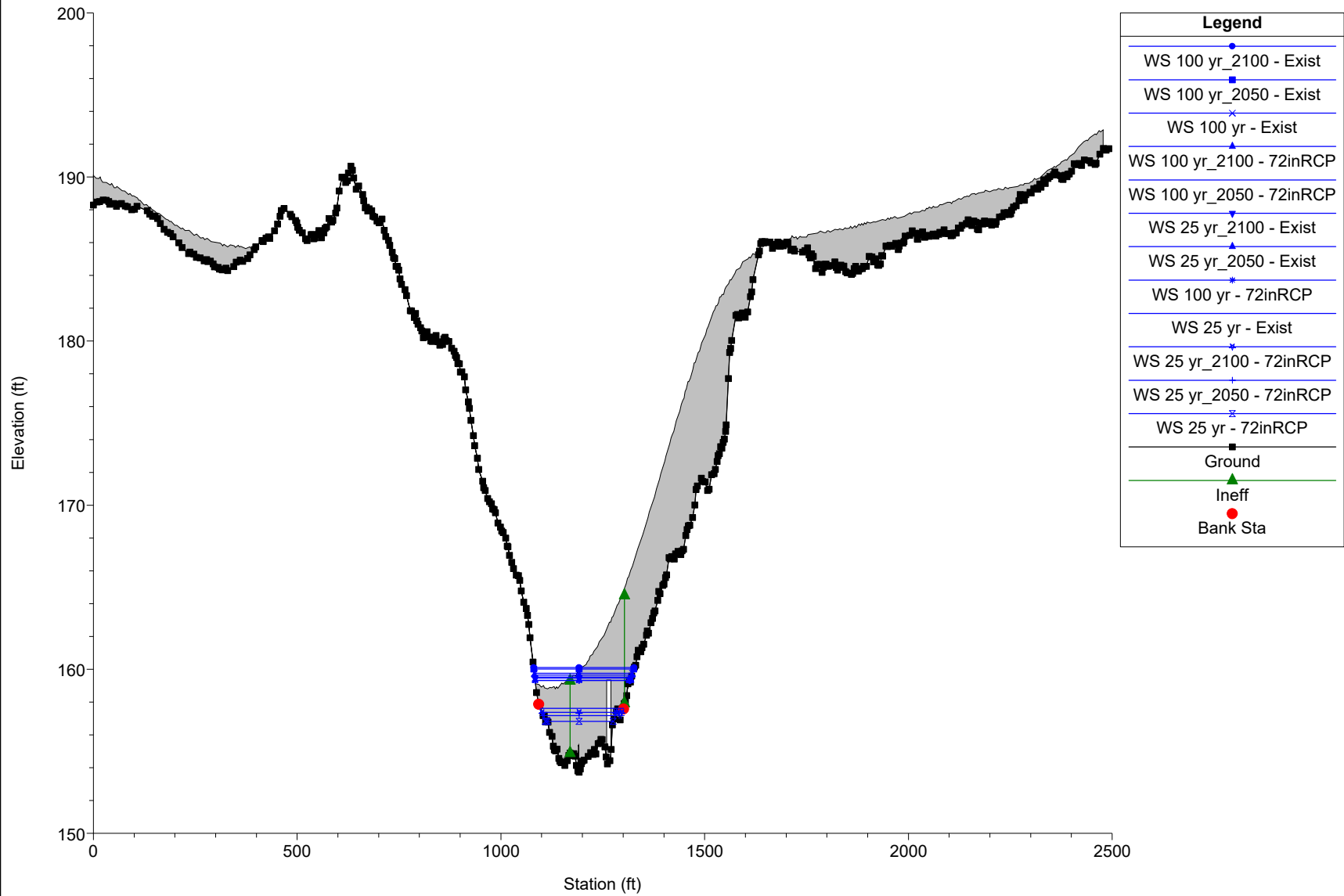
Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 2119

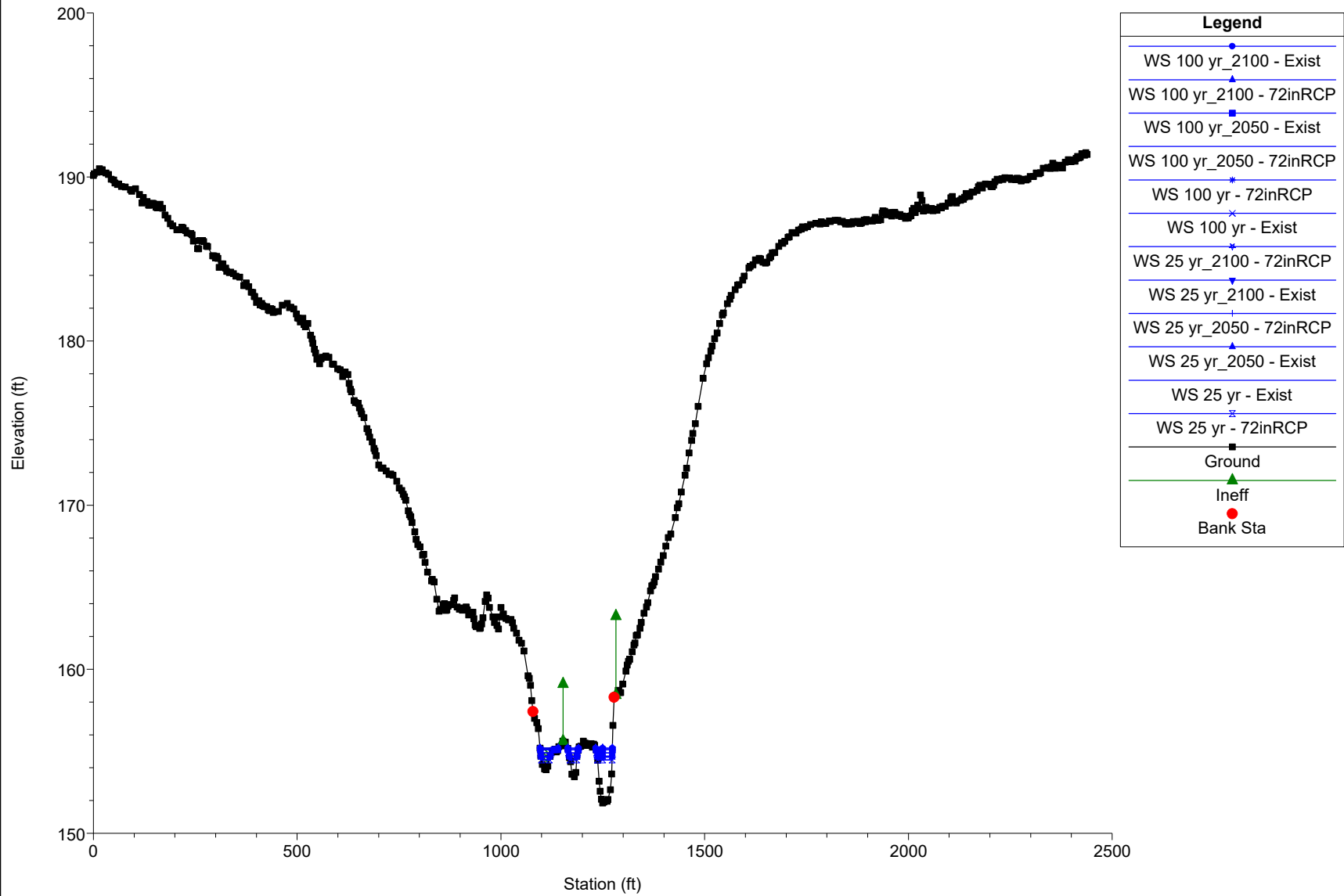


Poplar Hill Rd

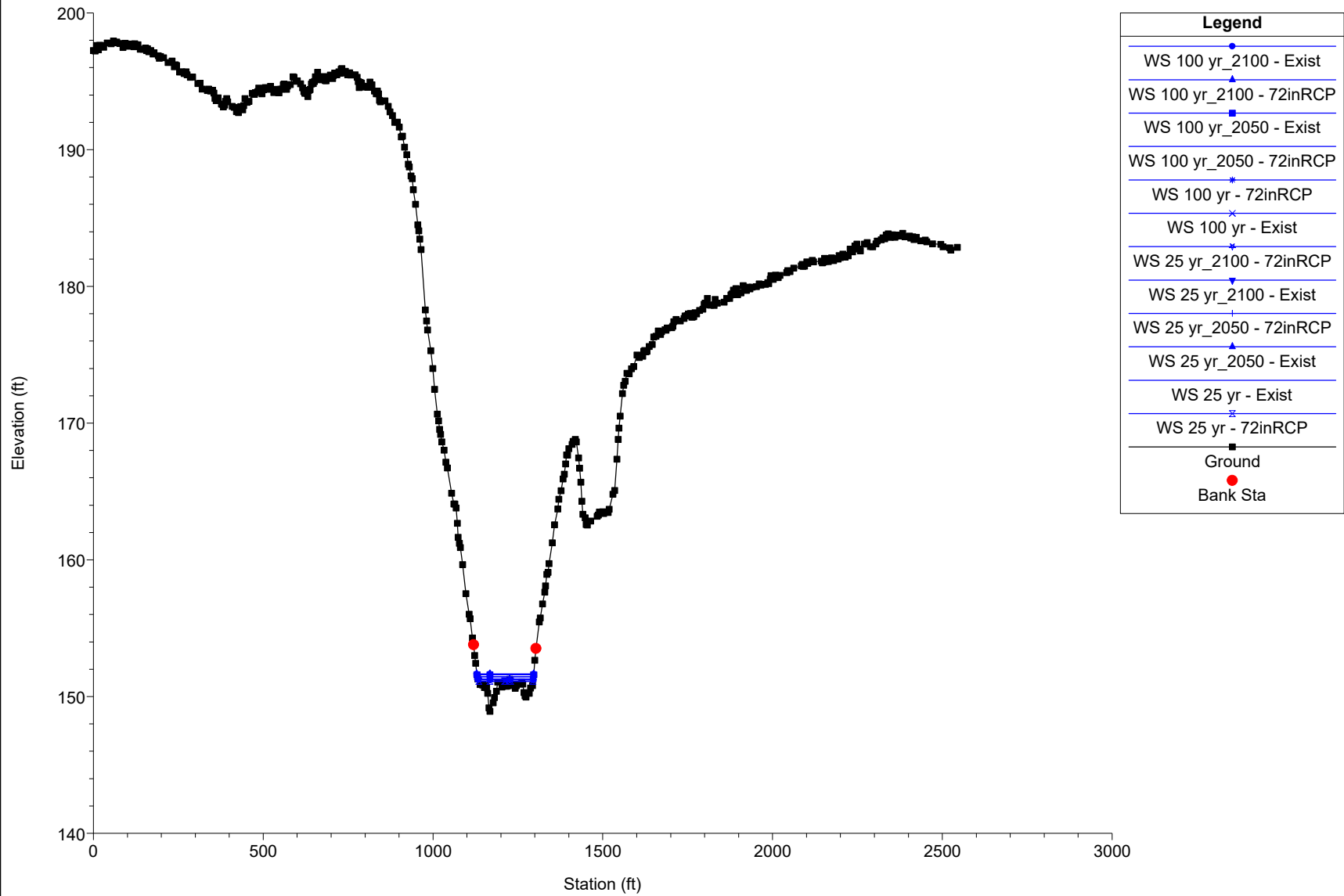
River = Zekiah Swamp Reach = Poplar Hill Road RS = 2085 Culv Poplar Hill Road



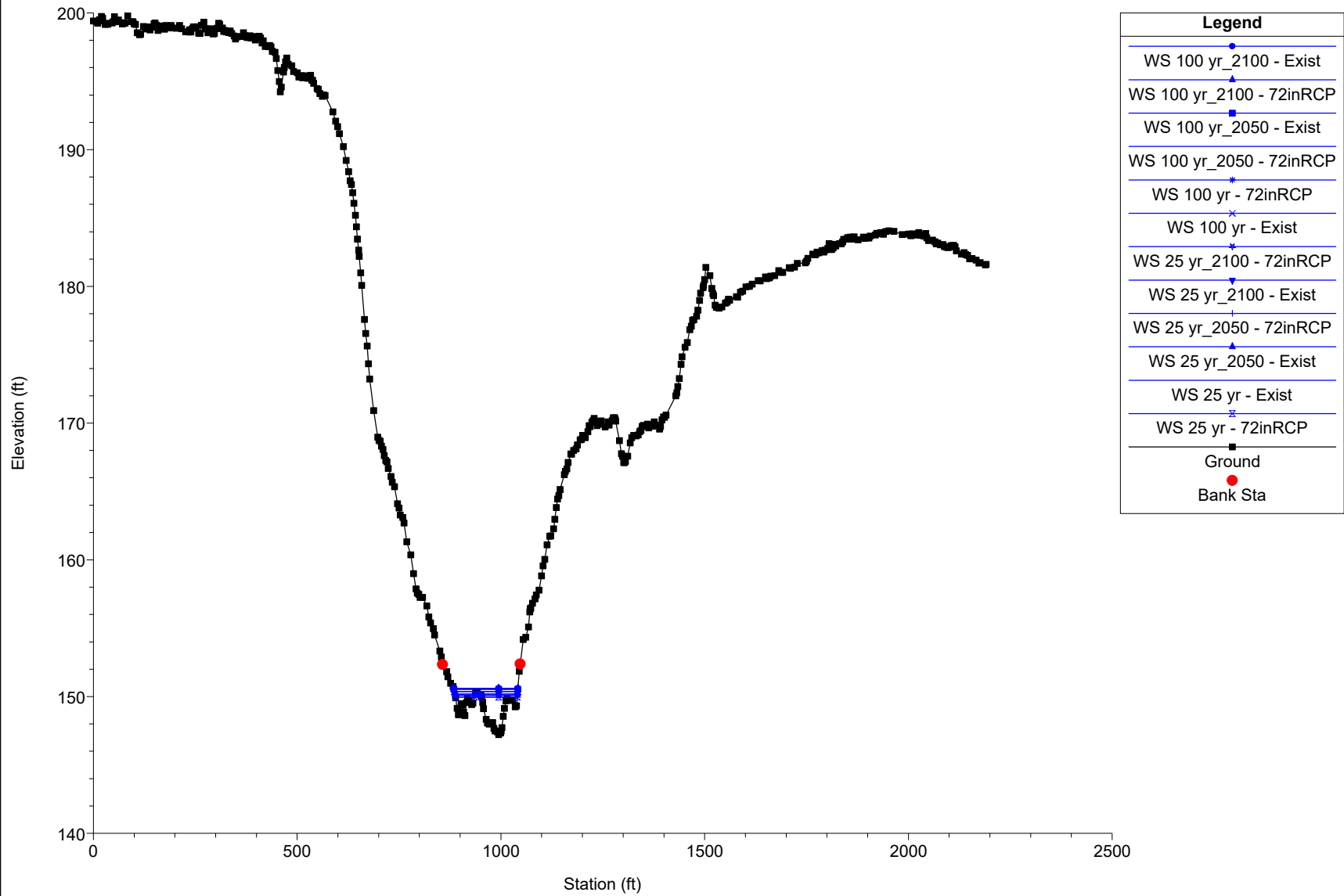
Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 2040



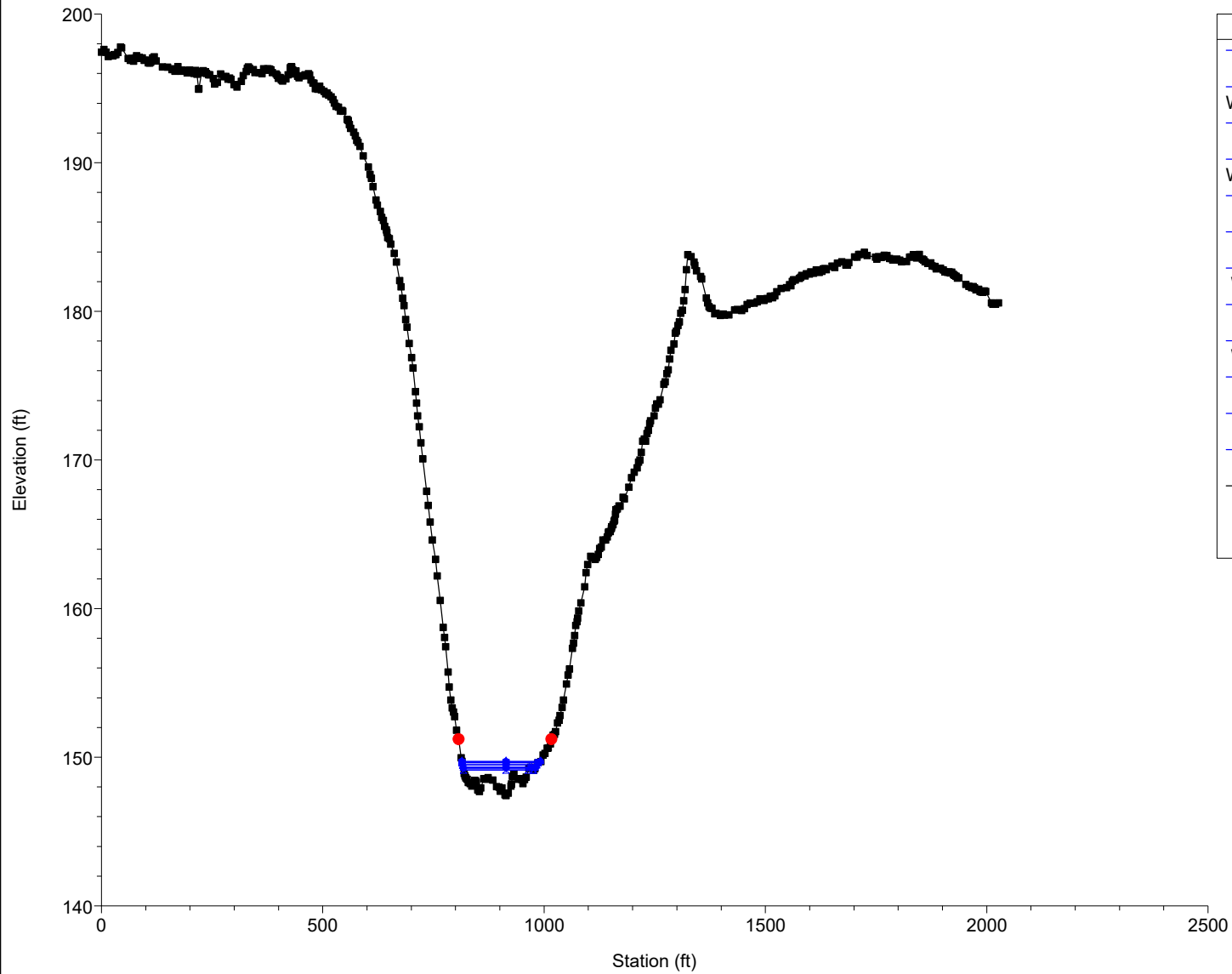
Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 1606



Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 1360



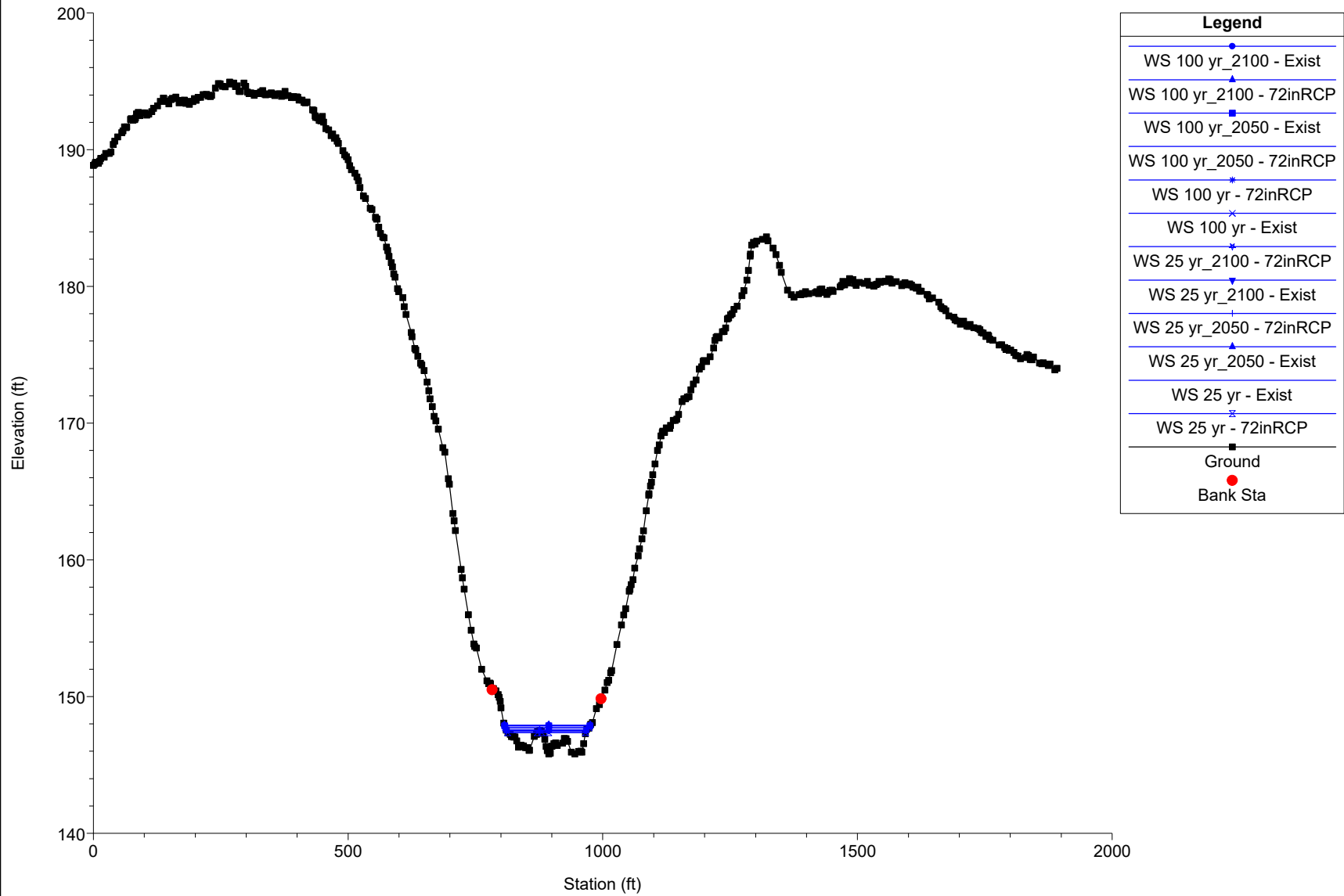
Poplar Hill Rd
River = Zekiah Swamp Reach = Poplar Hill Road RS = 1109



Legend	
WS 100 yr_2100 - Exist	●
WS 100 yr_2100 - 72inRCP	▲
WS 100 yr_2050 - Exist	■
WS 100 yr_2050 - 72inRCP	*
WS 100 yr - 72inRCP	×
WS 100 yr - Exist	+
WS 25 yr_2100 - 72inRCP	▼
WS 25 yr_2100 - Exist	+
WS 25 yr_2050 - 72inRCP	▲
WS 25 yr_2050 - Exist	+
WS 25 yr - Exist	×
WS 25 yr - 72inRCP	■
Ground	■
Bank Sta	●

Poplar Hill Rd

River = Zekiah Swamp Reach = Poplar Hill Road RS = 722



HEC-RAS River: Zekiah Swamp Reach: Poplar Hill Road

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Poplar Hill Road	7881	25 yr	Exist	281.00	176.25	178.04		178.16	0.005162	2.70	104.13	102.14	0.47
Poplar Hill Road	7881	25 yr	72inRCP	281.00	176.25	178.04		178.16	0.005162	2.70	104.13	102.14	0.47
Poplar Hill Road	7881	25 yr_2050	Exist	339.00	176.25	178.18		178.31	0.005082	2.86	118.56	105.38	0.48
Poplar Hill Road	7881	25 yr_2050	72inRCP	339.00	176.25	178.18		178.31	0.005082	2.86	118.56	105.38	0.48
Poplar Hill Road	7881	25 yr_2100	Exist	374.00	176.25	178.26		178.39	0.005066	2.95	126.73	107.17	0.48
Poplar Hill Road	7881	25 yr_2100	72inRCP	374.00	176.25	178.26		178.39	0.005066	2.95	126.73	107.17	0.48
Poplar Hill Road	7881	100 yr	Exist	469.00	176.25	178.48		178.63	0.005182	3.07	152.75	123.86	0.49
Poplar Hill Road	7881	100 yr	72inRCP	469.00	176.25	178.48		178.63	0.005182	3.07	152.75	123.86	0.49
Poplar Hill Road	7881	100 yr_2050	Exist	578.00	176.25	178.68		178.84	0.005186	3.26	177.45	131.72	0.49
Poplar Hill Road	7881	100 yr_2050	72inRCP	578.00	176.25	178.68		178.84	0.005186	3.26	177.45	131.72	0.49
Poplar Hill Road	7881	100 yr_2100	Exist	622.00	176.25	178.77		178.93	0.005240	3.28	189.57	140.29	0.50
Poplar Hill Road	7881	100 yr_2100	72inRCP	622.00	176.25	178.77		178.93	0.005240	3.28	189.57	140.29	0.50
Poplar Hill Road	7596	25 yr	Exist	281.00	173.63	176.78		176.87	0.003944	2.37	118.51	114.81	0.41
Poplar Hill Road	7596	25 yr	72inRCP	281.00	173.63	176.78		176.87	0.003944	2.37	118.51	114.81	0.41
Poplar Hill Road	7596	25 yr_2050	Exist	339.00	173.63	176.90		177.00	0.004116	2.58	131.54	116.10	0.43
Poplar Hill Road	7596	25 yr_2050	72inRCP	339.00	173.63	176.90		177.00	0.004116	2.58	131.54	116.10	0.43
Poplar Hill Road	7596	25 yr_2100	Exist	374.00	173.63	176.96		177.07	0.004182	2.69	139.23	116.86	0.43
Poplar Hill Road	7596	25 yr_2100	72inRCP	374.00	173.63	176.96		177.07	0.004182	2.69	139.23	116.86	0.43
Poplar Hill Road	7596	100 yr	Exist	469.00	173.63	177.12		177.26	0.004377	2.96	158.32	118.72	0.45
Poplar Hill Road	7596	100 yr	72inRCP	469.00	173.63	177.12		177.26	0.004377	2.96	158.32	118.72	0.45
Poplar Hill Road	7596	100 yr_2050	Exist	578.00	173.63	177.29		177.46	0.004542	3.24	178.65	120.67	0.47
Poplar Hill Road	7596	100 yr_2050	72inRCP	578.00	173.63	177.29		177.46	0.004542	3.24	178.65	120.67	0.47
Poplar Hill Road	7596	100 yr_2100	Exist	622.00	173.63	177.36		177.53	0.004620	3.34	186.18	121.38	0.48
Poplar Hill Road	7596	100 yr_2100	72inRCP	622.00	173.63	177.36		177.53	0.004620	3.34	186.18	121.38	0.48
Poplar Hill Road	7269	25 yr	Exist	281.00	172.54	175.02		175.13	0.007602	2.68	104.74	137.84	0.54
Poplar Hill Road	7269	25 yr	72inRCP	281.00	172.54	175.02		175.13	0.007602	2.68	104.74	137.84	0.54
Poplar Hill Road	7269	25 yr_2050	Exist	339.00	172.54	175.12		175.25	0.007305	2.84	119.19	139.48	0.54
Poplar Hill Road	7269	25 yr_2050	72inRCP	339.00	172.54	175.12		175.25	0.007305	2.84	119.19	139.48	0.54
Poplar Hill Road	7269	25 yr_2100	Exist	374.00	172.54	175.18		175.31	0.007168	2.93	127.48	140.39	0.54
Poplar Hill Road	7269	25 yr_2100	72inRCP	374.00	172.54	175.18		175.31	0.007168	2.93	127.48	140.39	0.54
Poplar Hill Road	7269	100 yr	Exist	469.00	172.54	175.33		175.48	0.006965	3.16	148.23	142.65	0.55
Poplar Hill Road	7269	100 yr	72inRCP	469.00	172.54	175.33		175.48	0.006965	3.16	148.23	142.65	0.55
Poplar Hill Road	7269	100 yr_2050	Exist	578.00	172.54	175.48		175.66	0.006742	3.38	170.82	145.07	0.55
Poplar Hill Road	7269	100 yr_2050	72inRCP	578.00	172.54	175.48		175.66	0.006742	3.38	170.82	145.07	0.55
Poplar Hill Road	7269	100 yr_2100	Exist	622.00	172.54	175.55		175.73	0.006630	3.46	179.89	146.03	0.55
Poplar Hill Road	7269	100 yr_2100	72inRCP	622.00	172.54	175.55		175.73	0.006630	3.46	179.89	146.03	0.55
Poplar Hill Road	7056	25 yr	Exist	281.00	171.51	173.84		173.93	0.004288	2.36	118.96	123.85	0.42
Poplar Hill Road	7056	25 yr	72inRCP	281.00	171.51	173.84		173.93	0.004288	2.36	118.96	123.85	0.42
Poplar Hill Road	7056	25 yr_2050	Exist	339.00	171.51	173.97		174.06	0.004313	2.52	134.69	128.04	0.43
Poplar Hill Road	7056	25 yr_2050	72inRCP	339.00	171.51	173.97		174.06	0.004313	2.52	134.69	128.04	0.43
Poplar Hill Road	7056	25 yr_2100	Exist	374.00	171.51	174.04		174.14	0.004313	2.60	143.92	130.40	0.44
Poplar Hill Road	7056	25 yr_2100	72inRCP	374.00	171.51	174.04		174.14	0.004313	2.60	143.92	130.40	0.44
Poplar Hill Road	7056	100 yr	Exist	469.00	171.51	174.21		174.33	0.004290	2.81	166.92	133.98	0.44
Poplar Hill Road	7056	100 yr	72inRCP	469.00	171.51	174.21		174.33	0.004290	2.81	166.92	133.98	0.44
Poplar Hill Road	7056	100 yr_2050	Exist	578.00	171.51	174.40		174.54	0.004175	3.00	192.56	137.15	0.45
Poplar Hill Road	7056	100 yr_2050	72inRCP	578.00	171.51	174.40		174.54	0.004175	3.00	192.56	137.15	0.45
Poplar Hill Road	7056	100 yr_2100	Exist	622.00	171.51	174.47		174.62	0.004192	3.08	201.95	138.80	0.45
Poplar Hill Road	7056	100 yr_2100	72inRCP	622.00	171.51	174.47		174.62	0.004192	3.08	201.95	138.80	0.45
Poplar Hill Road	6826	25 yr	Exist	281.00	171.37	172.93		173.01	0.003696	2.24	125.29	126.31	0.40
Poplar Hill Road	6826	25 yr	72inRCP	281.00	171.37	172.93		173.01	0.003696	2.24	125.29	126.31	0.40
Poplar Hill Road	6826	25 yr_2050	Exist	339.00	171.37	173.07		173.16	0.003590	2.38	142.72	129.16	0.40
Poplar Hill Road	6826	25 yr_2050	72inRCP	339.00	171.37	173.07		173.16	0.003590	2.38	142.72	129.16	0.40
Poplar Hill Road	6826	25 yr_2100	Exist	374.00	171.37	173.14		173.24	0.003566	2.46	152.34	130.54	0.40
Poplar Hill Road	6826	25 yr_2100	72inRCP	374.00	171.37	173.14		173.24	0.003566	2.46	152.34	130.54	0.40
Poplar Hill Road	6826	100 yr	Exist	469.00	171.37	173.33		173.44	0.003499	2.65	176.93	133.20	0.41
Poplar Hill Road	6826	100 yr	72inRCP	469.00	171.37	173.33		173.44	0.003499	2.65	176.93	133.20	0.41
Poplar Hill Road	6826	100 yr_2050	Exist	578.00	171.37	173.54		173.66	0.003432	2.82	205.23	139.02	0.41
Poplar Hill Road	6826	100 yr_2050	72inRCP	578.00	171.37	173.54		173.66	0.003432	2.82	205.23	139.02	0.41
Poplar Hill Road	6826	100 yr_2100	Exist	622.00	171.37	173.62		173.75	0.003393	2.88	216.16	140.58	0.41
Poplar Hill Road	6826	100 yr_2100	72inRCP	622.00	171.37	173.62		173.75	0.003393	2.88	216.16	140.58	0.41
Poplar Hill Road	6654	25 yr	Exist	281.00	169.07	172.18		172.29	0.004904	2.65	106.22	102.60	0.46
Poplar Hill Road	6654	25 yr	72inRCP	281.00	169.07	172.18		172.29	0.004904	2.65	106.22	102.60	0.46
Poplar Hill Road	6654	25 yr_2050	Exist	339.00	169.07	172.32		172.44	0.004852	2.80	120.97	106.34	0.46
Poplar Hill Road	6654	25 yr_2050	72inRCP	339.00	169.07	172.32		172.44	0.004851	2.80	120.97	106.34	0.46
Poplar Hill Road	6654	25 yr_2100	Exist	374.00	169.07	172.40		172.53	0.004810	2.89	129.26	107.60	0.47
Poplar Hill Road	6654	25 yr_2100	72inRCP	374.00	169.07	172.40		172.53	0.004810	2.89	129.26	107.60	0.47
Poplar Hill Road	6654	100 yr	Exist	469.00	169.07	172.61		172.75	0.004546	3.08	152.25	110.59	0.46
Poplar Hill Road	6654	100 yr	72inRCP	469.00	169.07	172.61		172.75	0.004546	3.08	152.25	110.59	0.46
Poplar Hill Road	6654	100 yr_2050	Exist	578.00	169.07	172.85		173.01	0.004144	3.22	179.65	114.06	0.45
Poplar Hill Road	6654	100 yr_2050	72inRCP	578.00	169.07	172.85		173.01	0.004144	3.22	179.65	114.06	0.45
Poplar Hill Road	6654	100 yr_2100	Exist	622.00	169.07	172.94		173.10	0.004071	3.28	189.45	115.13	0.45
Poplar Hill Road	6654	100 yr_2100	72inRCP	622.00	169.07	172.94		173.10	0.004071	3.28	189.45	115.13	0.45
Poplar Hill Road	6360	25 yr	Exist	281.00	168.21	170.89		171.00	0.003935	2.67	105.08	84.66	0.42
Poplar Hill Road	6360	25 yr	72inRCP	281.00	168.21	170.89		171.00	0.003935	2.67	105.08	84.66	0.42
Poplar Hill Road	6360	25 yr_2050	Exist	339.00	168.21	171.06		171.18	0.003854	2.82	120.07	87.80	0.43
Poplar Hill Road	6360	25 yr_2050	72inRCP	339.00	168.21	171.06		171.18	0.003854	2.82	120.07	87.80	0.43
Poplar Hill Road	6360	25 yr_2100	Exist	374.00	168.21	171.17		171.30	0.003690	2.88	130.00	89.46	0.42
Poplar Hill Road	6360	25 yr_2100	72inRCP	374.00	168.21	171.17		171.30	0.003690	2.88	130.00	89.46	0.42

HEC-RAS River: Zekiah Swamp Reach: Poplar Hill Road (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Poplar Hill Road	6360	100 yr	Exist	469.00	168.21	171.40		171.55	0.003754	3.11	150.78	93.48	0.43
Poplar Hill Road	6360	100 yr	72inRCP	469.00	168.21	171.40		171.55	0.003754	3.11	150.78	93.48	0.43
Poplar Hill Road	6360	100 yr_2050	Exist	578.00	168.21	171.66		171.82	0.003939	3.28	176.32	104.84	0.45
Poplar Hill Road	6360	100 yr_2050	72inRCP	578.00	168.21	171.66		171.82	0.003939	3.28	176.32	104.84	0.45
Poplar Hill Road	6360	100 yr_2100	Exist	622.00	168.21	171.75		171.92	0.003986	3.35	185.81	108.06	0.45
Poplar Hill Road	6360	100 yr_2100	72inRCP	622.00	168.21	171.75		171.92	0.003986	3.35	185.81	108.06	0.45
Poplar Hill Road	6034	25 yr	Exist	281.00	166.40	169.67		169.77	0.003637	2.51	111.98	93.55	0.40
Poplar Hill Road	6034	25 yr	72inRCP	281.00	166.40	169.67		169.77	0.003637	2.51	111.97	93.55	0.40
Poplar Hill Road	6034	25 yr_2050	Exist	339.00	166.40	169.81		169.93	0.003865	2.69	125.79	98.88	0.42
Poplar Hill Road	6034	25 yr_2050	72inRCP	339.00	166.40	169.81		169.93	0.003865	2.69	125.80	98.88	0.42
Poplar Hill Road	6034	25 yr_2100	Exist	374.00	166.40	169.91		170.03	0.004129	2.75	135.94	108.95	0.43
Poplar Hill Road	6034	25 yr_2100	72inRCP	374.00	166.40	169.91		170.03	0.004130	2.75	135.94	108.95	0.43
Poplar Hill Road	6034	100 yr	Exist	469.00	166.40	170.08		170.22	0.004487	3.02	155.11	114.88	0.46
Poplar Hill Road	6034	100 yr	72inRCP	469.00	166.40	170.08		170.22	0.004487	3.02	155.11	114.88	0.46
Poplar Hill Road	6034	100 yr_2050	Exist	578.00	166.40	170.25		170.42	0.004752	3.31	174.78	118.13	0.48
Poplar Hill Road	6034	100 yr_2050	72inRCP	578.00	166.40	170.25		170.42	0.004752	3.31	174.78	118.13	0.48
Poplar Hill Road	6034	100 yr_2100	Exist	622.00	166.40	170.31		170.49	0.004844	3.41	182.48	119.58	0.49
Poplar Hill Road	6034	100 yr_2100	72inRCP	622.00	166.40	170.31		170.49	0.004844	3.41	182.48	119.58	0.49
Poplar Hill Road	5576	25 yr	Exist	281.00	165.82	167.71		167.80	0.005120	2.39	117.55	138.54	0.46
Poplar Hill Road	5576	25 yr	72inRCP	281.00	165.82	167.71		167.80	0.005121	2.39	117.54	138.54	0.46
Poplar Hill Road	5576	25 yr_2050	Exist	339.00	165.82	167.83		167.93	0.004915	2.54	133.69	141.33	0.46
Poplar Hill Road	5576	25 yr_2050	72inRCP	339.00	165.82	167.83		167.93	0.004916	2.54	133.69	141.33	0.46
Poplar Hill Road	5576	25 yr_2100	Exist	374.00	165.82	167.90		168.00	0.004691	2.60	144.22	142.39	0.45
Poplar Hill Road	5576	25 yr_2100	72inRCP	374.00	165.82	167.90		168.00	0.004691	2.60	144.21	142.39	0.45
Poplar Hill Road	5576	100 yr	Exist	469.00	165.82	168.08		168.20	0.004320	2.78	170.45	147.88	0.44
Poplar Hill Road	5576	100 yr	72inRCP	469.00	165.82	168.08		168.20	0.004320	2.78	170.45	147.88	0.44
Poplar Hill Road	5576	100 yr_2050	Exist	578.00	165.82	168.27		168.41	0.004026	2.95	198.89	150.18	0.44
Poplar Hill Road	5576	100 yr_2050	72inRCP	578.00	165.82	168.27		168.41	0.004026	2.95	198.89	150.18	0.44
Poplar Hill Road	5576	100 yr_2100	Exist	622.00	165.82	168.34		168.48	0.003949	3.02	209.63	150.82	0.44
Poplar Hill Road	5576	100 yr_2100	72inRCP	622.00	165.82	168.34		168.48	0.003949	3.02	209.63	150.82	0.44
Poplar Hill Road	5302	25 yr	Exist	281.00	164.25	166.68		166.75	0.002952	2.19	128.20	112.47	0.36
Poplar Hill Road	5302	25 yr	72inRCP	281.00	164.25	166.68		166.75	0.002951	2.19	128.21	112.47	0.36
Poplar Hill Road	5302	25 yr_2050	Exist	339.00	164.25	166.84		166.92	0.002803	2.31	146.99	114.93	0.36
Poplar Hill Road	5302	25 yr_2050	72inRCP	339.00	164.25	166.84		166.92	0.002803	2.31	146.99	114.93	0.36
Poplar Hill Road	5302	25 yr_2100	Exist	374.00	164.25	166.93		167.01	0.002841	2.39	156.81	117.76	0.36
Poplar Hill Road	5302	25 yr_2100	72inRCP	374.00	164.25	166.93		167.01	0.002841	2.39	156.81	117.76	0.36
Poplar Hill Road	5302	100 yr	Exist	469.00	164.25	167.13		167.24	0.002934	2.57	182.23	125.10	0.38
Poplar Hill Road	5302	100 yr	72inRCP	469.00	164.25	167.13		167.24	0.002934	2.57	182.23	125.10	0.38
Poplar Hill Road	5302	100 yr_2050	Exist	578.00	164.25	167.34		167.46	0.002979	2.76	209.08	130.45	0.38
Poplar Hill Road	5302	100 yr_2050	72inRCP	578.00	164.25	167.34		167.46	0.002979	2.76	209.08	130.45	0.38
Poplar Hill Road	5302	100 yr_2100	Exist	622.00	164.25	167.42		167.55	0.002986	2.84	219.33	131.90	0.39
Poplar Hill Road	5302	100 yr_2100	72inRCP	622.00	164.25	167.42		167.55	0.002986	2.84	219.32	131.90	0.39
Poplar Hill Road	4848	25 yr	Exist	281.00	163.88	165.98		166.01	0.001016	1.37	204.57	163.25	0.22
Poplar Hill Road	4848	25 yr	72inRCP	281.00	163.88	165.97		166.00	0.001019	1.37	204.37	163.21	0.22
Poplar Hill Road	4848	25 yr_2050	Exist	339.00	163.88	166.13		166.17	0.001069	1.46	231.53	174.85	0.22
Poplar Hill Road	4848	25 yr_2050	72inRCP	339.00	163.88	166.13		166.17	0.001069	1.46	231.50	174.85	0.22
Poplar Hill Road	4848	25 yr_2100	Exist	374.00	163.88	166.21		166.24	0.001090	1.53	244.25	176.13	0.23
Poplar Hill Road	4848	25 yr_2100	72inRCP	374.00	163.88	166.21		166.24	0.001090	1.53	244.21	176.12	0.23
Poplar Hill Road	4848	100 yr	Exist	469.00	163.88	166.40		166.44	0.001116	1.69	278.42	180.12	0.24
Poplar Hill Road	4848	100 yr	72inRCP	469.00	163.88	166.40		166.44	0.001116	1.69	278.42	180.12	0.24
Poplar Hill Road	4848	100 yr_2050	Exist	578.00	163.88	166.59		166.64	0.001166	1.86	312.79	184.06	0.25
Poplar Hill Road	4848	100 yr_2050	72inRCP	578.00	163.88	166.59		166.64	0.001166	1.86	312.76	184.05	0.25
Poplar Hill Road	4848	100 yr_2100	Exist	622.00	163.88	166.66		166.72	0.001173	1.92	326.90	185.88	0.25
Poplar Hill Road	4848	100 yr_2100	72inRCP	622.00	163.88	166.66		166.72	0.001173	1.92	326.89	185.88	0.25
Poplar Hill Road	4582	25 yr	Exist	281.00	163.35	164.87	164.86	165.21	0.026762	4.68	60.03	88.62	1.00
Poplar Hill Road	4582	25 yr	72inRCP	281.00	163.35	164.87	164.86	165.21	0.026268	4.65	60.42	88.81	0.99
Poplar Hill Road	4582	25 yr_2050	Exist	339.00	163.35	164.98	164.98	165.34	0.026240	4.85	69.84	96.21	1.00
Poplar Hill Road	4582	25 yr_2050	72inRCP	339.00	163.35	164.98	164.98	165.34	0.026208	4.85	69.90	96.31	1.00
Poplar Hill Road	4582	25 yr_2100	Exist	374.00	163.35	165.03	165.03	165.41	0.026888	4.97	75.29	102.02	1.02
Poplar Hill Road	4582	25 yr_2100	72inRCP	374.00	163.35	165.03	165.03	165.41	0.026767	4.96	75.41	102.09	1.02
Poplar Hill Road	4582	100 yr	Exist	469.00	163.35	165.17	165.17	165.59	0.025770	5.22	89.82	109.39	1.02
Poplar Hill Road	4582	100 yr	72inRCP	469.00	163.35	165.17	165.17	165.59	0.025770	5.22	89.82	109.39	1.02
Poplar Hill Road	4582	100 yr_2050	Exist	578.00	163.35	165.32	165.32	165.77	0.023403	5.38	107.43	116.53	0.99
Poplar Hill Road	4582	100 yr_2050	72inRCP	578.00	163.35	165.32	165.32	165.77	0.023403	5.38	107.43	116.53	0.99
Poplar Hill Road	4582	100 yr_2100	Exist	622.00	163.35	165.36	165.36	165.84	0.023881	5.55	112.10	119.89	1.00
Poplar Hill Road	4582	100 yr_2100	72inRCP	622.00	163.35	165.36	165.36	165.84	0.023881	5.55	112.10	119.89	1.00
Poplar Hill Road	4355	25 yr	Exist	281.00	161.71	163.48		163.54	0.003166	1.93	145.55	163.36	0.36
Poplar Hill Road	4355	25 yr	72inRCP	281.00	161.71	163.48		163.54	0.003178	1.93	145.37	163.32	0.36
Poplar Hill Road	4355	25 yr_2050	Exist	339.00	161.71	163.60		163.67	0.003047	2.04	166.29	167.14	0.36
Poplar Hill Road	4355	25 yr_2050	72inRCP	339.00	161.71	163.60		163.67	0.003057	2.04	166.13	167.12	0.36
Poplar Hill Road	4355	25 yr_2100	Exist	374.00	161.71	163.67		163.74	0.003004	2.10	177.90	168.93	0.36
Poplar Hill Road	4355	25 yr_2100	72inRCP	374.00	161.71	163.67		163.74	0.003003	2.10	177.92	168.94	0.36
Poplar Hill Road	4355	100 yr	Exist	469.00	161.71	163.85		163.93	0.002864	2.25	208.18	171.91	0.36
Poplar Hill Road	4355	100 yr	72inRCP	469.00	161.71	163.85		163.93	0.002866	2.25	208.12	171.90	0.36
Poplar Hill Road	4355	100 yr_2050	Exist	578.00	161.71	164.04		164.13	0.002757	2.40	240.39	174.97	0.36
Poplar Hill Road	4355	100 yr_2050	72inRCP	578.00	161.71	164.03		164.12	0.002772	2.41	239.98	174.93	0.36
Poplar Hill Road	4355	100 yr_2100	Exist	622.00	161.71	164.11		164.21	0.002744	2.45	253.75	178.80	0.36
Poplar Hill Road	4355	100 yr_2100	72inRCP	622.00	161.71	164.11		164.20	0.002754	2.45	253.42	178.71	0.36

HEC-RAS River: Zekiah Swamp Reach: Poplar Hill Road (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Poplar Hill Road	4087	25 yr	Exist	281.00	160.19	162.75		162.80	0.002389	1.85	151.99	147.29	0.32
Poplar Hill Road	4087	25 yr	72inRCP	281.00	160.19	162.78		162.83	0.002211	1.80	156.37	149.24	0.31
Poplar Hill Road	4087	25 yr_2050	Exist	339.00	160.19	162.90		162.96	0.002328	1.95	174.27	153.47	0.32
Poplar Hill Road	4087	25 yr_2050	72inRCP	339.00	160.19	162.92		162.98	0.002198	1.91	177.53	153.96	0.31
Poplar Hill Road	4087	25 yr_2100	Exist	374.00	160.19	162.98		163.04	0.002293	2.00	186.61	155.39	0.32
Poplar Hill Road	4087	25 yr_2100	72inRCP	374.00	160.19	162.99		163.05	0.002203	1.98	189.13	155.91	0.32
Poplar Hill Road	4087	100 yr	Exist	469.00	160.19	163.19		163.26	0.002195	2.13	219.85	161.33	0.32
Poplar Hill Road	4087	100 yr	72inRCP	469.00	160.19	163.18		163.25	0.002219	2.14	219.08	161.21	0.32
Poplar Hill Road	4087	100 yr_2050	Exist	578.00	160.19	163.40		163.48	0.002128	2.27	254.92	166.76	0.32
Poplar Hill Road	4087	100 yr_2050	72inRCP	578.00	160.19	163.39		163.47	0.002188	2.29	252.59	166.41	0.33
Poplar Hill Road	4087	100 yr_2100	Exist	622.00	160.19	163.48		163.56	0.002117	2.32	267.56	169.43	0.32
Poplar Hill Road	4087	100 yr_2100	72inRCP	622.00	160.19	163.46		163.55	0.002177	2.34	265.29	168.77	0.33
Poplar Hill Road	3698	25 yr	Exist	281.00	158.02	161.53	160.89	161.62	0.003974	2.39	117.60	112.62	0.41
Poplar Hill Road	3698	25 yr	72inRCP	281.00	158.02	161.37		161.49	0.006122	2.82	99.76	103.14	0.50
Poplar Hill Road	3698	25 yr_2050	Exist	339.00	158.02	161.62	161.00	161.73	0.004505	2.64	128.23	115.95	0.44
Poplar Hill Road	3698	25 yr_2050	72inRCP	339.00	158.02	161.51		161.65	0.006036	2.93	115.69	111.60	0.51
Poplar Hill Road	3698	25 yr_2100	Exist	374.00	158.02	161.67	161.07	161.79	0.004858	2.80	133.35	116.77	0.46
Poplar Hill Road	3698	25 yr_2100	72inRCP	374.00	158.02	161.60		161.74	0.005817	2.97	125.81	115.56	0.50
Poplar Hill Road	3698	100 yr	Exist	469.00	158.02	161.76	161.23	161.92	0.005988	3.25	144.31	118.50	0.52
Poplar Hill Road	3698	100 yr	72inRCP	469.00	158.02	161.78	161.23	161.94	0.005646	3.19	147.09	118.94	0.51
Poplar Hill Road	3698	100 yr_2050	Exist	578.00	158.02	161.87	161.37	162.08	0.007213	3.67	157.68	124.37	0.57
Poplar Hill Road	3698	100 yr_2050	72inRCP	578.00	158.02	161.93	161.37	162.12	0.006275	3.51	164.77	125.04	0.54
Poplar Hill Road	3698	100 yr_2100	Exist	622.00	158.02	161.91	161.45	162.14	0.007606	3.83	162.42	124.82	0.59
Poplar Hill Road	3698	100 yr_2100	72inRCP	622.00	158.02	161.97	161.45	162.18	0.006543	3.65	170.33	125.57	0.55
Poplar Hill Road	3358	25 yr	Exist	281.00	157.42	159.93		160.00	0.005796	2.14	131.40	198.92	0.46
Poplar Hill Road	3358	25 yr	72inRCP	281.00	157.42	160.10	159.50	160.15	0.002681	1.68	167.11	203.50	0.33
Poplar Hill Road	3358	25 yr_2050	Exist	339.00	157.42	160.05		160.12	0.004922	2.18	155.61	202.66	0.44
Poplar Hill Road	3358	25 yr_2050	72inRCP	339.00	157.42	160.18		160.23	0.002958	1.86	181.94	206.86	0.35
Poplar Hill Road	3358	25 yr_2100	Exist	374.00	157.42	160.12		160.20	0.004426	2.19	170.77	203.77	0.42
Poplar Hill Road	3358	25 yr_2100	72inRCP	374.00	157.42	160.21		160.27	0.003233	1.99	188.09	207.54	0.37
Poplar Hill Road	3358	100 yr	Exist	469.00	157.42	160.33		160.40	0.003383	2.20	213.70	215.40	0.38
Poplar Hill Road	3358	100 yr	72inRCP	469.00	157.42	160.29		160.37	0.003773	2.28	206.42	213.79	0.40
Poplar Hill Road	3358	100 yr_2050	Exist	578.00	157.42	160.55		160.63	0.002681	2.23	262.22	218.84	0.35
Poplar Hill Road	3358	100 yr_2050	72inRCP	578.00	157.42	160.47		160.55	0.003398	2.39	243.54	217.60	0.39
Poplar Hill Road	3358	100 yr_2100	Exist	622.00	157.42	160.63		160.71	0.002506	2.25	280.34	220.26	0.34
Poplar Hill Road	3358	100 yr_2100	72inRCP	622.00	157.42	160.54		160.63	0.003236	2.43	258.84	218.62	0.38
Poplar Hill Road	3017	25 yr	Exist	281.00	156.54	159.25		159.28	0.001055	1.38	202.93	164.29	0.22
Poplar Hill Road	3017	25 yr	72inRCP	281.00	156.54	158.64		158.75	0.007137	2.56	109.71	148.09	0.52
Poplar Hill Road	3017	25 yr_2050	Exist	339.00	156.54	159.44		159.47	0.000980	1.44	235.09	169.44	0.22
Poplar Hill Road	3017	25 yr_2050	72inRCP	339.00	156.54	158.82		158.91	0.005311	2.50	135.50	151.77	0.47
Poplar Hill Road	3017	25 yr_2100	Exist	374.00	156.54	159.57		159.60	0.000901	1.45	257.11	171.74	0.21
Poplar Hill Road	3017	25 yr_2100	72inRCP	374.00	156.54	159.97		159.06	0.003853	2.35	159.05	153.67	0.41
Poplar Hill Road	3017	100 yr	Exist	469.00	156.54	159.86		159.90	0.000793	1.52	308.22	174.72	0.20
Poplar Hill Road	3017	100 yr	72inRCP	469.00	156.54	159.51		159.57	0.001610	1.90	246.89	170.72	0.28
Poplar Hill Road	3017	100 yr_2050	Exist	578.00	156.54	160.14		160.18	0.000756	1.62	356.04	177.55	0.20
Poplar Hill Road	3017	100 yr_2050	72inRCP	578.00	156.54	159.75		159.81	0.001493	2.01	288.15	173.55	0.27
Poplar Hill Road	3017	100 yr_2100	Exist	622.00	156.54	160.23		160.27	0.000754	1.67	372.60	178.48	0.20
Poplar Hill Road	3017	100 yr_2100	72inRCP	622.00	156.54	159.86		159.92	0.001404	2.02	307.57	174.68	0.27
Poplar Hill Road	2708	25 yr	Exist	281.00	156.19	159.19		159.20	0.000100	0.61	464.23	221.74	0.07
Poplar Hill Road	2708	25 yr	72inRCP	281.00	156.19	158.19		158.21	0.000721	1.13	248.98	206.20	0.18
Poplar Hill Road	2708	25 yr_2050	Exist	339.00	156.19	159.38		159.39	0.000111	0.67	506.26	224.78	0.08
Poplar Hill Road	2708	25 yr_2050	72inRCP	339.00	156.19	158.52		158.54	0.000478	1.06	318.67	211.93	0.15
Poplar Hill Road	2708	25 yr_2100	Exist	374.00	156.19	159.51		159.52	0.000113	0.70	535.48	227.29	0.08
Poplar Hill Road	2708	25 yr_2100	72inRCP	374.00	156.19	158.75		158.77	0.000368	1.02	368.22	215.44	0.14
Poplar Hill Road	2708	100 yr	Exist	469.00	156.19	159.80		159.81	0.000124	0.78	603.05	233.47	0.09
Poplar Hill Road	2708	100 yr	72inRCP	469.00	156.19	159.40		159.41	0.000206	0.92	510.81	225.17	0.11
Poplar Hill Road	2708	100 yr_2050	Exist	578.00	156.19	160.07		160.08	0.000142	0.87	666.52	241.93	0.09
Poplar Hill Road	2708	100 yr_2050	72inRCP	578.00	156.19	159.63		159.65	0.000231	1.03	563.70	229.68	0.12
Poplar Hill Road	2708	100 yr_2100	Exist	622.00	156.19	160.16		160.17	0.000149	0.90	688.67	243.61	0.09
Poplar Hill Road	2708	100 yr_2100	72inRCP	622.00	156.19	159.75		159.76	0.000234	1.05	589.82	232.14	0.12
Poplar Hill Road	2305	25 yr	Exist	281.00	154.86	159.15		159.16	0.000096	0.58	483.54	237.83	0.07
Poplar Hill Road	2305	25 yr	72inRCP	281.00	154.86	157.81		157.84	0.001193	1.42	197.29	167.47	0.23
Poplar Hill Road	2305	25 yr_2050	Exist	339.00	154.86	159.34		159.34	0.000106	0.64	527.65	241.12	0.08
Poplar Hill Road	2305	25 yr_2050	72inRCP	339.00	154.86	158.30		158.32	0.000637	1.18	288.14	203.73	0.17
Poplar Hill Road	2305	25 yr_2100	Exist	374.00	154.86	159.47		159.47	0.000108	0.67	558.77	244.65	0.08
Poplar Hill Road	2305	25 yr_2100	72inRCP	374.00	154.86	158.59		158.60	0.000467	1.07	351.15	228.40	0.15
Poplar Hill Road	2305	100 yr	Exist	469.00	154.86	159.76		159.76	0.000118	0.74	631.54	258.03	0.08
Poplar Hill Road	2305	100 yr	72inRCP	469.00	154.86	159.32		159.33	0.000209	0.90	522.82	240.77	0.11
Poplar Hill Road	2305	100 yr_2050	Exist	578.00	154.86	160.02		160.03	0.000129	0.83	699.38	261.18	0.09
Poplar Hill Road	2305	100 yr_2050	72inRCP	578.00	154.86	159.54		159.56	0.000234	1.00	577.08	248.57	0.12
Poplar Hill Road	2305	100 yr_2100	Exist	622.00	154.86	160.11		160.12	0.000135	0.87	722.63	262.29	0.09
Poplar Hill Road	2305	100 yr_2100	72inRCP	622.00	154.86	159.65		159.67	0.000234	1.03	605.37	252.83	0.12
Poplar Hill Road	2119	25 yr	Exist	281.00	153.73	159.14	155.29	159.15	0.000037	0.55	508.66	227.30	0.05
Poplar Hill Road	2119	25 yr	72inRCP	281.00	153.73	157.75	155.29	157.76	0.000167	0.87	323.13	205.46	0.10
Poplar Hill Road	2119	25 yr_2050	Exist	339.00	153.73	159.33	155.40	159.34	0.000020	0.42	825.22	234.65	0.04
Poplar Hill Road	2119	25 yr_2050	72inRCP	339.00	153.73	158.26	155.40	158.27	0.000130	0.87	390.17	217.45	0.09
Poplar Hill Road	2119	25 yr_2100	Exist	374.00	153.73	159.46	155.45	159.46	0.000022	0.44	853.29	236.59	0.04

HEC-RAS River: Zekiah Swamp Reach: Poplar Hill Road (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Poplar Hill Road	2119	25 yr_2100	72inRCP	374.00	153.73	158.55	155.45	158.56	0.000116	0.87	429.49	221.57	0.09
Poplar Hill Road	2119	100 yr	Exist	469.00	153.73	159.75	155.60	159.75	0.000028	0.52	916.75	240.84	0.04
Poplar Hill Road	2119	100 yr	72inRCP	469.00	153.73	159.31	155.60	159.31	0.000040	0.58	819.68	233.31	0.05
Poplar Hill Road	2119	100 yr_2050	Exist	578.00	153.73	160.01	155.75	160.01	0.000035	0.60	974.33	245.06	0.05
Poplar Hill Road	2119	100 yr_2050	72inRCP	578.00	153.73	159.53	155.75	159.53	0.000050	0.67	868.00	237.44	0.06
Poplar Hill Road	2119	100 yr_2100	Exist	622.00	153.73	160.10	155.81	160.10	0.000038	0.64	993.93	246.49	0.05
Poplar Hill Road	2119	100 yr_2100	72inRCP	622.00	153.73	159.64	155.81	159.65	0.000053	0.71	892.70	239.08	0.06
Poplar Hill Road	2085												
Poplar Hill Road	2040	25 yr	Exist	281.00	151.84	154.47	153.72	154.65	0.004665	3.41	82.52	71.11	0.48
Poplar Hill Road	2040	25 yr	72inRCP	281.00	151.84	154.47	153.72	154.65	0.004665	3.41	82.52	71.11	0.48
Poplar Hill Road	2040	25 yr_2050	Exist	339.00	151.84	154.63	153.88	154.85	0.005247	3.71	91.29	76.86	0.51
Poplar Hill Road	2040	25 yr_2050	72inRCP	339.00	151.84	154.63	153.88	154.85	0.005247	3.71	91.29	76.86	0.51
Poplar Hill Road	2040	25 yr_2100	Exist	374.00	151.84	154.71	153.97	154.95	0.005684	3.92	95.39	79.42	0.53
Poplar Hill Road	2040	25 yr_2100	72inRCP	374.00	151.84	154.71	153.97	154.95	0.005684	3.92	95.39	79.42	0.53
Poplar Hill Road	2040	100 yr	Exist	469.00	151.84	154.89	154.21	155.20	0.006801	4.41	106.26	86.80	0.59
Poplar Hill Road	2040	100 yr	72inRCP	469.00	151.84	154.89	154.21	155.20	0.006801	4.41	106.26	86.80	0.59
Poplar Hill Road	2040	100 yr_2050	Exist	578.00	151.84	155.10	154.44	155.47	0.007803	4.86	119.03	105.42	0.63
Poplar Hill Road	2040	100 yr_2050	72inRCP	578.00	151.84	155.10	154.44	155.47	0.007803	4.86	119.03	105.42	0.63
Poplar Hill Road	2040	100 yr_2100	Exist	622.00	151.84	155.19	154.54	155.57	0.008182	4.98	124.94	112.86	0.65
Poplar Hill Road	2040	100 yr_2100	72inRCP	622.00	151.84	155.19	154.54	155.57	0.008182	4.98	124.94	112.86	0.65
Poplar Hill Road	1606	25 yr	Exist	281.00	148.92	151.12		151.27	0.015265	3.18	88.32	152.44	0.74
Poplar Hill Road	1606	25 yr	72inRCP	281.00	148.92	151.12		151.27	0.015265	3.18	88.32	152.44	0.74
Poplar Hill Road	1606	25 yr_2050	Exist	339.00	148.92	151.22		151.38	0.013237	3.22	105.32	160.54	0.70
Poplar Hill Road	1606	25 yr_2050	72inRCP	339.00	148.92	151.22		151.38	0.013237	3.22	105.32	160.54	0.70
Poplar Hill Road	1606	25 yr_2100	Exist	374.00	148.92	151.29		151.45	0.011914	3.22	116.03	163.10	0.67
Poplar Hill Road	1606	25 yr_2100	72inRCP	374.00	148.92	151.29		151.45	0.011914	3.22	116.03	163.10	0.67
Poplar Hill Road	1606	100 yr	Exist	469.00	148.92	151.45		151.62	0.009751	3.30	141.94	165.39	0.63
Poplar Hill Road	1606	100 yr	72inRCP	469.00	148.92	151.45		151.62	0.009751	3.30	141.94	165.39	0.63
Poplar Hill Road	1606	100 yr_2050	Exist	578.00	148.92	151.60		151.78	0.008792	3.46	166.85	167.56	0.61
Poplar Hill Road	1606	100 yr_2050	72inRCP	578.00	148.92	151.60		151.78	0.008792	3.46	166.85	167.56	0.61
Poplar Hill Road	1606	100 yr_2100	Exist	622.00	148.92	151.65		151.85	0.008554	3.53	175.97	167.95	0.61
Poplar Hill Road	1606	100 yr_2100	72inRCP	622.00	148.92	151.65		151.85	0.008554	3.53	175.97	167.95	0.61
Poplar Hill Road	1360	25 yr	Exist	281.00	147.21	149.96		150.02	0.002425	1.93	145.64	133.46	0.33
Poplar Hill Road	1360	25 yr	72inRCP	281.00	147.21	149.96		150.02	0.002425	1.93	145.64	133.46	0.33
Poplar Hill Road	1360	25 yr_2050	Exist	339.00	147.21	150.10		150.17	0.002485	2.06	164.29	138.65	0.33
Poplar Hill Road	1360	25 yr_2050	72inRCP	339.00	147.21	150.10		150.17	0.002485	2.06	164.29	138.65	0.33
Poplar Hill Road	1360	25 yr_2100	Exist	374.00	147.21	150.19		150.26	0.002544	2.12	176.72	146.14	0.34
Poplar Hill Road	1360	25 yr_2100	72inRCP	374.00	147.21	150.19		150.26	0.002544	2.12	176.72	146.14	0.34
Poplar Hill Road	1360	100 yr	Exist	469.00	147.21	150.36		150.45	0.002736	2.31	203.02	155.50	0.36
Poplar Hill Road	1360	100 yr	72inRCP	469.00	147.21	150.36		150.45	0.002736	2.31	203.02	155.50	0.36
Poplar Hill Road	1360	100 yr_2050	Exist	578.00	147.21	150.53		150.63	0.002829	2.53	228.85	157.18	0.37
Poplar Hill Road	1360	100 yr_2050	72inRCP	578.00	147.21	150.53		150.63	0.002829	2.53	228.85	157.18	0.37
Poplar Hill Road	1360	100 yr_2100	Exist	622.00	147.21	150.60		150.70	0.002822	2.59	239.77	157.89	0.37
Poplar Hill Road	1360	100 yr_2100	72inRCP	622.00	147.21	150.60		150.70	0.002822	2.59	239.77	157.89	0.37
Poplar Hill Road	1109	25 yr	Exist	281.00	147.42	149.14		149.22	0.004423	2.23	126.22	147.22	0.42
Poplar Hill Road	1109	25 yr	72inRCP	281.00	147.42	149.14		149.22	0.004423	2.23	126.22	147.22	0.42
Poplar Hill Road	1109	25 yr_2050	Exist	339.00	147.42	149.26		149.35	0.004473	2.34	144.71	157.69	0.43
Poplar Hill Road	1109	25 yr_2050	72inRCP	339.00	147.42	149.26		149.35	0.004473	2.34	144.71	157.69	0.43
Poplar Hill Road	1109	25 yr_2100	Exist	374.00	147.42	149.33		149.42	0.004471	2.40	156.08	164.33	0.43
Poplar Hill Road	1109	25 yr_2100	72inRCP	374.00	147.42	149.33		149.42	0.004471	2.40	156.08	164.33	0.43
Poplar Hill Road	1109	100 yr	Exist	469.00	147.42	149.48		149.58	0.004432	2.59	180.78	167.85	0.44
Poplar Hill Road	1109	100 yr	72inRCP	469.00	147.42	149.48		149.58	0.004432	2.59	180.78	167.85	0.44
Poplar Hill Road	1109	100 yr_2050	Exist	578.00	147.42	149.63		149.75	0.004449	2.80	206.48	171.55	0.45
Poplar Hill Road	1109	100 yr_2050	72inRCP	578.00	147.42	149.63		149.75	0.004449	2.80	206.48	171.55	0.45
Poplar Hill Road	1109	100 yr_2100	Exist	622.00	147.42	149.70		149.83	0.004450	2.84	218.86	177.78	0.45
Poplar Hill Road	1109	100 yr_2100	72inRCP	622.00	147.42	149.70		149.83	0.004450	2.84	218.86	177.78	0.45
Poplar Hill Road	722	25 yr	Exist	281.00	145.80	147.37	146.90	147.45	0.004686	2.28	123.06	144.12	0.44
Poplar Hill Road	722	25 yr	72inRCP	281.00	145.80	147.37	146.90	147.45	0.004686	2.28	123.06	144.12	0.44
Poplar Hill Road	722	25 yr_2050	Exist	339.00	145.80	147.50	146.98	147.58	0.004685	2.39	141.98	155.51	0.44
Poplar Hill Road	722	25 yr_2050	72inRCP	339.00	145.80	147.50	146.98	147.58	0.004685	2.39	141.98	155.51	0.44
Poplar Hill Road	722	25 yr_2100	Exist	374.00	145.80	147.56	147.04	147.65	0.004685	2.47	151.40	157.56	0.44
Poplar Hill Road	722	25 yr_2100	72inRCP	374.00	145.80	147.56	147.04	147.65	0.004685	2.47	151.40	157.56	0.44
Poplar Hill Road	722	100 yr	Exist	469.00	145.80	147.71	147.16	147.82	0.004689	2.66	176.10	163.84	0.45
Poplar Hill Road	722	100 yr	72inRCP	469.00	145.80	147.71	147.16	147.82	0.004689	2.66	176.10	163.84	0.45
Poplar Hill Road	722	100 yr_2050	Exist	578.00	145.80	147.86	147.29	147.99	0.004682	2.87	201.37	167.26	0.46
Poplar Hill Road	722	100 yr_2050	72inRCP	578.00	145.80	147.86	147.29	147.99	0.004682	2.87	201.37	167.26	0.46
Poplar Hill Road	722	100 yr_2100	Exist	622.00	145.80	147.92	147.34	148.06	0.004687	2.95	211.02	168.54	0.46
Poplar Hill Road	722	100 yr_2100	72inRCP	622.00	145.80	147.92	147.34	148.06	0.004687	2.95	211.02	168.54	0.46

Attachment 7

ALTERNATIVES MATRIX



Alternatives Matrix - Location 10: Old Washington Rd and Shoppers World

December 2022

PPA
*pending SME and local official feedback

Alternatives			1: No Build	2: Drainage System Improvements	3: Drainage System Improvements, restore portion of lot to pervious, add GI and/or underground Detention	4: Drainage System Improvements, Add GI and/or Underground Detention	5: Drainage System Improvements, Add GI, and Install Pump Station
Overview							
Advantages	1	Description	• No advantages.	• Upsize and replace old CMP, recessed pipes, and inlets • Re-establish positive pipe slopes • Clean existing system • Stabilize, widen, and clean streams	• Upsize and replace old CMP, recessed pipes, and inlets • Re-establish positive pipe slopes • Clean existing system • Stabilize, widen, and clean streams • Remove portion of impervious area at loading zone • Install GI and subsurface detention at multiple parking locations to capture runoff close to the source to provide storage to increase overall system capacity	• Upsize and replace old CMP, recessed pipes, and inlets • Re-establish positive pipe slopes • Clean existing system • Stabilize, widen, and clean streams • Install GI at multiple parking locations at multiple locations to capture runoff close to the source	• Upsize and replace old CMP, recessed pipes, and inlets • Re-establish positive pipe slopes • Clean existing system • Stabilize, widen, and clean streams • Install GI at multiple parking locations at multiple locations to capture runoff close to the source • Install pump station near Old Washington Rd
	2	Description	• Does not address Purpose and Need	• Roadway may still flood during larger, high volume rainfall events. • May increase flooding downstream near existing basin	• Will provide storage and flow attenuation • Flooding may still occur in larger, high intensity events • ROW acquisition will be required.	• Will provide storage and flow attenuation • Flooding may still occur in larger, high intensity events • ROW acquisition will be required.	• Provides faster drainage during large, high intensity events. • Provides storage to alleviate roadway flooding in larger rain events. • Most costly option. • ROW acquisition will be required.
Purpose & Need							
Address chronic flooding	3		Y/N	N	N	Y	Y
	4	Description	None	25 year rainfall event	25 year rainfall event	25 year rainfall event	25 year rainfall event
Goals & Objectives							
Minimize present day flooding while implementing a resilient design to account for future flooding condition	5		Y/N	N	N	Y	Y
Avoid and/or minimize environmental impacts	6		Y/N	N/A	N	Y	Y
Minimize right-of-way impacts	7		Y/N	N/A	Y	N	N
Minimize utility impacts and relocations	8		Y/N	N/A	Y	N	N
Environmental							
Approximate Wetland and Waterway Impacts	9		Y/N	N/A	Y	Y	Y
Rights-of-Way							
Within ROW	10		Y/N	N/A	N	N	N
Construction Duration and Cost							
Construction Duration	11	months	N/A	5	6	6	7
	12	\$	N/A	\$1,170,000	\$1,480,000	\$1,450,000	\$1,940,000

Notes: 1. Assumed \$160/LF of pipe to be replaced
2. Approximately 10 drainage structures (inlets/manhole) need to be replaced/reconstructed assumed at \$2,000
3. Assumed \$100,000 for mobilization, traffic control, and access
4. Assumed \$300,000 for pavement work
5. \$15/ft^3 assumed for detention storage cost
6. \$350,000 assumed for pump station
7. \$25,000 assumed for re-vegetation
8. 30% added contingency

3: Drainage System Improvements, restore portion of lot to pervious, add GI and/or underground Detention
• Upsize and replace old CMP, recessed pipes, and inlets • Re-establish positive pipe slopes • Clean existing system • Stabilize, widen, and clean streams • Remove portion of impervious area at loading zone • Install GI and subsurface detention at multiple parking locations to capture runoff close to the source to provide storage to increase overall system capacity
• Will provide storage and flow attenuation • Flooding may still occur in larger, high intensity events • ROW acquisition will be required.
Y
25 year rainfall event
Y
Y
N
N
Y
N
6
\$1,480,000

Alternatives Matrix - Location 12: Industrial Park Drive and Post Office Road

December 2022

PPA
*pending SME and local official feedback

Alternatives			1: No Build	2: Drainage System Improvements; replace 60" RCP with dual 48" RCP	3: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP	4: Drainage System Improvements; replace 60" RCP with dual 48" RCP and add GI	5: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP and add GI
Overview							
Advantages	1	Description	• No advantages.	• Clean existing RCP pipe system and curb inlets • Upsize pipes • Re-establish positive pipe slopes • Stabilize, widen, and clean streams at system inlets	• Clean existing RCP pipe system and curb inlets • Upsize pipes • Re-establish positive pipe slopes • Stabilize, widen, and clean streams at system inlets • Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity	• Clean existing RCP pipe system and curb inlets • Upsize pipes • Re-establish positive pipe slopes • Stabilize, widen, and clean streams at system inlets • Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity	• Clean existing RCP pipe system and curb inlets • Upsize pipes • Re-establish positive pipe slopes • Stabilize, widen, and clean streams at system inlets • Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity
	2	Description	• Does not address Purpose and Need	• Roadway may still flood during larger, high volume rainfall events. • Will increase flooding downstream	• Roadway may still flood during larger, high volume rainfall events. • Will increase flooding downstream	• Flooding may still occur in larger, high intensity events • ROW acquisition may be required.	• Flooding may still occur in larger, high intensity events • ROW acquisition may be required.
Purpose & Need							
Address chronic flooding	3	Y/N	N	Y	Y	Y	Y
	4	Description	None	25 year storm event	25 year storm event	25 year storm event	25 year storm event
Goals & Objectives							
Minimize present day flooding while implementing a resilient design to account for future flooding conditions	5	Y/N	N	Y	Y	Y	Y
Avoid and/or minimize environmental impacts	6	Y/N	N/A	Y	Y	Y	Y
Minimize right-of-way impacts	7	Y/N	N/A	Y	Y	N	N
Minimize utility impacts and relocations	8	Y/N	N/A	Y	Y	N	N
Environmental							
Approximate Wetland and Waterway Impacts	9	Y/N	N/A	Y	Y	Y	Y
	10	Y/N	N/A	Y	Y	N	N
Rights-of-Way							
Construction Duration and Cost							
Construction Duration	11	months	N/A	2	2	3	3
	12	\$	N/A	\$1,020,000	\$960,000	\$1,090,000	\$1,020,000

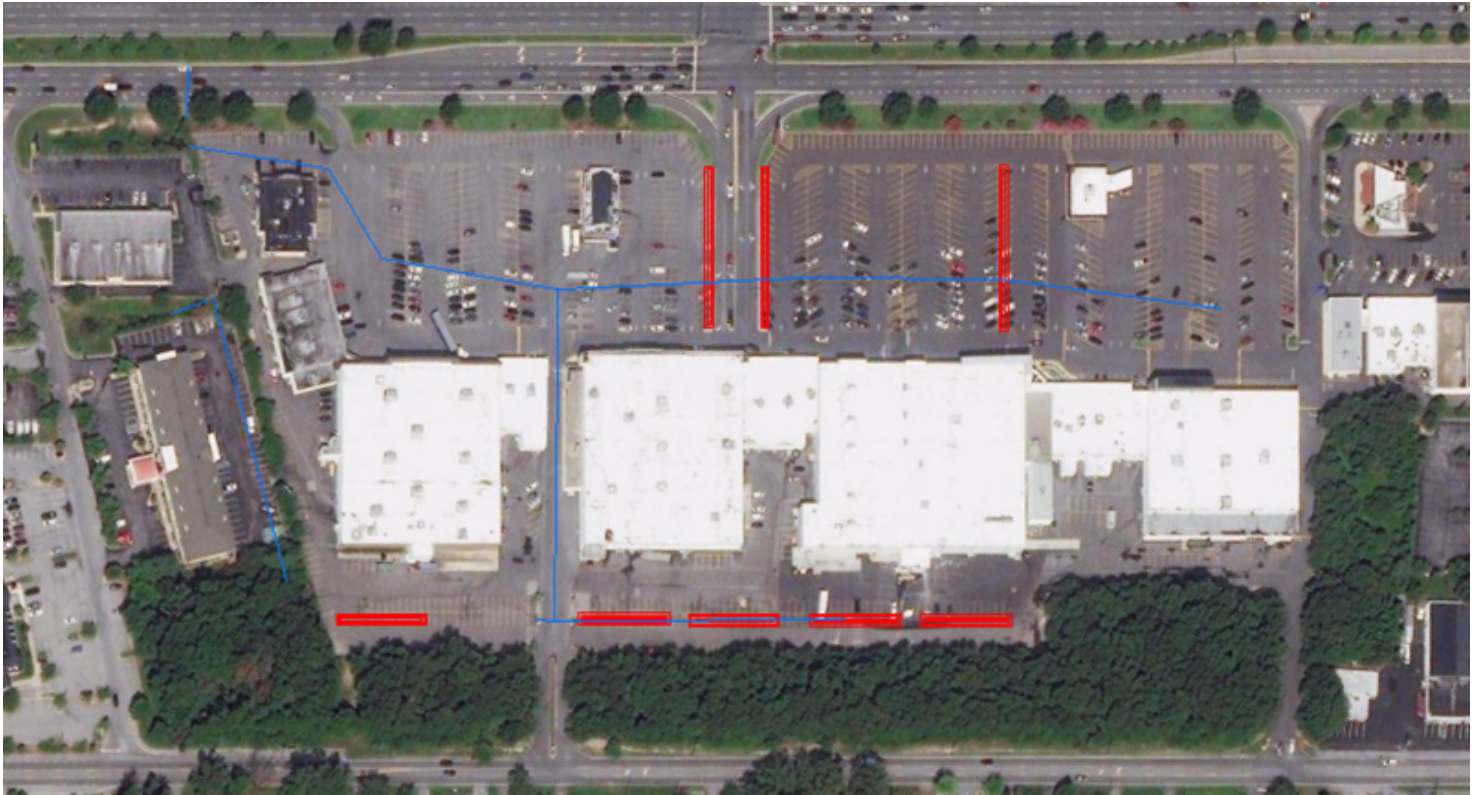
Notes: 1. 48" RCP assumed \$500/LF
2. 58" x 91" RCEP assumed \$800/LF
3. Ancillary drainage assumed \$150/LF
4. Approximately 6 drainage structures (inlets/manhole) need to be replaced/reconstructed assumed at \$2,000/ea
5. Assumed \$100,000 for mobilization, traffic control, and access
6. Assumed \$50,000 for pavement work
7. Assumed \$50,000 assumed for GI/basin
8. Headwalls assumed \$75,000/ea
9. Excavation and stream diversion assumed \$200,000
9. 30% added contingency

5: Drainage System Improvements; replace 60" RCP with 58" x 91" RCEP and add GI
• Clean existing RCP pipe system and curb inlets • Upsize pipes • Re-establish positive pipe slopes • Stabilize, widen, and clean streams at system inlets • Install additional GI surface retention and curb cuts to capture runoff close to the source, provide storage, and increase overall system storage capacity
• Flooding may still occur in larger, high intensity events • ROW acquisition may be required.
Y
25 year storm event
Y
N
N
Y
N
3
\$1,020,000

Alternatives Matrix - Location 24: Poplar Hill Rd between St. Peters Church Rd & Mattawoman Beantown Rd

December 2022

Alternatives			1: No Build	2: Replace with dual 60" RCP and restore stream	3: Replace dual 60" CMPs with dual 60" RCP, raise the low point of the roadway, and perform stream restoration	4: Replace dual 60" CMPs with dual 72" RCP (beveled entrance), replace 22" HDPE with 36" HDPE and stream restoration	5: Replace dual 60" CMPs with single 10' x 5' reinforced concrete box culvert and stream restoration	PPA *pending SME and local official feedback	
								4: Replace dual 60" CMPs with dual 72" RCP (beveled entrance), replace 22" HDPE with 36" HDPE and stream restoration	
Overview									
Advantages	1	Description	• No advantages.	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls	• Promote positive drainage by upsizing old drainage system • Increase conveyance along the stream through restoration and debris removal • Reduce scour and erosion by stabilizing stream banks and outfalls
	2	Description	• Does not address Purpose and Need	• Does not meet the 25 year flood capacity	• Most costly option • Longest construction duration • Roadway will need to be raised a couple of feet to meet 25 year capacity	• Roadway will still flood during larger, high volume rainfall events.	• Does not meet the 25 year flood capacity	• Roadway will still flood during larger, high volume rainfall events.	• Roadway will still flood during larger, high volume rainfall events.
Purpose & Need									
Address chronic flooding	3	Y/N	N	N	Y	Y	N	Y	
	4	Description	Does not meet 25 year rainfall event	Does not meet 25 year rainfall event	25 year rainfall event	25 year rainfall event (2050, 2100)	Does not meet 25 year rainfall event	25 year rainfall event (2050, 2100)	
Goals & Objectives									
Minimize present day flooding while implementing a resilient design to account for future flooding conditions	5	Y/N	N	N	Y	Y	N	Y	
Avoid and/or minimize environmental impacts	6	Y/N	N/A	Y	Y	Y	Y	Y	
Minimize right-of-way impacts	7	Y/N	N/A	Y	Y	Y	Y	Y	
Minimize utility impacts and relocations	8	Y/N	N/A	Y	Y	Y	Y	Y	
Environmental									
Approximate Wetland and Waterway Impacts	9	Y/N	N/A	Y	Y	Y	Y	Y	
Rights-of-Way									
Within ROW	10	Y/N	N/A	Y	Y	Y	Y	Y	
Construction Duration and Cost									
Construction Duration	11	months	N/A	3	5	4	3	4	
	12	\$	N/A	\$960,000	\$1,020,000	\$980,000	\$1,120,000	\$980,000	
Total Project Cost									
Notes:		1. 60" RCP assumed \$400/LF 2. 72" RCP assumed \$600/LF 3. Pipe Excavation assumed \$100,000 4. 10'x5' Box Culvert assumed \$2,000/LF 5. 36" HDPE assumed \$120/LF 6. Stream restoration assumed \$200,000 7. Stream diversion assumed \$150,000 8. Headwall assumed \$100,000/ea 9. Assumed \$50,000 for mobilization, access, and traffic control 10. Profile raise assume \$50,000 11. 30% added contingency							



Location 10: Old Washington Rd and Shoppers World Potential Basin Locations



Location 12: Industrial Park and Post office Road Potential Basin Location